# LRFD Beam-Column Graphical Design Aid

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## ABSTRACT

A graphical design aid is presented for beam-columns, members subjected to combined loading of axial forces and bending moments, designed in accordance with the American Institute of Steel Construction's (AISC) 1993 *LRFD Specification for Structural Steel Buildings*. Design aids have been published in the AISC *LRFD Manual of Steel Construction,* 2nd Edition, addressing many facets of structural steel design. These include the beam tables, beam charts, and column tables. However, meager information is available revealing how to design a beam-column accurately and quickly. The common method is entirely based on an assumed axial load due to bending moments which is then used via trial-and-error to size a member from the column (axial load only) design tables. There are various problems with this method of design.

This article presents an alternative design procedure based on the Equations H1-1a and H1-1b of the 1993 *LRFD Specification for Structural Steel Buildings*. The proposed design method consists of a standard set of graphs depicting the interaction diagram for steel W-shapes commonly used as column members. The diagrams are derived for structural members subjected to axial compression and strong-axis bending. This new procedure also utilizes a set of linear transformation factors applied to design conditions different from the graphical standard. This method is advantageous to design engineers because it facilitates the selection of a beam-column.


## INTRODUCTION

The AISC *LRFD Manual of Steel Construction,* 2nd Edition, provides aids for the designer of steel columns and beams. The design of columns for axial loads only is precisely tabulated for several shapes commonly used as columns. The design of beams for strong-axis bending moments is accurately tabulated and plotted for several shapes commonly used as beams. However, a trial-and-error solution process is suggested to design a beam-column, a member subjected to combined axial load and bending moments (refer to Preliminary Beam-Columns, Table 3-2, LRFD Manual, Volume I, 2nd Edition). Design by trial-and-error is enlightening through chance and discovery but this process does consume valuable time. A more precise method would expedite the design procedure to repeat the task efficiently.

The scope of this article is to introduce and propose a simplified LRFD design aid for beam-columns. Wide-flange shapes normally used as structural columns, with a combined loading of an axial compressive load and a strong-axis bending moment are addressed. This document recommends a new design approach and demonstrates how to perform the required calculations. The proposed design procedure utilizes a standard interaction diagram and various conversion factors to efficiently design beam-columns. The conversion factors are necessary for the linear transformation of design conditions different from the graphical standards.

The proposed design procedure is derived from Equations H1-1a and H1-1b of the 1993 LRFD Specification which define the interaction diagram for the design of a beam-column (refer to Figure 1, which is identical to Figure C-H1.1 in the 1993 LRFD Specification). Any combination of axial load, $P_u$, and bending moment, $M_u$, that plots below or on the line indicates an acceptable result. Any condition plotted above the member interaction line is not adequate. Interaction diagrams have been developed for a compressive axial load and bending moment

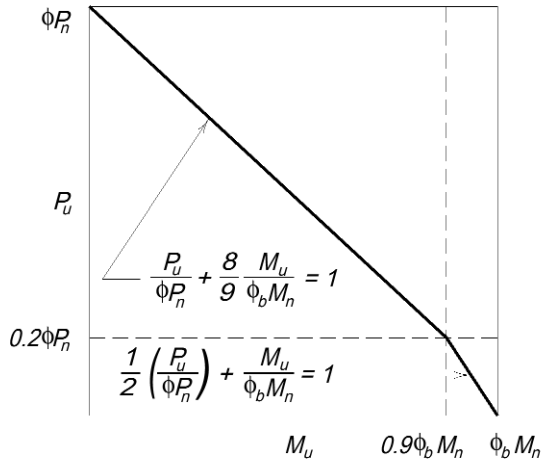



*Fig. 1. Typical beam-column interaction curve per LRFD Specifications.*

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about the major axis. These design curves comply with AISC's 1993 LRFD Specification.

## DERIVATION OF THE DESIGN PROCEDURE

A beam-column must conform to the interaction Equations H1-1a and H1-1b defined in LRFD Specification Chapter H. The plot of both equations yields a continuous interaction diagram similar to Figure 1 for every member. This graph is affected by the column member size, column end conditions, the unbraced length, and lateral-torsional buckling criteria.

The following derivation by example illustrates the author's discovery process. Curves 1, 2, and 3 in Figure 2 are plotted with the assumption that the unbraced length is equal to the effective length. A single member, W14×61, is graphed with differing lengths and end conditions in Figure 2.

Curve 1 in Figure 2 depicts the interaction diagram for the following conditions:

Member Shape = W14×61
$F_y$ = 50 ksi
$K$ =1.0
$KL_x$, $KL_y$, $L_b$ = 12 ft
$C_b$ = 1.0
$\phi P_n$ = 591 kips
$\phi M_n$ = 361 kip-ft

The point of intersection of lines H1-1a and H1-1b can be algebraically derived once all the other variables are known. The basis for the nominal axial strength is defined in LRFD Specification Chapter E. Likewise, the basis for the nominal moment strength is defined in LRFD Specification Chapter F.

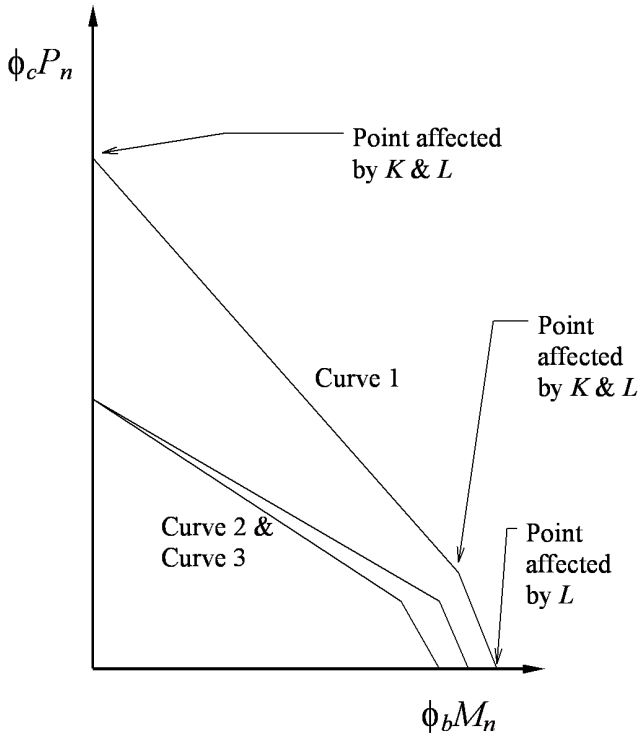



*Fig. 2. Interaction diagram plots.*

Conservative assumptions of $C_b$ = 1.0 and $L_b = KL_x$, $KL_y$ were selected to simplify the design standards. However, $L_b = KL$ is unconservative for values of $K$ less than one. For example, if $K$ is equal to 0.5 and $L$ is equal to 40 ft, then the moment strength would be based on $KL$ equal to 20 ft instead of the correct value of 40 ft. The designer must be aware of the magnitude of this assumption. Proper detailing of the structure to conform to the design calculations is essential.

For every possible length there exists a similar interaction diagram for the W14×61. In addition to an infinite number of lengths, there are multiple end conditions that will affect the plotted diagram. The end conditions are incorporated with the effective length factor, $K$, and it varies from 0.5 to 2.10. The theoretical $K$ values and their physical interpretation can be found in Table C-C2.1 on page 6-184 of the LRFD Specification. The member length will also control what the plot looks like (see Figure 2 for affected points). An interaction diagram cannot be drawn for every member, every end condition and every length because there are an infinite number of combinations. Therefore, a correlation must be derived. The plots of Curve 2 and Curve 3 illustrate the graphical correlation.

Curve 2 in Figure 2 depicts the interaction diagram for the following conditions:

Member Shape = W14×61
$F_y$ = 50 ksi
$K$ =1.0
$L_b$ = KL = 24 ft
$C_b$ = 1.0
$\phi P_n$ = 276 kips
$\phi M_n$ = 315 kip-ft

Curve 3 in Figure 2 depicts the interaction diagram for the following conditions:

Member Shape = W14×61
$F_y$ = 50 ksi
$K$ =2.0
$L_x$, $L_y$ = 12 ft
$L_b = KL$ = 24 ft
$C_b$ = 1.0
$\phi P_n$ = 276 kips
$\phi M_n$ = 315 kip-ft

Notice that the last two conditions plot identically. Since both portions of the interaction diagram are straight lines, a simple linear transformation can be used to convert any length and end condition to a selected graphical standard.

Curve 3′ illustrates the interaction diagram for the W14×61 if the unbraced length is not equal to the effective length.

Curve 3′ in Figure 2 depicts the interaction diagram for the following conditions:

Member Shape = W14×61

$F_y$ = 50 ksi
$K$ = 2.0
$L_x$, $L_y$ = 12 ft
$L_b$ = 12 ft
$C_b$ = 1.0

$\phi P_n$ = 276 kips
$\phi M_n$ = 361 kip-ft

Take note that the maximum axial load remains the same as Curve 3 and therefore the axial portion of the point of intersection of Equations H1-1a and H1-1b remains the same. However, the flexural strength for the member plot for Curve 3′ has increased resulting in a shift in the curve. As long as $KL$ is greater than $L_b$, the standard interaction graphs will be conservative. If $KL$ is less than $L_b$, then the standard interaction graphs will be unconservative. In order to simplify the design procedure, the assumption that the limiting effective length, $KL$, is equal to $L_b$ was used to construct the interaction diagrams.

As with all design aids there are assumptions that are included in the derivation of the method. The basic assumptions for the construction of the standard column interaction curves are:

- the material is A992 steel;
- the member is subjected to axial compression and strong-axis bending only;
- the member graphs are derived with $K$ = 1.0 and $L$ = 12 ft;
- the flexural strength of the section is based on $L_b$ = KL and $C_b$ = 1.0; and
- the point of intersection of Equations H1-1a and H1-1b is derived algebraically from the other known values.

With the above correlation, a set of conversion factors is defined that is used to perform the linear transformations. Two conversion factors are necessary because the end condition and the length affect the axial strength and the length of the member affects the flexural strength. Conversion factors were calculated for 50 ksi steel. Additional factors may be calculated by using the equations discussed below.

The end conditions and the length affect the axial strength. Therefore, to use an interaction diagram with $K$ = 1.0 and $L$ = 12 ft a conversion factor is needed for a member that does not have $K$ = 1.0 and $L$ = 12 ft. The general form of the equation is:

$$\phi_c P_{n(KL = 12\text{ ft})} = B_{KL} \times \phi_c P_{n(KL \neq 12\text{ ft})}$$

In general, the conversion factor, $B_{KL}$, for a different effective length due to the end condition and length is defined as:

$$B_{KL} = [\phi_c P_{n(KL = 12\text{ ft})}] / [\phi_c P_{n(KL \neq 12\text{ ft})}]$$

The length of the member affects the flexural strength. Therefore, a conversion factor is needed for the bending moment when a member's effective length is not equal to 12 ft. The general form of the equation for the moment capacity factor is:

$$\phi_b M_{n(KL = 12\text{ ft})} = B_{LM} \times \phi_b M_{n(KL \neq 12)}$$

In general, the conversion factor, $B_{LM}$, for a member's different effective length is defined as:

$$B_{LM} = [\phi_b M_{n(KL = 12\text{ ft})}] / [\phi_b M_{n(KL \neq 12\text{ ft})}]$$

Hence, if a member does not have $L$ = 12 ft or $K$ = 1.0 then two linear transformations are required: 1) for the axial load conversion due to the different effective length and 2) for the bending moment conversion due to the deviation of the member's effective length from the graphical standard. Since the conversion factors are based on the individual member's axial and flexural strength, a set of initial design approximations was created (see Appendix B). These approximations are an average of the exact values (see Appendix D) and allow the use of the design aid without previously knowing the member size, except for a target group size such as W14.

As can be determined from the list in Appendix D, the values of $B_{KL}$ and $B_{LM}$ vary within each group size. The lighter members of each group size vary by a greater margin than the heavier members of a group. So the lighter members were ignored when computing the average for the design approximations of $B_{KL}$ and $B_{LM}$. The design approximations may be utilized for all member weights listed even if it was not included in the average calculation of the design approximation. The design approximations for W14s includes members weighing 90 pounds per linear foot (plf) to 730 plf. The design approximations for W12s includes members weighing 53 plf to 336 plf. The design approximations for W10s includes members weighing 49 plf to 112 plf. All W8s and W6s listed are included in the calculation of the design approximations.

The author must caution the designer to confirm that the design conditions, such as the effective slenderness ratio and the lateral-torsional buckling criteria, for the graphical standards, $K$ = 1.0, $L$ = 12 ft, and $F_y$ = 50 ksi, are maintained at the differing condition requiring the transformation. In other words, verification that the effective slenderness ratio remains below 200 and that the section maintains the same lateral-torsional buckling criteria must be calculated for the actual conditions. Furthermore, the unbraced length, $L_b$, shall be considered equal to the effective length, $KL$. Review Appendix E to see a listing of conditions where the slenderness ratio would be exceeded for each conversion.

In summary, the tabulated values are for shapes typically used as columns; however, this graphical approach may be applied to all shapes provided that adherence to the graphical standards is maintained. The additional interaction dia-

grams may be plotted along with the curves in Appendix D. The graphical design method is limited to a combined loading of an axial compressive force and a major-axis bending moment because a graphical method for a column with biaxial bending would require a three-dimensional graph, one axis for the axial load and one axis each for the orthogonal bending moments.

## PROPOSED DESIGN PROCEDURE

This graphical design procedure for a steel beam-column is a precise method that incorporates the correct interaction of a compressive axial load and a bending moment according to the LRFD Specification. The procedure is as follows:

1. Given the effective length factor, $K$, and the member length, $L$, find the appropriate design approximations for $B_{KL}$ and $B_{LM}$ from Appendix B where:
   $B_{KL}$ = axial conversion factor
   $B_{LM}$ = bending moment conversion factor
   Note: The tabulated design approximations deviate less than 10 percent from the true values for the majority of the shapes in a given group classification such as W14. Linear interpolation between the conversion factors is valid with the difference being less than 0.5 percent from the true value.
2. Calculate $P_u' = B_{KL} \times P_u$
   Calculate $Mu' = B_{LM} \times M_u$
   where:
   $P_u$ = factored axial load, kips
   $M_u$ = factored bending moment, kip-ft
   $P_u'$ = transformed axial load, kips
   $M_u'$ = transformed bending moment, kip-ft
3. Plot ($M_u'$, $P_u'$) on the appropriate graph in Appendix D and select a member whose interaction diagram lies above and to the right of the plotted point.
4. Find the exact values of $B_{KL}$ and $B_{LM}$ from Appendix C for the member selected.
5. Recalculate $M_u'$ and $P_u'$.
6. Replot ($M_u'$, $P_u'$) on the appropriate graph in Appendix D to verify that the member selected is adequate.
7. Confirm the selected member is adequate with the applicable provisions of the AISC LRFD Specification.

## ILLUSTRATIVE EXAMPLE

The following example demonstrates the application of the proposed method. Note, the interaction calculation checks use the actual unbraced length, $L_b$, to determine the bending moment.

**Example**

Given the loading below, select the lightest W14 and W12:

$P_u$ = 3,400 kips  $K$ = 1.0
$M_u$ = 650 kip-ft  $L$ = 16 ft
$F_y$ = 50 ksi

Determine the design approximations for the W14 first (Appendix B):

$B_{KL}$ = 1.072
$B_{LM}$ = 1.007
$P_u' = B_{KL} \times P_u$
$= 1.072 \times 3{,}400 = 3{,}640$ kips
$M_u' = B_{LM} \times M_u$
$= 1.007 \times 650 = 655$ kip-ft

Plot the point ($M_u'$, $P_u'$) = (655, 3,640) on the appropriate graph in Appendix D.

From the plotted point, proceed up and to the right across the page until the lightest W14 is found. Try W14×398.

Determine the exact values of $B_{KL}$ and $B_{LM}$ from Appendix C:

$B_{KL}$ = 1.066
$B_{LM}$ = 1.002
$P_u' = B_{KL} \times P_u$
$= 1.066 \times 3{,}400 = 3{,}620$ kips
$M_u' = B_{LM} \times M_u$
$= 1.002 \times 650 = 651$ kip-ft

The transformed point plots to the left of the first point, therefore select W14×398 again.

To confirm the procedure, verify the result by using Equation H1-1a:

$\phi P_n$ = 4,300 kips via the column tables, Part 3, LRFD Manual, 2nd Edition.
$\phi M_n$ = 2,997 kip-ft via Chapter F, Part 6, LRFD Specification (December 1993).

Interaction Calculation = 0.983

**Use W14×398.**

Determine the design approximations for the W12 (Appendix B):

$B_{KL}$ = 1.131
$B_{LM}$ = 1.031

By inspection of the graphs, the largest W12 is located down and to the left of the first plotted point. By inspection of the design approximation tables, the $B_{KL}$ and $B_{LM}$ factors are greater for a W12 than a W14. Therefore, it can be concluded that no adequate W12 section exists.

## CONCLUSION

A graphical design aid for beam-column members has been presented. By utilizing a standard set of graphs conforming to the interaction Equations H1-1a and H1-1b and conversion factors, most members can be designed accurately and efficiently. The conversion factors allow many design conditions to be made equivalent to the graphical standards and facilitate the selection of a beam-column. This design method is advantageous to design engineers performing hand calculations or checking computer program results because it expedites the design of a complex framing member. Some advantages associated with this design procedure are it reduces the number of calculations required thereby reducing design time and cost and it is a more precise method based on the LRFD Specifications instead of an equivalent axial load equation involving trial-and-error.

## REFERENCES


AISC (1994), *LRFD Manual of Steel Construction*, 2nd ed., American Institute of Steel Construction, Chicago, IL.

AISC (1995), *ASD Manual of Steel Construction*, 2nd rev., 9th ed., American Institute of Steel Construction, Chicago, IL.

Austin, Walter J. (1961), "Strength and Design of Metal Beam-Columns," *Journal of the Structural Division*, ASCE, Vol. 87, No. ST4, April, pp. 1-32.

Bjorhovde, Reidar, Galambos, Theodore V., and Ravindra, Mayasandra K. (1978), "LRFD Criteria for Steel Beam-Columns," *Journal of the Structural Division*, ASCE, Vol. 104, No. ST9, September, pp. 1371-1387.

Chen, Wai-Fah and Zhou, Suiping (1987), "$C_m$ Factor in Load and Resistance Factor Design," *Journal of Structural Engineering*, ASCE, Vol. 113, No. 8, August, pp. 1738-1754.

Cheong-Siat-Moy, Francois and Downs, Tom (1980), "New Interaction Equation for Steel Beam-Columns," *Journal of the Structural Division*, ASCE, Vol. 106, No. ST5, May, pp. 1047-1061.

Duan, Lian and Chen, Wai-Fah (1989), "Design Interaction Equation for Steel Beam-Columns," *Journal of Structural Engineering*, ASCE, Vol. 115, No. 5, May, pp. 1225-1243.

LeMessurier, W. J. (1976), "A Practical Method of Second Order Analysis: Part 1—Pin Jointed Systems," *Engineering Journal*, AISC, Vol. 13, No. 4, Fourth Quarter, pp. 89-96.

LeMessurier, W. J. (1977), "A Practical Method of Second Order Analysis: Part 2—Rigid Frames," *Engineering Journal*, AISC, Vol. 14, No. 2, Second Quarter, pp. 49-67.

Massonnet, Charles (1959), "Stability Considerations in the Design of Steel Columns," *Journal of the Structural Division*, ASCE, Vol. 85, No. ST7, September, pp. 75-111.

Monasa, Frank and Snyder, John K (1981), "Generalized Design of Columns Subjected to Combined Axial Load and Bending Moment," *Engineering Journal*, AISC, Vol.18, No. 1, First Quarter, pp. 8-21.

Myers, Greg, AutoLISP program for member plots.

Salmon, Charles G. and Johnson, John E. (1990), *Steel Structures Design and Behavior*, 3rd ed., Harper & Row, New York.

Sokal, Iqbal S., Duan, Lian and Chen, Wai-Fah (1989), "Design Interaction Equations for Steel Members," *Journal of Structural Engineering*, ASCE, Vol. 115, No. 7, July, pp. 1225-1243.

Uang, Chia-Ming, Wattar, Samar W., and Leet, Kenneth M. (1990) "Proposed Revision of the Equivalent Axial Load Method for LRFD Steel and Composite Beam-Column Design," *Engineering Journal*, AISC, Fourth Quarter, pp. 150-157.

United States Steel (1969), *Column Design Curves*, Pittsburgh, PA.


## APPENDIX A—NOTATION

$\phi_b$ = resistance factor for flexure
$\phi_c$ = resistance factor for compression
$B_{KL}$ = axial conversion factor for effective length, *KL*, not equal to 12 ft
$B_{LM}$ = bending conversion factor for effective length, *KL*, not equal to 12 ft
$C_b$ = bending coefficient dependent upon the moment gradient between bracing points.
$F_y$ = specified minimum yield stress of the steel type being analyzed, ksi
$K$ = effective length factor for a prismatic member
$l$ = unbraced length of member, in.
$L$ = unbraced length of member, ft
$L_b$ = laterally unbraced length of member, ft
$L_p$ = limiting laterally unbraced length of member for full plastic bending capacity, ft
$L_r$ = limiting laterally unbraced member length for inelastic lateral-torsional buckling, ft
$m$ = coefficient for converting bending to an approximate equivalent axial load in columns subjected to combined loading conditions
$M_n$ = nominal flexural strength, kip-ft
$M_u$ = required flexural strength, kip-ft
$M_u'$ = transformed required flexural strength, kip-ft
$P_n$ = nominal axial strength (compression), kips
$P_u$ = required axial strength (compression), kips
$P_u'$ = transformed required axial strength (compression), kips

## APPENDIX B—DESIGN APPROXIMATIONS OF $B_{KL}$ AND $B_{LM}$

| | $B_{KL}$ & $B_{LM}$ Values (50 ksi) | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| | $KL$ (ft) | | | | | | | | | |
| | 6.00 | | 8.00 | | 10.00 | | 12.00 | | 14.00 | |
| Shape | $B_{KL}$ | $B_{LM}$ | $B_{KL}$ | $B_{LM}$ | $B_{KL}$ | $B_{LM}$ | $B_{KL}$ | $B_{LM}$ | $B_{KL}$ | $B_{LM}$ |
| W14 | 0.935 | 1.000 | 0.952 | 1.000 | 0.973 | 1.000 | 1.000 | 1.000 | 1.033 | 1.001 |
| W12 | 0.888 | 0.990 | 0.916 | 0.990 | 0.953 | 0.992 | 1.000 | 1.000 | 1.059 | 1.015 |
| W10 | 0.845 | 0.971 | 0.883 | 0.971 | 0.934 | 0.979 | 1.000 | 1.000 | 1.084 | 1.022 |
| W8 | 0.736 | 0.917 | 0.796 | 0.935 | 0.882 | 0.966 | 1.000 | 1.000 | 1.161 | 1.037 |
| W6 | 0.607 | 0.874 | 0.691 | 0.912 | 0.816 | 0.954 | 1.000 | 1.000 | 1.271 | 1.051 |

| | $B_{KL}$ & $B_{LM}$ Values (50 ksi) | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| | $KL$ (ft) | | | | | | | | | |
| | 16.00 | | 18.00 | | 20.00 | | 22.00 | | 24.00 | |
| Shape | $B_{KL}$ | $B_{LM}$ | $B_{KL}$ | $B_{LM}$ | $B_{KL}$ | $B_{LM}$ | $B_{KL}$ | $B_{LM}$ | $B_{KL}$ | $B_{LM}$ |
| W14 | 1.072 | 1.007 | 1.118 | 1.015 | 1.172 | 1.023 | 1.235 | 1.032 | 1.308 | 1.041 |
| W12 | 1.131 | 1.031 | 1.220 | 1.047 | 1.327 | 1.064 | 1.457 | 1.082 | 1.615 | 1.101 |
| W10 | 1.190 | 1.045 | 1.323 | 1.069 | 1.489 | 1.094 | 1.698 | 1.121 | 1.959 | 1.149 |
| W8 | 1.383 | 1.077 | 1.668 | 1.125 | 2.029 | 1.190 | 2.456 | 1.261 | 2.922 | 1.343 |
| W6 | 1.656 | 1.107 | 2.096 | 1.177 | 2.588 | 1.287 | 3.131 | 1.416 | 3.727 | 1.560 |

| | $B_{KL}$ & $B_{LM}$ Values (50 ksi) | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| | $KL$ (ft) | | | | | | | | | |
| | 26.00 | | 28.00 | | 30.00 | | 32.00 | | 34.00 | |
| Shape | $B_{KL}$ | $B_{LM}$ | $B_{KL}$ | $B_{LM}$ | $B_{KL}$ | $B_{LM}$ | $B_{KL}$ | $B_{LM}$ | $B_{KL}$ | $B_{LM}$ |
| W14 | 1.392 | 1.050 | 1.489 | 1.059 | 1.601 | 1.069 | 1.730 | 1.078 | 1.879 | 1.088 |
| W12 | 1.805 | 1.121 | 2.029 | 1.148 | 2.296 | 1.177 | 2.602 | 1.226 | 2.937 | 1.263 |
| W10 | 2.290 | 1.178 | 2.656 | 1.210 | 3.048 | 1.249 | 3.468 | 1.298 | 3.916 | 1.353 |
| W8 | 3.430 | 1.435 | 3.978 | 1.534 | 4.566 | 1.634 | 5.195 | 1.738 | 5.865 | 1.845 |
| W6 | 4.373 | 1.704 | 5.072 | 1.848 | 5.823 | 1.990 | 6.625 | 2.132 | 7.479 | 2.274 |

| | $B_{KL}$ & $B_{LM}$ Values (50 ksi) | | | |
|---|---|---|---|---|
| | $KL$ (ft) | | | |
| | 36.00 | | 38.00 | |
| Shape | $B_{KL}$ | $B_{LM}$ | $B_{KL}$ | $B_{LM}$ |
| W14 | 2.052 | 1.099 | 2.250 | 1.109 |
| W12 | 3.293 | 1.303 | 3.669 | 1.345 |
| W10 | 4.390 | 1.410 | 4.891 | 1.473 |
| W8 | 6.575 | 1.952 | 7.326 | 2.061 |
| W6 | 8.385 | 2.416 | 9.342 | 2.557 |

## APPENDIX C—$B_{KL}$ AND $B_{LM}$ VALUES (50 ksi)

| | $B_{KL}$ and $B_{LM}$ Values (50 ksi) | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| | KL (ft) | | | | | | | | | |
| | 6.00 | | 8.00 | | 10.00 | | 12.00 | | 14.00 | |
| Shape | $B_{KL}$ | $B_{LM}$ | $B_{KL}$ | $B_{LM}$ | $B_{KL}$ | $B_{LM}$ | $B_{KL}$ | $B_{LM}$ | $B_{KL}$ | $B_{LM}$ |
| W14x730 | 0.950 | 1.000 | 0.962 | 1.000 | 0.979 | 1.000 | 1.000 | 1.000 | 1.025 | 1.000 |
| W14x665 | 0.948 | 1.000 | 0.961 | 1.000 | 0.979 | 1.000 | 1.000 | 1.000 | 1.026 | 1.000 |
| W14x605 | 0.947 | 1.000 | 0.960 | 1.000 | 0.978 | 1.000 | 1.000 | 1.000 | 1.027 | 1.000 |
| W14x550 | 0.945 | 1.000 | 0.959 | 1.000 | 0.977 | 1.000 | 1.000 | 1.000 | 1.028 | 1.000 |
| W14x500 | 0.944 | 1.000 | 0.958 | 1.000 | 0.977 | 1.000 | 1.000 | 1.000 | 1.028 | 1.000 |
| W14x455 | 0.942 | 1.000 | 0.957 | 1.000 | 0.976 | 1.000 | 1.000 | 1.000 | 1.029 | 1.000 |
| W14x426 | 0.941 | 1.000 | 0.956 | 1.000 | 0.976 | 1.000 | 1.000 | 1.000 | 1.029 | 1.000 |
| W14x398 | 0.941 | 1.000 | 0.956 | 1.000 | 0.975 | 1.000 | 1.000 | 1.000 | 1.030 | 1.000 |
| W14x370 | 0.940 | 1.000 | 0.955 | 1.000 | 0.975 | 1.000 | 1.000 | 1.000 | 1.030 | 1.000 |
| W14x342 | 0.939 | 1.000 | 0.954 | 1.000 | 0.975 | 1.000 | 1.000 | 1.000 | 1.031 | 1.000 |
| W14x311 | 0.938 | 1.000 | 0.953 | 1.000 | 0.974 | 1.000 | 1.000 | 1.000 | 1.032 | 1.000 |
| W14x283 | 0.937 | 1.000 | 0.953 | 1.000 | 0.974 | 1.000 | 1.000 | 1.000 | 1.032 | 1.000 |
| W14x257 | 0.936 | 1.000 | 0.952 | 1.000 | 0.973 | 1.000 | 1.000 | 1.000 | 1.033 | 1.000 |
| W14x233 | 0.935 | 1.000 | 0.951 | 1.000 | 0.973 | 1.000 | 1.000 | 1.000 | 1.033 | 1.000 |
| W14x211 | 0.934 | 1.000 | 0.950 | 1.000 | 0.972 | 1.000 | 1.000 | 1.000 | 1.034 | 1.000 |
| W14x193 | 0.933 | 1.000 | 0.950 | 1.000 | 0.972 | 1.000 | 1.000 | 1.000 | 1.034 | 1.000 |
| W14x176 | 0.932 | 1.000 | 0.949 | 1.000 | 0.972 | 1.000 | 1.000 | 1.000 | 1.034 | 1.000 |
| W14x159 | 0.931 | 1.000 | 0.949 | 1.000 | 0.971 | 1.000 | 1.000 | 1.000 | 1.035 | 1.000 |
| W14x145 | 0.931 | 1.000 | 0.948 | 1.000 | 0.971 | 1.000 | 1.000 | 1.000 | 1.035 | 1.000 |
| W14x132 | 0.923 | 1.000 | 0.942 | 1.000 | 0.968 | 1.000 | 1.000 | 1.000 | 1.039 | 1.006 |
| W14x120 | 0.922 | 1.000 | 0.942 | 1.000 | 0.967 | 1.000 | 1.000 | 1.000 | 1.040 | 1.007 |
| W14x109 | 0.922 | 1.000 | 0.941 | 1.000 | 0.967 | 1.000 | 1.000 | 1.000 | 1.040 | 1.008 |
| W14x99 | 0.921 | 1.000 | 0.941 | 1.000 | 0.967 | 1.000 | 1.000 | 1.000 | 1.041 | 1.000 |
| W14x90 | 0.920 | 1.000 | 0.940 | 1.000 | 0.967 | 1.000 | 1.000 | 1.000 | 1.041 | 1.000 |
| W14x82 | 0.831 | 0.955 | 0.872 | 0.955 | 0.927 | 0.971 | 1.000 | 1.000 | 1.093 | 1.030 |
| W14x74 | 0.831 | 0.951 | 0.872 | 0.951 | 0.927 | 0.969 | 1.000 | 1.000 | 1.093 | 1.033 |
| W14x68 | 0.829 | 0.947 | 0.870 | 0.947 | 0.926 | 0.967 | 1.000 | 1.000 | 1.095 | 1.035 |
| W14x61 | 0.827 | 0.943 | 0.869 | 0.943 | 0.926 | 0.965 | 1.000 | 1.000 | 1.096 | 1.037 |
| W14x53 | 0.735 | 0.888 | 0.796 | 0.912 | 0.882 | 0.954 | 1.000 | 1.000 | 1.160 | 1.051 |
| W14x48 | 0.732 | 0.880 | 0.794 | 0.906 | 0.881 | 0.951 | 1.000 | 1.000 | 1.162 | 1.055 |
| W12x336 | 0.910 | 1.000 | 0.932 | 1.000 | 0.962 | 1.000 | 1.000 | 1.000 | 1.047 | 1.005 |
| W12x305 | 0.907 | 1.000 | 0.931 | 1.000 | 0.961 | 1.000 | 1.000 | 1.000 | 1.048 | 1.006 |
| W12x279 | 0.905 | 1.000 | 0.929 | 1.000 | 0.960 | 1.000 | 1.000 | 1.000 | 1.049 | 1.007 |
| W12x252 | 0.903 | 0.999 | 0.927 | 0.999 | 0.959 | 0.999 | 1.000 | 1.000 | 1.050 | 1.008 |
| W12x230 | 0.901 | 0.999 | 0.926 | 0.999 | 0.959 | 0.999 | 1.000 | 1.000 | 1.051 | 1.008 |
| W12x210 | 0.900 | 0.998 | 0.925 | 0.998 | 0.958 | 0.998 | 1.000 | 1.000 | 1.052 | 1.009 |
| W12x190 | 0.898 | 0.997 | 0.923 | 0.997 | 0.957 | 0.997 | 1.000 | 1.000 | 1.053 | 1.010 |
| W12x170 | 0.896 | 0.997 | 0.922 | 0.997 | 0.956 | 0.997 | 1.000 | 1.000 | 1.054 | 1.011 |
| W12x152 | 0.894 | 0.996 | 0.921 | 0.996 | 0.955 | 0.996 | 1.000 | 1.000 | 1.055 | 1.012 |
| W12x136 | 0.892 | 0.994 | 0.919 | 0.994 | 0.955 | 0.994 | 1.000 | 1.000 | 1.056 | 1.014 |
| W12x120 | 0.890 | 0.993 | 0.918 | 0.993 | 0.954 | 0.993 | 1.000 | 1.000 | 1.057 | 1.016 |
| W12x106 | 0.889 | 0.991 | 0.917 | 0.991 | 0.953 | 0.991 | 1.000 | 1.000 | 1.058 | 1.018 |
| W12x96 | 0.888 | 0.990 | 0.916 | 0.990 | 0.953 | 0.990 | 1.000 | 1.000 | 1.059 | 1.019 |
| W12x87 | 0.886 | 0.988 | 0.915 | 0.988 | 0.952 | 0.988 | 1.000 | 1.000 | 1.060 | 1.021 |
| W12x79 | 0.885 | 0.986 | 0.913 | 0.986 | 0.951 | 0.986 | 1.000 | 1.000 | 1.061 | 1.023 |
| W12x72 | 0.884 | 0.985 | 0.913 | 0.985 | 0.951 | 0.985 | 1.000 | 1.000 | 1.061 | 1.025 |
| W12x65 | 0.883 | 1.000 | 0.912 | 1.000 | 0.950 | 1.000 | 1.000 | 1.000 | 1.062 | 1.000 |
| W12x58 | 0.835 | 0.952 | 0.875 | 0.952 | 0.929 | 0.969 | 1.000 | 1.000 | 1.091 | 1.033 |
| W12x53 | 0.831 | 0.947 | 0.872 | 0.947 | 0.927 | 0.967 | 1.000 | 1.000 | 1.093 | 1.036 |
| W12x50 | 0.744 | 0.902 | 0.803 | 0.921 | 0.886 | 0.959 | 1.000 | 1.000 | 1.153 | 1.045 |
| W12x45 | 0.739 | 0.893 | 0.799 | 0.914 | 0.884 | 0.955 | 1.000 | 1.000 | 1.157 | 1.049 |
| W12x40 | 0.737 | 0.884 | 0.798 | 0.908 | 0.883 | 0.952 | 1.000 | 1.000 | 1.158 | 1.053 |
| W10x112 | 0.854 | 0.983 | 0.889 | 0.983 | 0.938 | 0.987 | 1.000 | 1.000 | 1.079 | 1.014 |
| W10x100 | 0.851 | 0.980 | 0.887 | 0.980 | 0.936 | 0.985 | 1.000 | 1.000 | 1.081 | 1.016 |
| W10x88 | 0.848 | 0.977 | 0.885 | 0.977 | 0.935 | 0.983 | 1.000 | 1.000 | 1.082 | 1.018 |
| W10x77 | 0.845 | 0.973 | 0.883 | 0.973 | 0.934 | 0.981 | 1.000 | 1.000 | 1.084 | 1.020 |
| W10x68 | 0.844 | 0.969 | 0.882 | 0.969 | 0.933 | 0.978 | 1.000 | 1.000 | 1.085 | 1.023 |
| W10x60 | 0.842 | 0.965 | 0.880 | 0.965 | 0.932 | 0.976 | 1.000 | 1.000 | 1.086 | 1.026 |
| W10x54 | 0.841 | 0.961 | 0.879 | 0.961 | 0.932 | 0.973 | 1.000 | 1.000 | 1.087 | 1.028 |
| W10x49 | 0.838 | 0.957 | 0.878 | 0.957 | 0.931 | 0.971 | 1.000 | 1.000 | 1.089 | 1.031 |
| W10x45 | 0.755 | 0.918 | 0.812 | 0.932 | 0.892 | 0.965 | 1.000 | 1.000 | 1.145 | 1.038 |
| W10x39 | 0.748 | 0.906 | 0.807 | 0.923 | 0.889 | 0.960 | 1.000 | 1.000 | 1.150 | 1.044 |
| W10x33 | 0.739 | 0.889 | 0.799 | 0.911 | 0.884 | 0.954 | 1.000 | 1.000 | 1.157 | 1.051 |
| W8x67 | 0.776 | 0.959 | 0.829 | 0.964 | 0.902 | 0.981 | 1.000 | 1.000 | 1.130 | 1.019 |
| W8x58 | 0.773 | 0.953 | 0.826 | 0.958 | 0.900 | 0.979 | 1.000 | 1.000 | 1.132 | 1.022 |
| W8x48 | 0.769 | 0.943 | 0.823 | 0.950 | 0.898 | 0.974 | 1.000 | 1.000 | 1.135 | 1.027 |
| W8x40 | 0.761 | 0.929 | 0.817 | 0.940 | 0.895 | 0.969 | 1.000 | 1.000 | 1.141 | 1.033 |
| W8x35 | 0.759 | 0.920 | 0.815 | 0.933 | 0.894 | 0.965 | 1.000 | 1.000 | 1.142 | 1.037 |
| W8x31 | 0.757 | 0.912 | 0.813 | 0.926 | 0.893 | 0.962 | 1.000 | 1.000 | 1.144 | 1.042 |
| W8x28 | 0.648 | 0.869 | 0.725 | 0.909 | 0.838 | 0.952 | 1.000 | 1.000 | 1.232 | 1.053 |
| W8x24 | 0.645 | 0.854 | 0.723 | 0.897 | 0.836 | 0.946 | 1.000 | 1.000 | 1.235 | 1.061 |
| W6x25 | 0.611 | 0.886 | 0.694 | 0.921 | 0.818 | 0.959 | 1.000 | 1.000 | 1.267 | 1.045 |
| W6x20 | 0.603 | 0.862 | 0.688 | 0.903 | 0.814 | 0.949 | 1.000 | 1.000 | 1.275 | 1.057 |

## APPENDIX C—$B_{KL}$ AND $B_{LM}$ VALUES (50 ksi) (cont'd)

| | $B_{KL}$ and $B_{LM}$ Values (50 ksi) | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| | KL (ft) | | | | | | | | | |
| | 6.00 | | 8.00 | | 10.00 | | 12.00 | | 14.00 | |
| Shape | $B_{KL}$ | $B_{LM}$ | $B_{KL}$ | $B_{LM}$ | $B_{KL}$ | $B_{LM}$ | $B_{KL}$ | $B_{LM}$ | $B_{KL}$ | $B_{LM}$ |
| W14x730 | 0.950 | 1.000 | 0.962 | 1.000 | 0.979 | 1.000 | 1.000 | 1.000 | 1.025 | 1.000 |
| W14x665 | 0.948 | 1.000 | 0.961 | 1.000 | 0.979 | 1.000 | 1.000 | 1.000 | 1.026 | 1.000 |
| W14x605 | 0.947 | 1.000 | 0.960 | 1.000 | 0.978 | 1.000 | 1.000 | 1.000 | 1.027 | 1.000 |
| W14x550 | 0.945 | 1.000 | 0.959 | 1.000 | 0.977 | 1.000 | 1.000 | 1.000 | 1.028 | 1.000 |
| W14x500 | 0.944 | 1.000 | 0.958 | 1.000 | 0.977 | 1.000 | 1.000 | 1.000 | 1.028 | 1.000 |
| W14x455 | 0.942 | 1.000 | 0.957 | 1.000 | 0.976 | 1.000 | 1.000 | 1.000 | 1.029 | 1.000 |
| W14x426 | 0.941 | 1.000 | 0.956 | 1.000 | 0.976 | 1.000 | 1.000 | 1.000 | 1.029 | 1.000 |
| W14x398 | 0.941 | 1.000 | 0.956 | 1.000 | 0.975 | 1.000 | 1.000 | 1.000 | 1.030 | 1.000 |
| W14x370 | 0.940 | 1.000 | 0.955 | 1.000 | 0.975 | 1.000 | 1.000 | 1.000 | 1.030 | 1.000 |
| W14x342 | 0.939 | 1.000 | 0.954 | 1.000 | 0.975 | 1.000 | 1.000 | 1.000 | 1.031 | 1.000 |
| W14x311 | 0.938 | 1.000 | 0.953 | 1.000 | 0.974 | 1.000 | 1.000 | 1.000 | 1.032 | 1.000 |
| W14x283 | 0.937 | 1.000 | 0.953 | 1.000 | 0.974 | 1.000 | 1.000 | 1.000 | 1.032 | 1.000 |
| W14x257 | 0.936 | 1.000 | 0.952 | 1.000 | 0.973 | 1.000 | 1.000 | 1.000 | 1.033 | 1.000 |
| W14x233 | 0.935 | 1.000 | 0.951 | 1.000 | 0.973 | 1.000 | 1.000 | 1.000 | 1.033 | 1.000 |
| W14x211 | 0.934 | 1.000 | 0.950 | 1.000 | 0.972 | 1.000 | 1.000 | 1.000 | 1.034 | 1.000 |
| W14x193 | 0.933 | 1.000 | 0.950 | 1.000 | 0.972 | 1.000 | 1.000 | 1.000 | 1.034 | 1.000 |
| W14x176 | 0.932 | 1.000 | 0.949 | 1.000 | 0.972 | 1.000 | 1.000 | 1.000 | 1.034 | 1.000 |
| W14x159 | 0.931 | 1.000 | 0.949 | 1.000 | 0.971 | 1.000 | 1.000 | 1.000 | 1.035 | 1.000 |
| W14x145 | 0.931 | 1.000 | 0.948 | 1.000 | 0.971 | 1.000 | 1.000 | 1.000 | 1.035 | 1.000 |
| W14x132 | 0.923 | 1.000 | 0.942 | 1.000 | 0.968 | 1.000 | 1.000 | 1.000 | 1.039 | 1.006 |
| W14x120 | 0.922 | 1.000 | 0.942 | 1.000 | 0.967 | 1.000 | 1.000 | 1.000 | 1.040 | 1.007 |
| W14x109 | 0.922 | 1.000 | 0.941 | 1.000 | 0.967 | 1.000 | 1.000 | 1.000 | 1.040 | 1.008 |
| W14x99 | 0.921 | 1.000 | 0.941 | 1.000 | 0.967 | 1.000 | 1.000 | 1.000 | 1.041 | 1.000 |
| W14x90 | 0.920 | 1.000 | 0.940 | 1.000 | 0.967 | 1.000 | 1.000 | 1.000 | 1.041 | 1.000 |
| W14x82 | 0.831 | 0.955 | 0.872 | 0.955 | 0.927 | 0.971 | 1.000 | 1.000 | 1.093 | 1.030 |
| W14x74 | 0.831 | 0.951 | 0.872 | 0.951 | 0.927 | 0.969 | 1.000 | 1.000 | 1.093 | 1.033 |
| W14x68 | 0.829 | 0.947 | 0.870 | 0.947 | 0.926 | 0.967 | 1.000 | 1.000 | 1.095 | 1.035 |
| W14x61 | 0.827 | 0.943 | 0.869 | 0.943 | 0.926 | 0.965 | 1.000 | 1.000 | 1.096 | 1.037 |
| W14x53 | 0.735 | 0.888 | 0.796 | 0.912 | 0.882 | 0.954 | 1.000 | 1.000 | 1.160 | 1.051 |
| W14x48 | 0.732 | 0.880 | 0.794 | 0.906 | 0.881 | 0.951 | 1.000 | 1.000 | 1.162 | 1.055 |
| W12x336 | 0.910 | 1.000 | 0.932 | 1.000 | 0.962 | 1.000 | 1.000 | 1.000 | 1.047 | 1.005 |
| W12x305 | 0.907 | 1.000 | 0.931 | 1.000 | 0.961 | 1.000 | 1.000 | 1.000 | 1.048 | 1.006 |
| W12x279 | 0.905 | 1.000 | 0.929 | 1.000 | 0.960 | 1.000 | 1.000 | 1.000 | 1.049 | 1.007 |
| W12x252 | 0.903 | 0.999 | 0.927 | 0.999 | 0.959 | 0.999 | 1.000 | 1.000 | 1.050 | 1.008 |
| W12x230 | 0.901 | 0.999 | 0.926 | 0.999 | 0.959 | 0.999 | 1.000 | 1.000 | 1.051 | 1.008 |
| W12x210 | 0.900 | 0.998 | 0.925 | 0.998 | 0.958 | 0.998 | 1.000 | 1.000 | 1.052 | 1.009 |
| W12x190 | 0.898 | 0.997 | 0.923 | 0.997 | 0.957 | 0.997 | 1.000 | 1.000 | 1.053 | 1.010 |
| W12x170 | 0.896 | 0.997 | 0.922 | 0.997 | 0.956 | 0.997 | 1.000 | 1.000 | 1.054 | 1.011 |
| W12x152 | 0.894 | 0.996 | 0.921 | 0.996 | 0.955 | 0.996 | 1.000 | 1.000 | 1.055 | 1.012 |
| W12x136 | 0.892 | 0.994 | 0.919 | 0.994 | 0.955 | 0.994 | 1.000 | 1.000 | 1.056 | 1.014 |
| W12x120 | 0.890 | 0.993 | 0.918 | 0.993 | 0.954 | 0.993 | 1.000 | 1.000 | 1.057 | 1.016 |
| W12x106 | 0.889 | 0.991 | 0.917 | 0.991 | 0.953 | 0.991 | 1.000 | 1.000 | 1.058 | 1.018 |
| W12x96 | 0.888 | 0.990 | 0.916 | 0.990 | 0.953 | 0.990 | 1.000 | 1.000 | 1.059 | 1.019 |
| W12x87 | 0.886 | 0.988 | 0.915 | 0.988 | 0.952 | 0.988 | 1.000 | 1.000 | 1.060 | 1.021 |
| W12x79 | 0.885 | 0.986 | 0.913 | 0.986 | 0.951 | 0.986 | 1.000 | 1.000 | 1.061 | 1.023 |
| W12x72 | 0.884 | 0.985 | 0.913 | 0.985 | 0.951 | 0.985 | 1.000 | 1.000 | 1.061 | 1.025 |
| W12x65 | 0.883 | 1.000 | 0.912 | 1.000 | 0.950 | 1.000 | 1.000 | 1.000 | 1.062 | 1.000 |
| W12x58 | 0.835 | 0.952 | 0.875 | 0.952 | 0.929 | 0.969 | 1.000 | 1.000 | 1.091 | 1.033 |
| W12x53 | 0.831 | 0.947 | 0.872 | 0.947 | 0.927 | 0.967 | 1.000 | 1.000 | 1.093 | 1.036 |
| W12x50 | 0.744 | 0.902 | 0.803 | 0.921 | 0.886 | 0.959 | 1.000 | 1.000 | 1.153 | 1.045 |
| W12x45 | 0.739 | 0.893 | 0.799 | 0.914 | 0.884 | 0.955 | 1.000 | 1.000 | 1.157 | 1.049 |
| W12x40 | 0.737 | 0.884 | 0.798 | 0.908 | 0.883 | 0.952 | 1.000 | 1.000 | 1.158 | 1.053 |
| W10x112 | 0.854 | 0.983 | 0.889 | 0.983 | 0.938 | 0.987 | 1.000 | 1.000 | 1.079 | 1.014 |
| W10x100 | 0.851 | 0.980 | 0.887 | 0.980 | 0.936 | 0.985 | 1.000 | 1.000 | 1.081 | 1.016 |
| W10x88 | 0.848 | 0.977 | 0.885 | 0.977 | 0.935 | 0.983 | 1.000 | 1.000 | 1.082 | 1.018 |
| W10x77 | 0.845 | 0.973 | 0.883 | 0.973 | 0.934 | 0.981 | 1.000 | 1.000 | 1.084 | 1.020 |
| W10x68 | 0.844 | 0.969 | 0.882 | 0.969 | 0.933 | 0.978 | 1.000 | 1.000 | 1.085 | 1.023 |
| W10x60 | 0.842 | 0.965 | 0.880 | 0.965 | 0.932 | 0.976 | 1.000 | 1.000 | 1.086 | 1.026 |
| W10x54 | 0.841 | 0.961 | 0.879 | 0.961 | 0.932 | 0.973 | 1.000 | 1.000 | 1.087 | 1.028 |
| W10x49 | 0.838 | 0.957 | 0.878 | 0.957 | 0.931 | 0.971 | 1.000 | 1.000 | 1.089 | 1.031 |
| W10x45 | 0.755 | 0.918 | 0.812 | 0.932 | 0.892 | 0.965 | 1.000 | 1.000 | 1.145 | 1.038 |
| W10x39 | 0.748 | 0.906 | 0.807 | 0.923 | 0.889 | 0.960 | 1.000 | 1.000 | 1.150 | 1.044 |
| W10x33 | 0.739 | 0.889 | 0.799 | 0.911 | 0.884 | 0.954 | 1.000 | 1.000 | 1.157 | 1.051 |
| W8x67 | 0.776 | 0.959 | 0.829 | 0.964 | 0.902 | 0.981 | 1.000 | 1.000 | 1.130 | 1.019 |
| W8x58 | 0.773 | 0.953 | 0.826 | 0.958 | 0.900 | 0.979 | 1.000 | 1.000 | 1.132 | 1.022 |
| W8x48 | 0.769 | 0.943 | 0.823 | 0.950 | 0.898 | 0.974 | 1.000 | 1.000 | 1.135 | 1.027 |
| W8x40 | 0.761 | 0.929 | 0.817 | 0.940 | 0.895 | 0.969 | 1.000 | 1.000 | 1.141 | 1.033 |
| W8x35 | 0.759 | 0.920 | 0.815 | 0.933 | 0.894 | 0.965 | 1.000 | 1.000 | 1.142 | 1.037 |
| W8x31 | 0.757 | 0.912 | 0.813 | 0.926 | 0.893 | 0.962 | 1.000 | 1.000 | 1.144 | 1.042 |
| W8x28 | 0.648 | 0.869 | 0.725 | 0.909 | 0.838 | 0.952 | 1.000 | 1.000 | 1.232 | 1.053 |
| W8x24 | 0.645 | 0.854 | 0.723 | 0.897 | 0.836 | 0.946 | 1.000 | 1.000 | 1.235 | 1.061 |
| W6x25 | 0.611 | 0.886 | 0.694 | 0.921 | 0.818 | 0.959 | 1.000 | 1.000 | 1.267 | 1.045 |
| W6x20 | 0.603 | 0.862 | 0.688 | 0.903 | 0.814 | 0.949 | 1.000 | 1.000 | 1.275 | 1.057 |

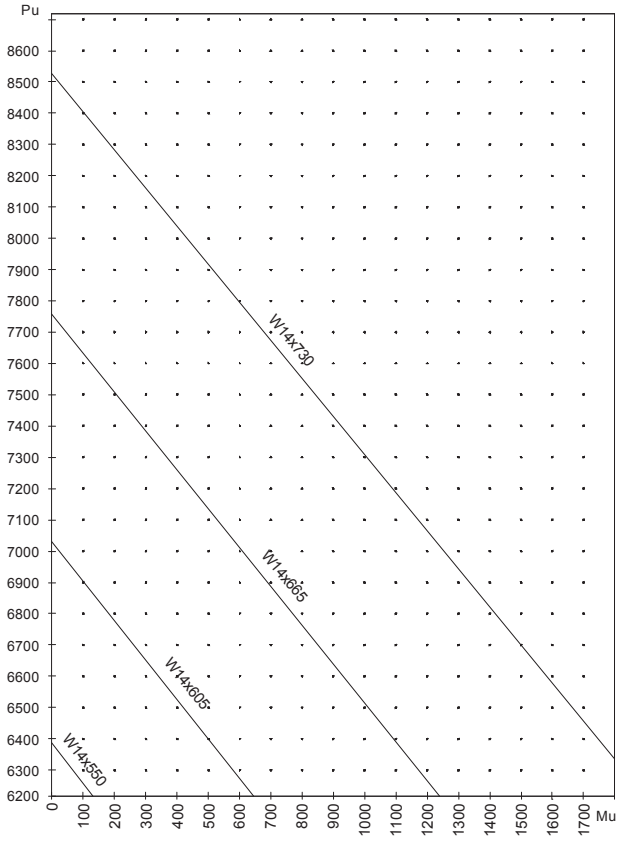
## APPENDIX C—$B_{KL}$ AND $B_{LM}$ VALUES (50 ksi) (cont'd)

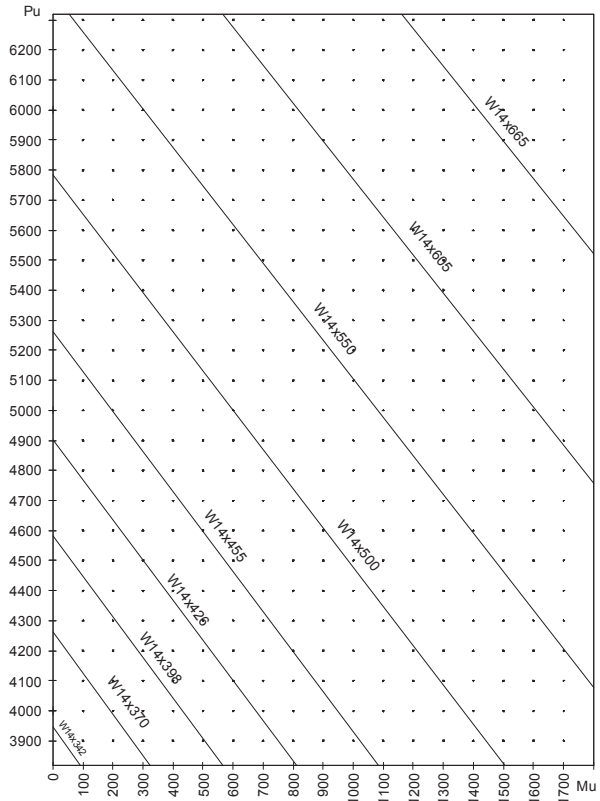
| | $B_{KL}$ and $B_{LM}$ Values (50 ksi) | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| | KL (ft) | | | | | | | | | |
| | 6.00 | | 8.00 | | 10.00 | | 12.00 | | 14.00 | |
| Shape | $B_{KL}$ | $B_{LM}$ | $B_{KL}$ | $B_{LM}$ | $B_{KL}$ | $B_{LM}$ | $B_{KL}$ | $B_{LM}$ | $B_{KL}$ | $B_{LM}$ |
| W14x730 | 0.950 | 1.000 | 0.962 | 1.000 | 0.979 | 1.000 | 1.000 | 1.000 | 1.025 | 1.000 |
| W14x665 | 0.948 | 1.000 | 0.961 | 1.000 | 0.979 | 1.000 | 1.000 | 1.000 | 1.026 | 1.000 |
| W14x605 | 0.947 | 1.000 | 0.960 | 1.000 | 0.978 | 1.000 | 1.000 | 1.000 | 1.027 | 1.000 |
| W14x550 | 0.945 | 1.000 | 0.959 | 1.000 | 0.977 | 1.000 | 1.000 | 1.000 | 1.028 | 1.000 |
| W14x500 | 0.944 | 1.000 | 0.958 | 1.000 | 0.977 | 1.000 | 1.000 | 1.000 | 1.028 | 1.000 |
| W14x455 | 0.942 | 1.000 | 0.957 | 1.000 | 0.976 | 1.000 | 1.000 | 1.000 | 1.029 | 1.000 |
| W14x426 | 0.941 | 1.000 | 0.956 | 1.000 | 0.976 | 1.000 | 1.000 | 1.000 | 1.029 | 1.000 |
| W14x398 | 0.941 | 1.000 | 0.956 | 1.000 | 0.975 | 1.000 | 1.000 | 1.000 | 1.030 | 1.000 |
| W14x370 | 0.940 | 1.000 | 0.955 | 1.000 | 0.975 | 1.000 | 1.000 | 1.000 | 1.030 | 1.000 |
| W14x342 | 0.939 | 1.000 | 0.954 | 1.000 | 0.975 | 1.000 | 1.000 | 1.000 | 1.031 | 1.000 |
| W14x311 | 0.938 | 1.000 | 0.953 | 1.000 | 0.974 | 1.000 | 1.000 | 1.000 | 1.032 | 1.000 |
| W14x283 | 0.937 | 1.000 | 0.953 | 1.000 | 0.974 | 1.000 | 1.000 | 1.000 | 1.032 | 1.000 |
| W14x257 | 0.936 | 1.000 | 0.952 | 1.000 | 0.973 | 1.000 | 1.000 | 1.000 | 1.033 | 1.000 |
| W14x233 | 0.935 | 1.000 | 0.951 | 1.000 | 0.973 | 1.000 | 1.000 | 1.000 | 1.033 | 1.000 |
| W14x211 | 0.934 | 1.000 | 0.950 | 1.000 | 0.972 | 1.000 | 1.000 | 1.000 | 1.034 | 1.000 |
| W14x193 | 0.933 | 1.000 | 0.950 | 1.000 | 0.972 | 1.000 | 1.000 | 1.000 | 1.034 | 1.000 |
| W14x176 | 0.932 | 1.000 | 0.949 | 1.000 | 0.972 | 1.000 | 1.000 | 1.000 | 1.034 | 1.000 |
| W14x159 | 0.931 | 1.000 | 0.949 | 1.000 | 0.971 | 1.000 | 1.000 | 1.000 | 1.035 | 1.000 |
| W14x145 | 0.931 | 1.000 | 0.948 | 1.000 | 0.971 | 1.000 | 1.000 | 1.000 | 1.035 | 1.000 |
| W14x132 | 0.923 | 1.000 | 0.942 | 1.000 | 0.968 | 1.000 | 1.000 | 1.000 | 1.039 | 1.006 |
| W14x120 | 0.922 | 1.000 | 0.942 | 1.000 | 0.967 | 1.000 | 1.000 | 1.000 | 1.040 | 1.007 |
| W14x109 | 0.922 | 1.000 | 0.941 | 1.000 | 0.967 | 1.000 | 1.000 | 1.000 | 1.040 | 1.008 |
| W14x99 | 0.921 | 1.000 | 0.941 | 1.000 | 0.967 | 1.000 | 1.000 | 1.000 | 1.041 | 1.000 |
| W14x90 | 0.920 | 1.000 | 0.940 | 1.000 | 0.967 | 1.000 | 1.000 | 1.000 | 1.041 | 1.000 |
| W14x82 | 0.831 | 0.955 | 0.872 | 0.955 | 0.927 | 0.971 | 1.000 | 1.000 | 1.093 | 1.030 |
| W14x74 | 0.831 | 0.951 | 0.872 | 0.951 | 0.927 | 0.969 | 1.000 | 1.000 | 1.093 | 1.033 |
| W14x68 | 0.829 | 0.947 | 0.870 | 0.947 | 0.926 | 0.967 | 1.000 | 1.000 | 1.095 | 1.035 |
| W14x61 | 0.827 | 0.943 | 0.869 | 0.943 | 0.926 | 0.965 | 1.000 | 1.000 | 1.096 | 1.037 |
| W14x53 | 0.735 | 0.888 | 0.796 | 0.912 | 0.882 | 0.954 | 1.000 | 1.000 | 1.160 | 1.051 |
| W14x48 | 0.732 | 0.880 | 0.794 | 0.906 | 0.881 | 0.951 | 1.000 | 1.000 | 1.162 | 1.055 |
| W12x336 | 0.910 | 1.000 | 0.932 | 1.000 | 0.962 | 1.000 | 1.000 | 1.000 | 1.047 | 1.005 |
| W12x305 | 0.907 | 1.000 | 0.931 | 1.000 | 0.961 | 1.000 | 1.000 | 1.000 | 1.048 | 1.006 |
| W12x279 | 0.905 | 1.000 | 0.929 | 1.000 | 0.960 | 1.000 | 1.000 | 1.000 | 1.049 | 1.007 |
| W12x252 | 0.903 | 0.999 | 0.927 | 0.999 | 0.959 | 0.999 | 1.000 | 1.000 | 1.050 | 1.008 |
| W12x230 | 0.901 | 0.999 | 0.926 | 0.999 | 0.959 | 0.999 | 1.000 | 1.000 | 1.051 | 1.008 |
| W12x210 | 0.900 | 0.998 | 0.925 | 0.998 | 0.958 | 0.998 | 1.000 | 1.000 | 1.052 | 1.009 |
| W12x190 | 0.898 | 0.997 | 0.923 | 0.997 | 0.957 | 0.997 | 1.000 | 1.000 | 1.053 | 1.010 |
| W12x170 | 0.896 | 0.997 | 0.922 | 0.997 | 0.956 | 0.997 | 1.000 | 1.000 | 1.054 | 1.011 |
| W12x152 | 0.894 | 0.996 | 0.921 | 0.996 | 0.955 | 0.996 | 1.000 | 1.000 | 1.055 | 1.012 |
| W12x136 | 0.892 | 0.994 | 0.919 | 0.994 | 0.955 | 0.994 | 1.000 | 1.000 | 1.056 | 1.014 |
| W12x120 | 0.890 | 0.993 | 0.918 | 0.993 | 0.954 | 0.993 | 1.000 | 1.000 | 1.057 | 1.016 |
| W12x106 | 0.889 | 0.991 | 0.917 | 0.991 | 0.953 | 0.991 | 1.000 | 1.000 | 1.058 | 1.018 |
| W12x96 | 0.888 | 0.990 | 0.916 | 0.990 | 0.953 | 0.990 | 1.000 | 1.000 | 1.059 | 1.019 |
| W12x87 | 0.886 | 0.988 | 0.915 | 0.988 | 0.952 | 0.988 | 1.000 | 1.000 | 1.060 | 1.021 |
| W12x79 | 0.885 | 0.986 | 0.913 | 0.986 | 0.951 | 0.986 | 1.000 | 1.000 | 1.061 | 1.023 |
| W12x72 | 0.884 | 0.985 | 0.913 | 0.985 | 0.951 | 0.985 | 1.000 | 1.000 | 1.061 | 1.025 |
| W12x65 | 0.883 | 1.000 | 0.912 | 1.000 | 0.950 | 1.000 | 1.000 | 1.000 | 1.062 | 1.000 |
| W12x58 | 0.835 | 0.952 | 0.875 | 0.952 | 0.929 | 0.969 | 1.000 | 1.000 | 1.091 | 1.033 |
| W12x53 | 0.831 | 0.947 | 0.872 | 0.947 | 0.927 | 0.967 | 1.000 | 1.000 | 1.093 | 1.036 |
| W12x50 | 0.744 | 0.902 | 0.803 | 0.921 | 0.886 | 0.959 | 1.000 | 1.000 | 1.153 | 1.045 |
| W12x45 | 0.739 | 0.893 | 0.799 | 0.914 | 0.884 | 0.955 | 1.000 | 1.000 | 1.157 | 1.049 |
| W12x40 | 0.737 | 0.884 | 0.798 | 0.908 | 0.883 | 0.952 | 1.000 | 1.000 | 1.158 | 1.053 |
| W10x112 | 0.854 | 0.983 | 0.889 | 0.983 | 0.938 | 0.987 | 1.000 | 1.000 | 1.079 | 1.014 |
| W10x100 | 0.851 | 0.980 | 0.887 | 0.980 | 0.936 | 0.985 | 1.000 | 1.000 | 1.081 | 1.016 |
| W10x88 | 0.848 | 0.977 | 0.885 | 0.977 | 0.935 | 0.983 | 1.000 | 1.000 | 1.082 | 1.018 |
| W10x77 | 0.845 | 0.973 | 0.883 | 0.973 | 0.934 | 0.981 | 1.000 | 1.000 | 1.084 | 1.020 |
| W10x68 | 0.844 | 0.969 | 0.882 | 0.969 | 0.933 | 0.978 | 1.000 | 1.000 | 1.085 | 1.023 |
| W10x60 | 0.842 | 0.965 | 0.880 | 0.965 | 0.932 | 0.976 | 1.000 | 1.000 | 1.086 | 1.026 |
| W10x54 | 0.841 | 0.961 | 0.879 | 0.961 | 0.932 | 0.973 | 1.000 | 1.000 | 1.087 | 1.028 |
| W10x49 | 0.838 | 0.957 | 0.878 | 0.957 | 0.931 | 0.971 | 1.000 | 1.000 | 1.089 | 1.031 |
| W10x45 | 0.755 | 0.918 | 0.812 | 0.932 | 0.892 | 0.965 | 1.000 | 1.000 | 1.145 | 1.038 |
| W10x39 | 0.748 | 0.906 | 0.807 | 0.923 | 0.889 | 0.960 | 1.000 | 1.000 | 1.150 | 1.044 |
| W10x33 | 0.739 | 0.889 | 0.799 | 0.911 | 0.884 | 0.954 | 1.000 | 1.000 | 1.157 | 1.051 |
| W8x67 | 0.776 | 0.959 | 0.829 | 0.964 | 0.902 | 0.981 | 1.000 | 1.000 | 1.130 | 1.019 |
| W8x58 | 0.773 | 0.953 | 0.826 | 0.958 | 0.900 | 0.979 | 1.000 | 1.000 | 1.132 | 1.022 |
| W8x48 | 0.769 | 0.943 | 0.823 | 0.950 | 0.898 | 0.974 | 1.000 | 1.000 | 1.135 | 1.027 |
| W8x40 | 0.761 | 0.929 | 0.817 | 0.940 | 0.895 | 0.969 | 1.000 | 1.000 | 1.141 | 1.033 |
| W8x35 | 0.759 | 0.920 | 0.815 | 0.933 | 0.894 | 0.965 | 1.000 | 1.000 | 1.142 | 1.037 |
| W8x31 | 0.757 | 0.912 | 0.813 | 0.926 | 0.893 | 0.962 | 1.000 | 1.000 | 1.144 | 1.042 |
| W8x28 | 0.648 | 0.869 | 0.725 | 0.909 | 0.838 | 0.952 | 1.000 | 1.000 | 1.232 | 1.053 |
| W8x24 | 0.645 | 0.854 | 0.723 | 0.897 | 0.836 | 0.946 | 1.000 | 1.000 | 1.235 | 1.061 |
| W8x25 | 0.611 | 0.886 | 0.694 | 0.921 | 0.818 | 0.959 | 1.000 | 1.000 | 1.267 | 1.045 |
| W8x20 | 0.603 | 0.862 | 0.688 | 0.903 | 0.814 | 0.949 | 1.000 | 1.000 | 1.275 | 1.057 |

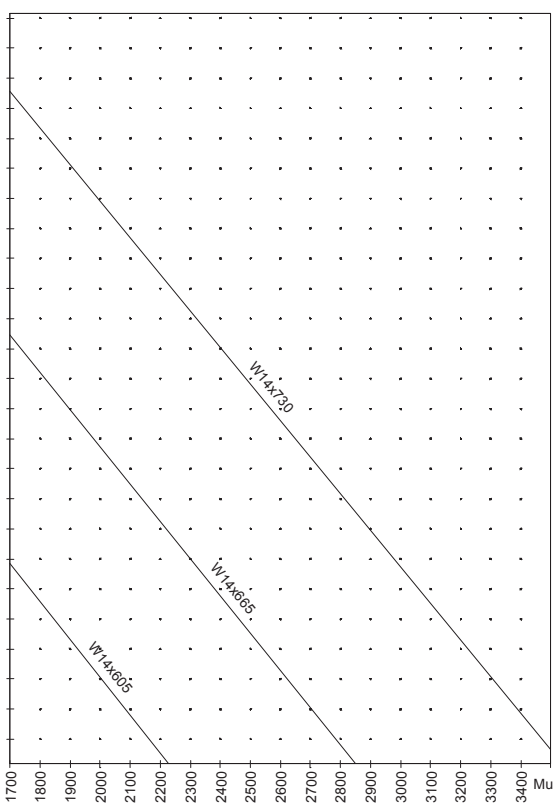
## APPENDIX C—$B_{KL}$ AND $B_{LM}$ VALUES (50 ksi) (cont'd)

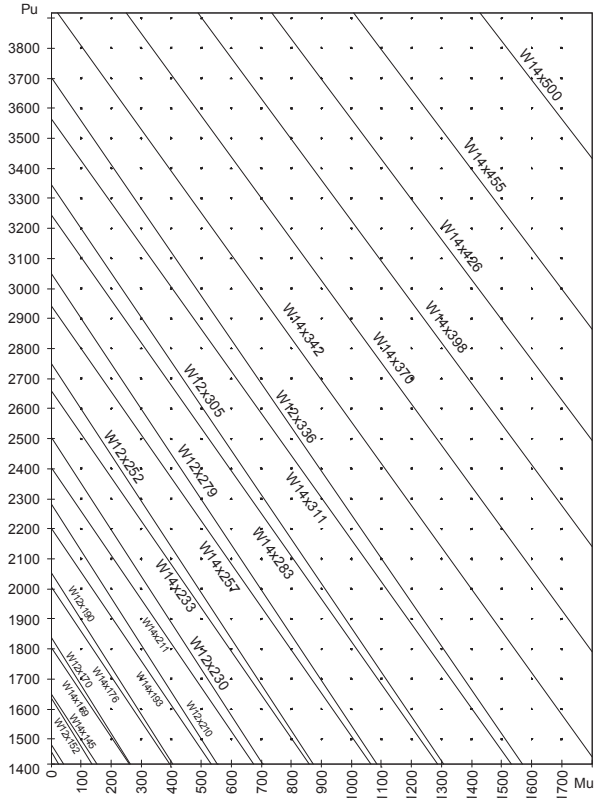
| | $B_{KL}$ and $B_{LM}$ Values (50 ksi) | | | |
|---|---|---|---|---|
| | $KL$ (ft) | | | |
| | 36.00 | | 38.00 | |
| Shape | $B_{KL}$ | $B_{LM}$ | $B_{KL}$ | $B_{LM}$ |
| W14x730 | 1.736 | 1.034 | 1.863 | 1.038 |
| W14x665 | 1.765 | 1.038 | 1.899 | 1.042 |
| W14x605 | 1.797 | 1.041 | 1.937 | 1.045 |
| W14x550 | 1.825 | 1.045 | 1.972 | 1.050 |
| W14x500 | 1.855 | 1.050 | 2.009 | 1.055 |
| W14x455 | 1.882 | 1.054 | 2.041 | 1.059 |
| W14x426 | 1.904 | 1.058 | 2.068 | 1.064 |
| W14x398 | 1.921 | 1.062 | 2.089 | 1.068 |
| W14x370 | 1.945 | 1.066 | 2.118 | 1.073 |
| W14x342 | 1.963 | 1.071 | 2.141 | 1.079 |
| W14x311 | 1.989 | 1.079 | 2.173 | 1.087 |
| W14x283 | 2.009 | 1.087 | 2.197 | 1.096 |
| W14x257 | 2.036 | 1.097 | 2.231 | 1.107 |
| W14x233 | 2.058 | 1.108 | 2.257 | 1.119 |
| W14x211 | 2.080 | 1.120 | 2.285 | 1.133 |
| W14x193 | 2.095 | 1.133 | 2.304 | 1.147 |
| W14x176 | 2.118 | 1.148 | 2.333 | 1.164 |
| W14x159 | 2.134 | 1.166 | 2.355 | 1.184 |
| W14x145 | 2.151 | 1.183 | 2.376 | 1.203 |
| W14x132 | 2.362 | 1.217 | 2.632 | 1.241 |
| W14x120 | 2.385 | 1.243 | 2.657 | 1.270 |
| W14x109 | 2.396 | 1.269 | 2.670 | 1.300 |
| W14x99 | 2.419 | 1.000 | 2.695 | 1.000 |
| W14x90 | 2.431 | 1.000 | 2.708 | 1.000 |
| W14x82 | 4.724 | 1.699 | 5.263 | 1.807 |
| W14x74 | 4.724 | 1.820 | 5.263 | 1.938 |
| W14x68 | 4.781 | 1.949 | 5.328 | 2.078 |
| W14x61 | 4.811 | 2.103 | 5.360 | 2.246 |
| W14x53 | 6.684 | 2.575 | 7.447 | 2.739 |
| W14x48 | 6.725 | 2.767 | 7.493 | 2.947 |
| W12x336 | 2.722 | 1.077 | 3.033 | 1.084 |
| W12x305 | 2.792 | 1.085 | 3.111 | 1.093 |
| W12x279 | 2.850 | 1.093 | 3.175 | 1.101 |
| W12x252 | 2.909 | 1.103 | 3.241 | 1.112 |
| W12x230 | 2.955 | 1.111 | 3.292 | 1.122 |
| W12x210 | 3.001 | 1.122 | 3.344 | 1.134 |
| W12x190 | 3.049 | 1.136 | 3.397 | 1.149 |
| W12x170 | 3.098 | 1.153 | 3.451 | 1.167 |
| W12x152 | 3.147 | 1.174 | 3.507 | 1.191 |
| W12x136 | 3.198 | 1.198 | 3.564 | 1.218 |
| W12x120 | 3.250 | 1.228 | 3.622 | 1.252 |
| W12x106 | 3.286 | 1.265 | 3.661 | 1.293 |
| W12x96 | 3.322 | 1.297 | 3.701 | 1.330 |
| W12x87 | 3.358 | 1.336 | 3.742 | 1.374 |
| W12x79 | 3.395 | 1.386 | 3.783 | 1.479 |
| W12x72 | 3.414 | 1.487 | 3.804 | 1.589 |
| W12x65 | 3.452 | 1.598 | 3.846 | 1.710 |
| W12x58 | 4.638 | 1.882 | 5.168 | 2.006 |
| W12x53 | 4.724 | 2.021 | 5.263 | 2.158 |
| W12x50 | 6.521 | 2.318 | 7.266 | 2.463 |
| W12x45 | 6.602 | 2.519 | 7.356 | 2.679 |
| W12x40 | 6.643 | 2.736 | 7.401 | 2.913 |
| W10x112 | 4.191 | 1.195 | 4.669 | 1.215 |
| W10x100 | 4.266 | 1.225 | 4.753 | 1.249 |
| W10x88 | 4.317 | 1.262 | 4.809 | 1.290 |
| W10x77 | 4.394 | 1.312 | 4.896 | 1.347 |
| W10x68 | 4.421 | 1.365 | 4.925 | 1.449 |
| W10x60 | 4.474 | 1.509 | 4.985 | 1.603 |
| W10x54 | 4.501 | 1.640 | 5.015 | 1.744 |
| W10x49 | 4.555 | 1.769 | 5.075 | 1.884 |
| W10x45 | 6.322 | 2.029 | 7.044 | 2.153 |
| W10x39 | 6.441 | 2.281 | 7.177 | 2.423 |
| W10x33 | 6.602 | 2.628 | 7.356 | 2.797 |
| W8x67 | 5.903 | 1.293 | 6.577 | 1.325 |
| W8x58 | 5.977 | 1.353 | 6.660 | 1.414 |
| W8x48 | 6.052 | 1.562 | 6.743 | 1.653 |
| W8x40 | 6.205 | 1.832 | 6.914 | 1.942 |
| W8x35 | 6.244 | 2.024 | 6.957 | 2.148 |
| W8x31 | 6.283 | 2.215 | 7.000 | 2.352 |
| W8x28 | 7.949 | 2.521 | 8.857 | 2.671 |
| W8x24 | 7.990 | 2.814 | 8.903 | 2.985 |
| W8x25 | 8.347 | 2.210 | 9.301 | 2.337 |
| W8x20 | 8.422 | 2.622 | 9.384 | 2.776 |

## APPENDIX D—STANDARD GRAPHS OF INTERACTION DIAGRAMS
## ($P_u$ in kips, $M_u$ in kip-ft)

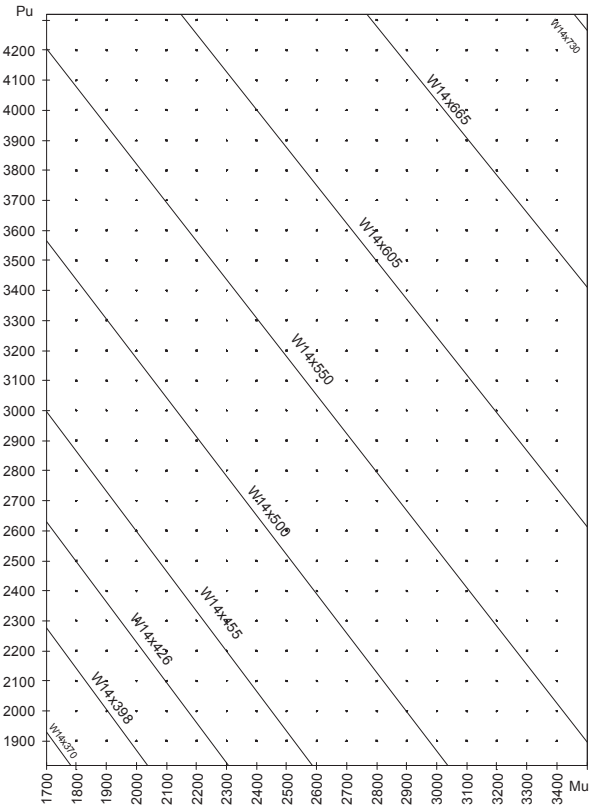


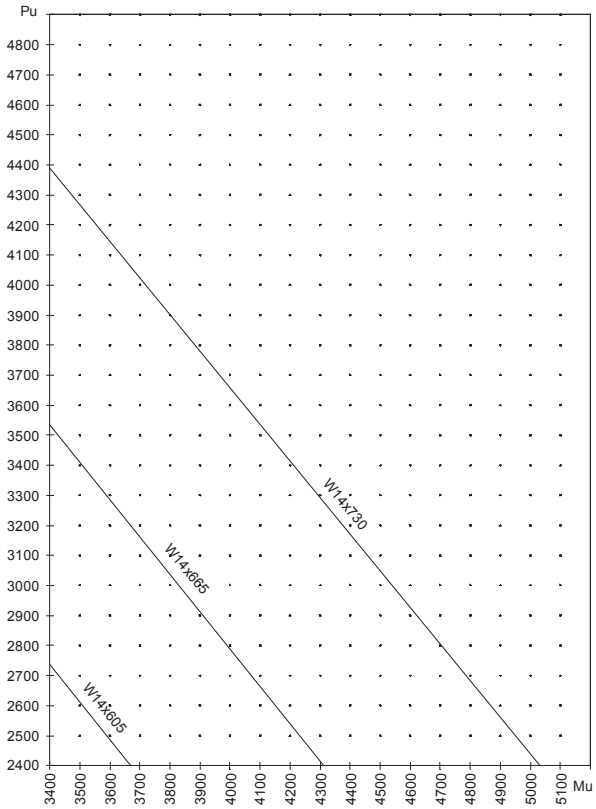



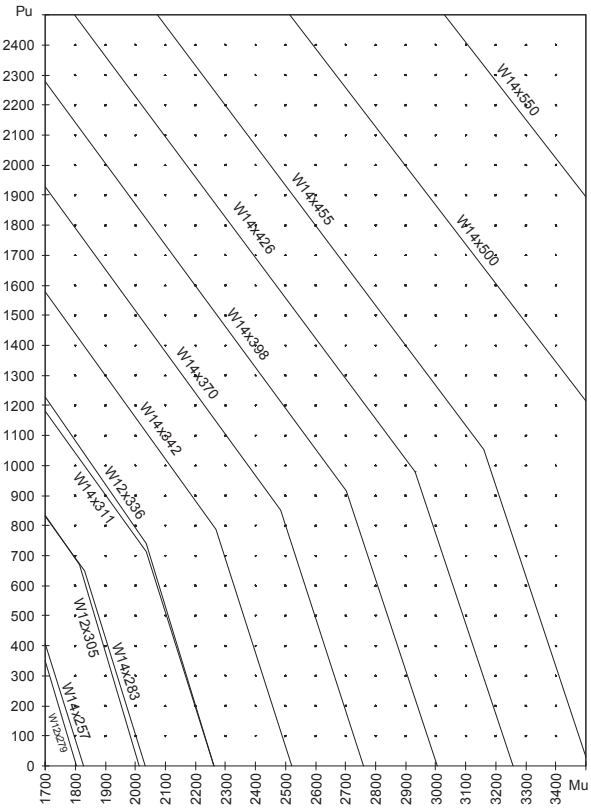



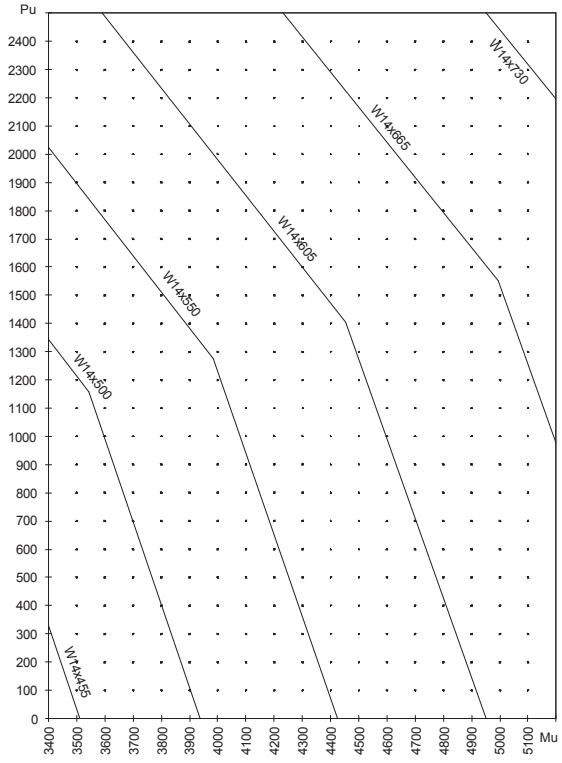



## APPENDIX D—STANDARD GRAPHS OF INTERACTION DIAGRAMS (cont'd)
## ($P_u$ in kips, $M_u$ in kip-ft)

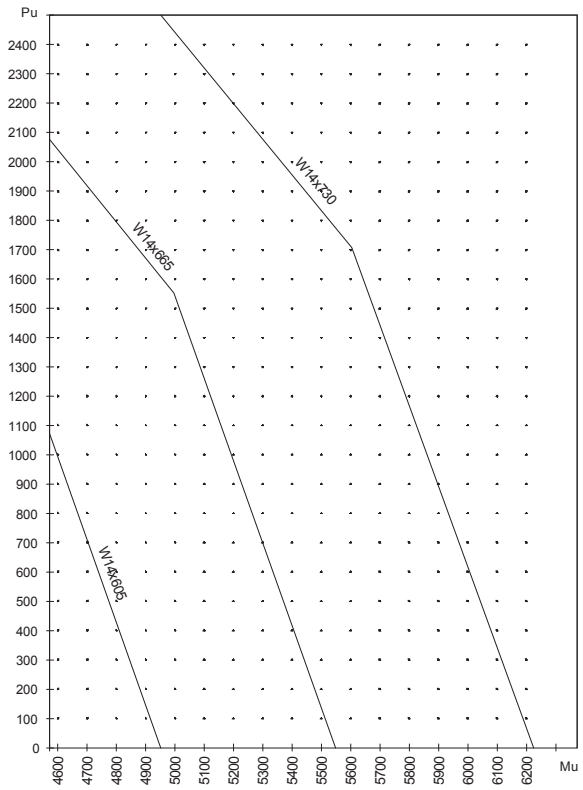


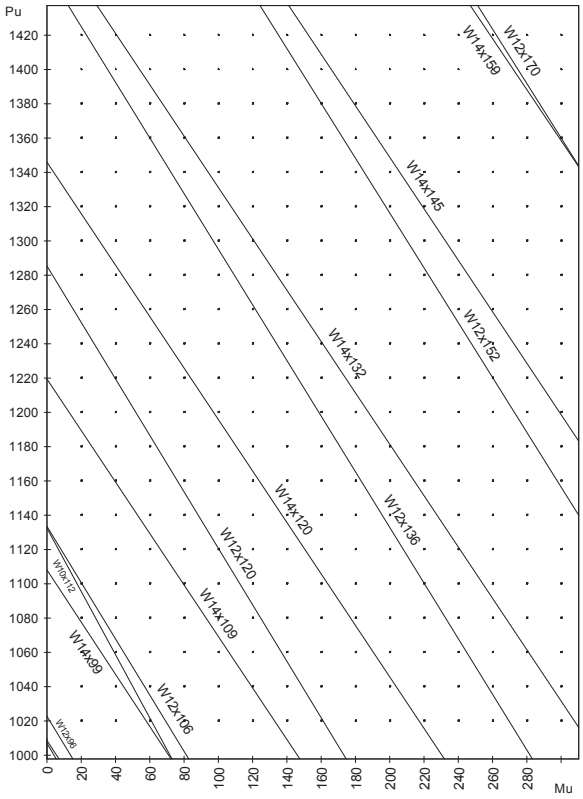



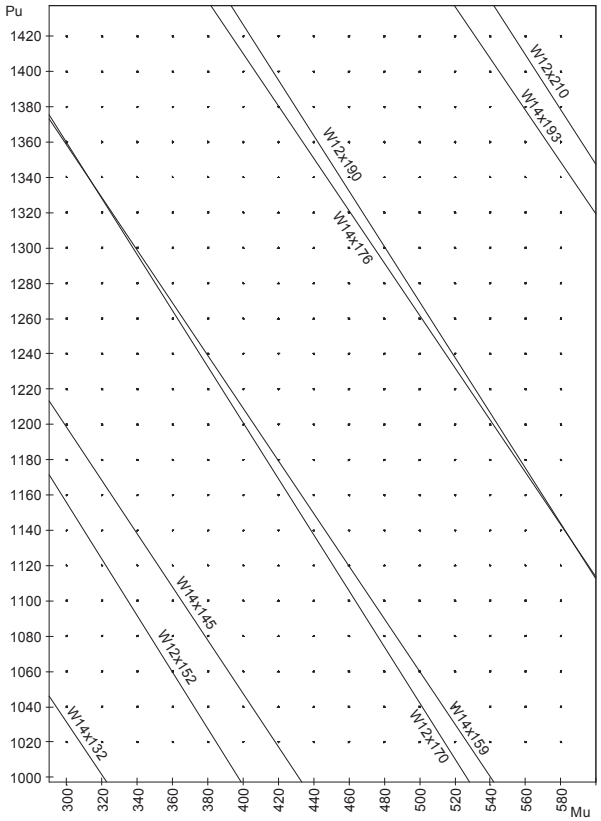



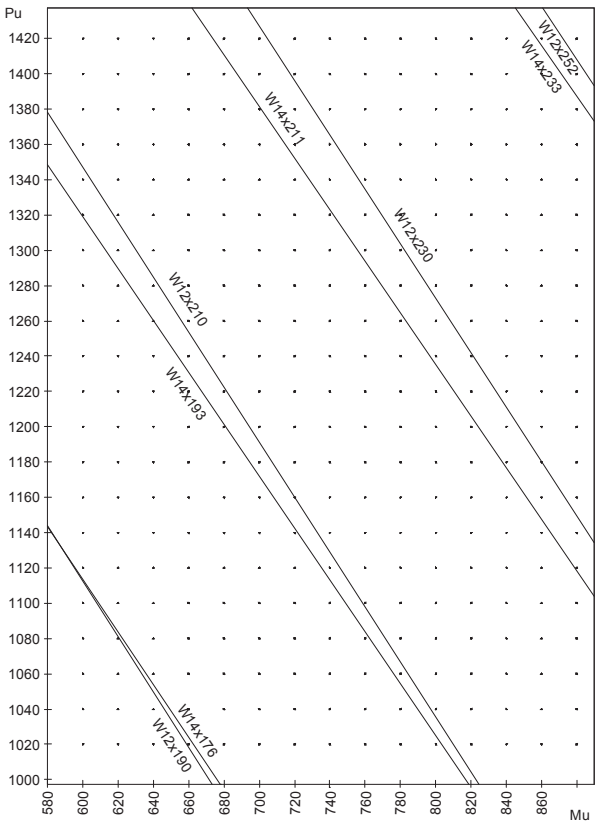



## APPENDIX D—STANDARD GRAPHS OF INTERACTION DIAGRAMS (cont'd)
## ($P_u$ in kips, $M_u$ in kip-ft)

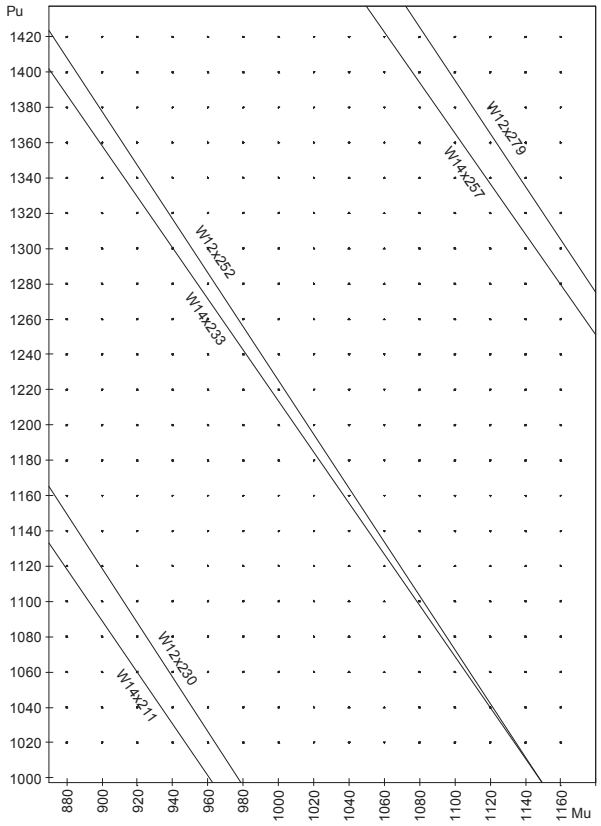


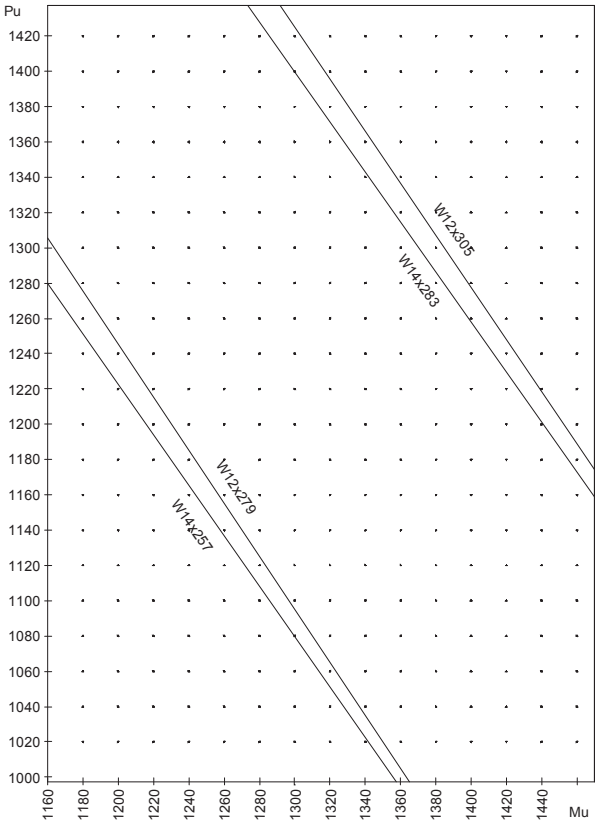



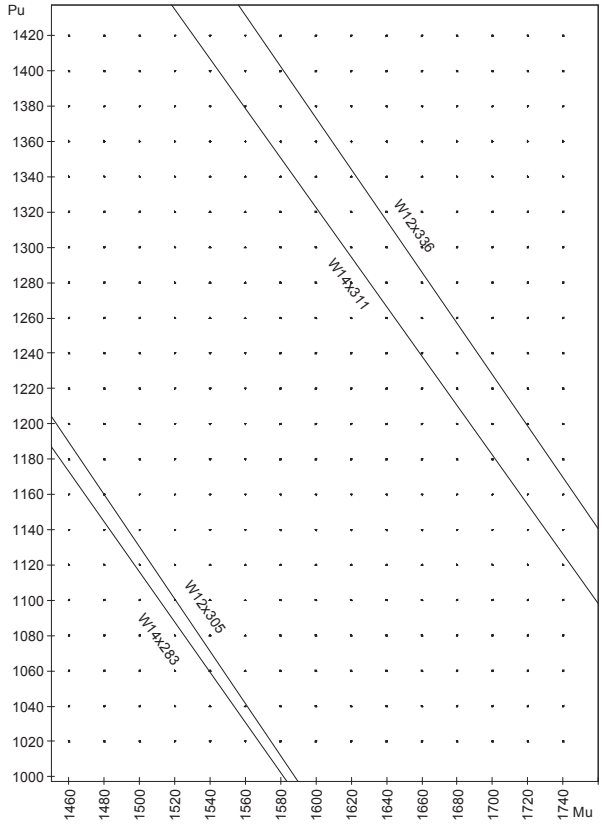



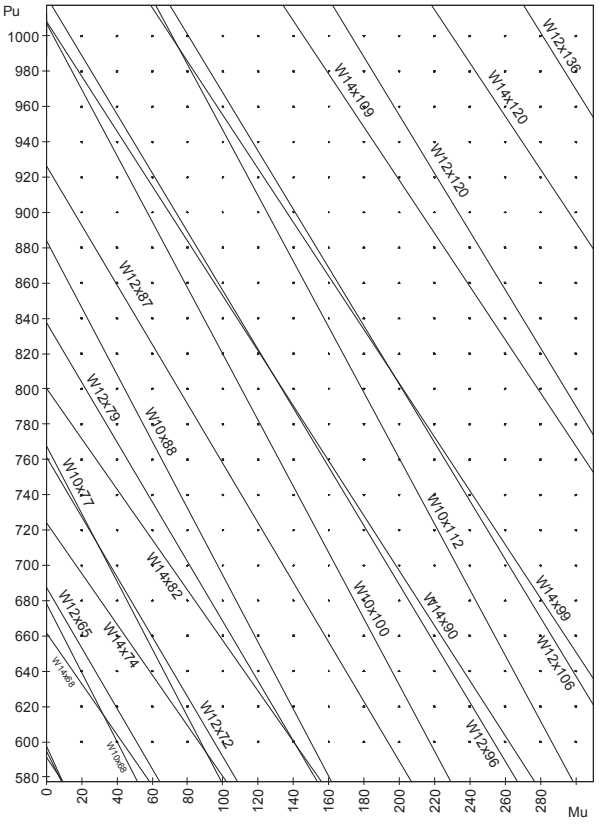



## APPENDIX D—STANDARD GRAPHS OF INTERACTION DIAGRAMS (cont'd)
## ($P_u$ in kips, $M_u$ in kip-ft)

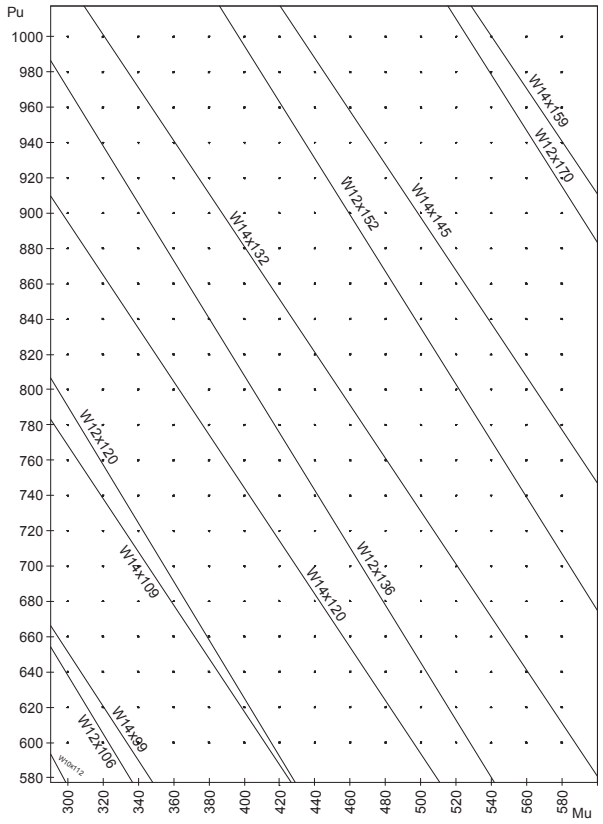


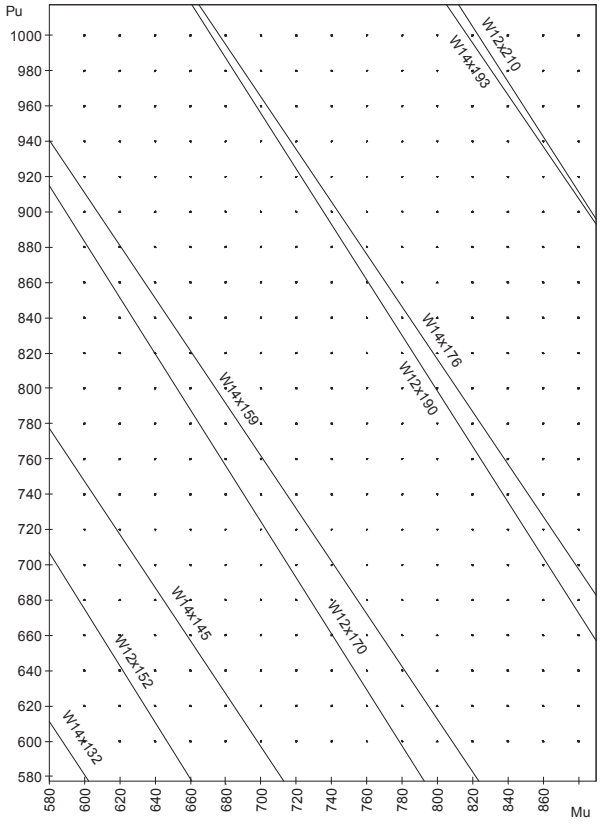



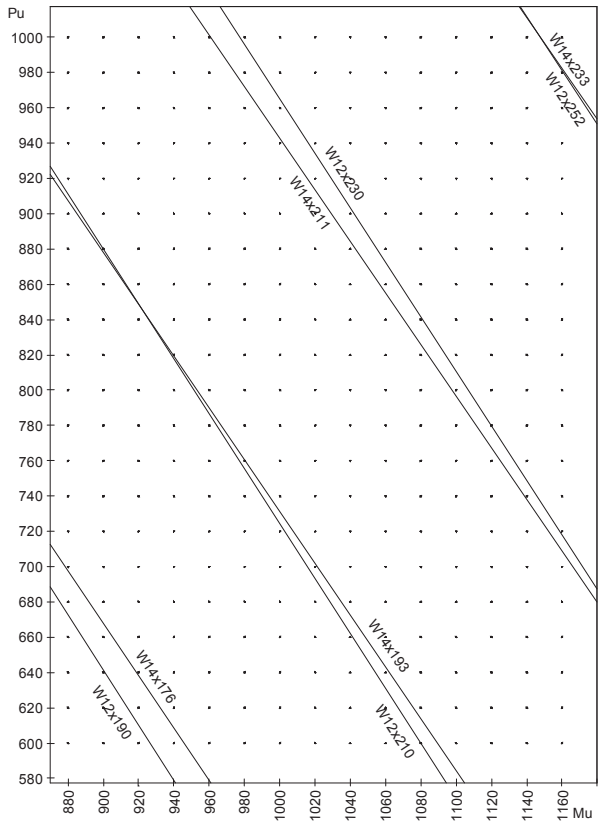



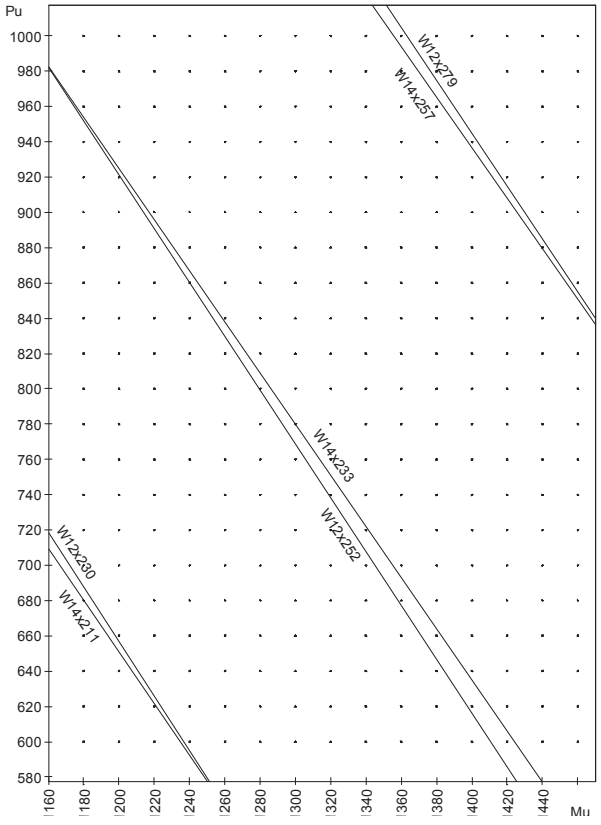



## APPENDIX D—STANDARD GRAPHS OF INTERACTION DIAGRAMS (cont'd)
## ($P_u$ in kips, $M_u$ in kip-ft)

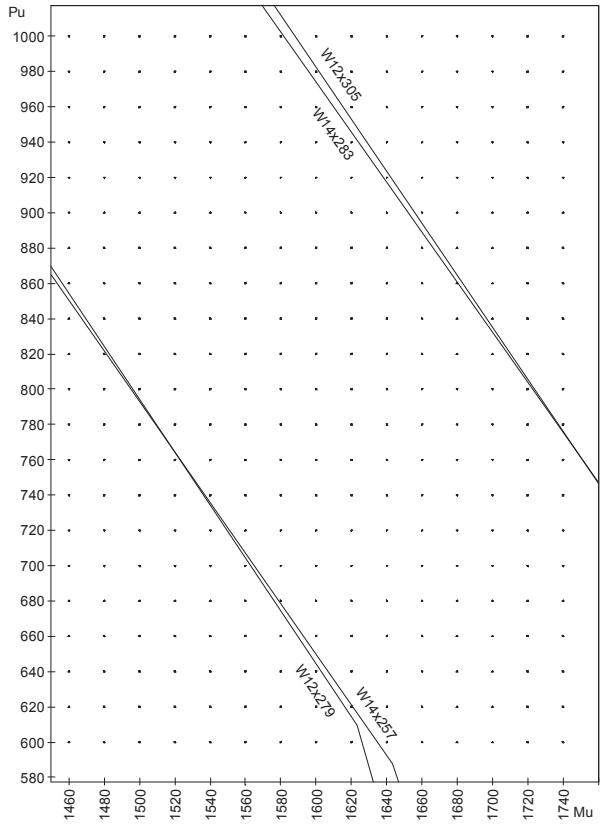


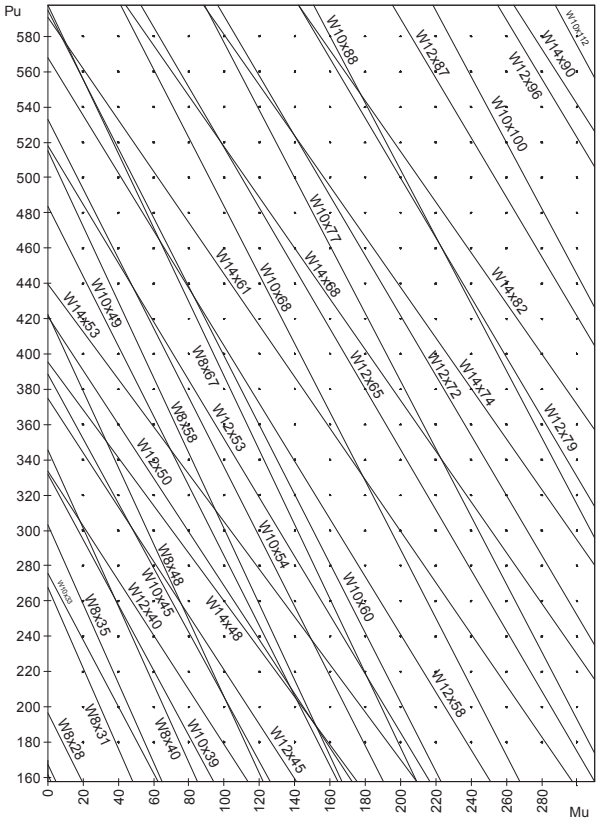



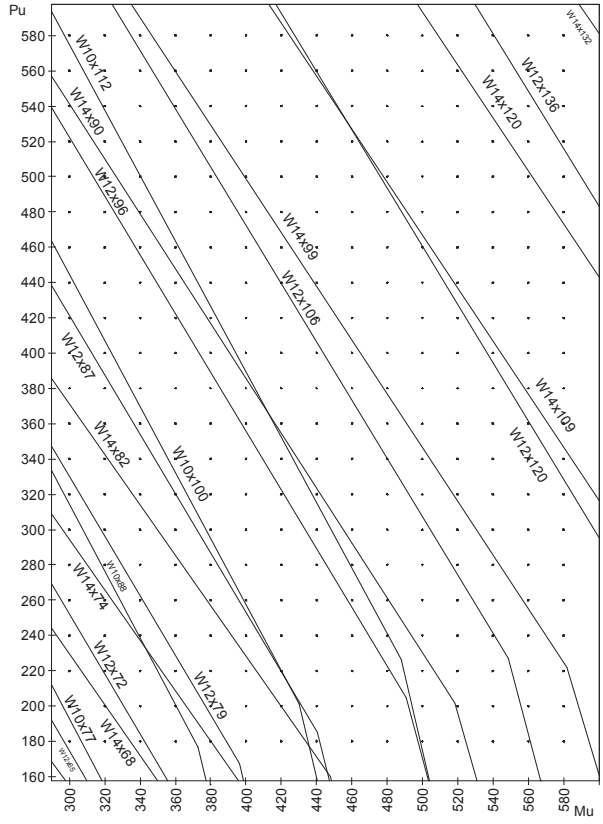



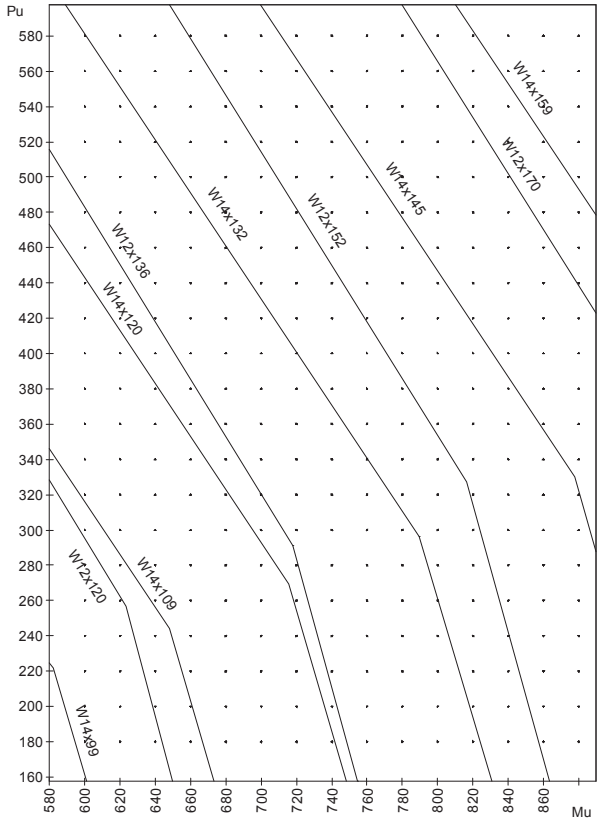



## APPENDIX D—STANDARD GRAPHS OF INTERACTION DIAGRAMS (cont'd)
## ($P_u$ in kips, $M_u$ in kip-ft)

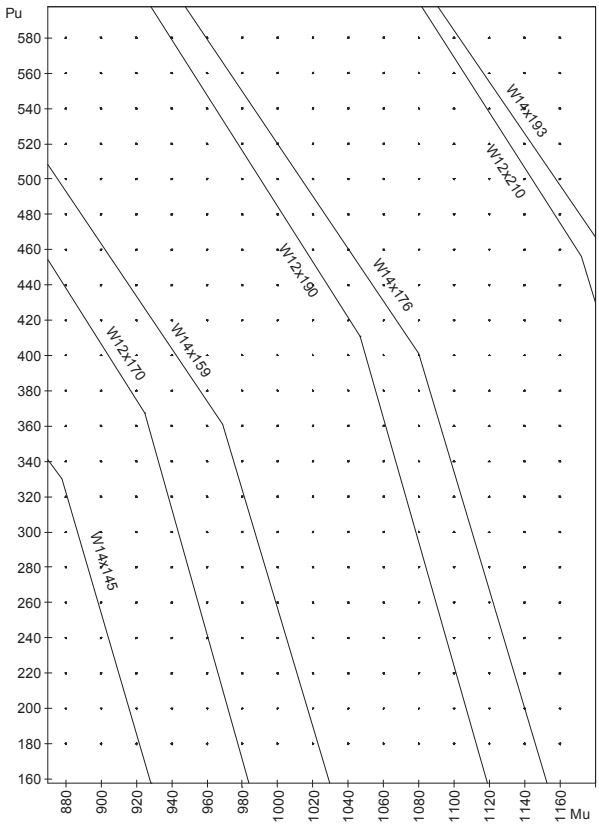


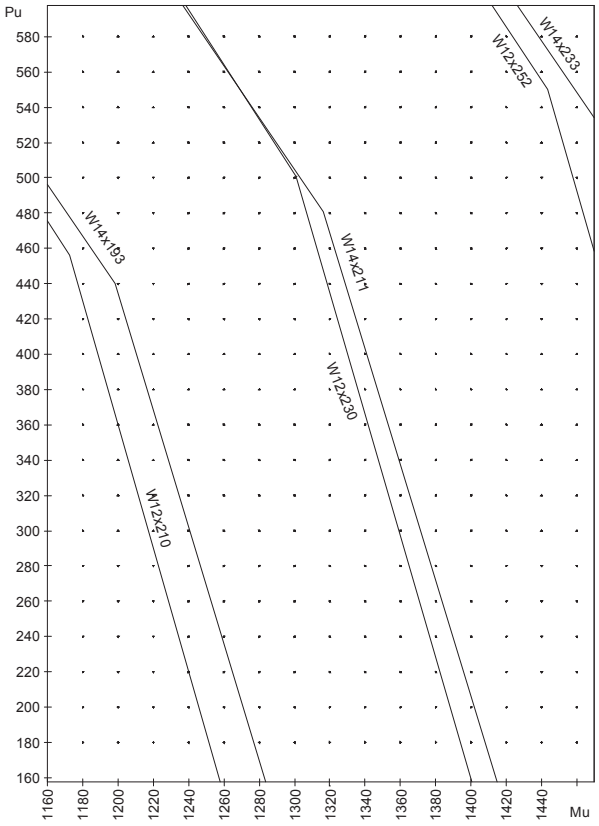



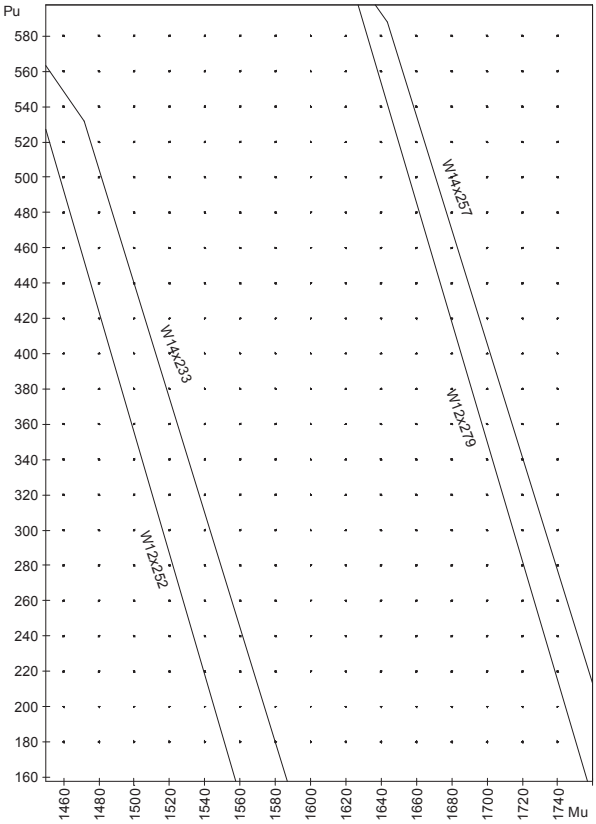



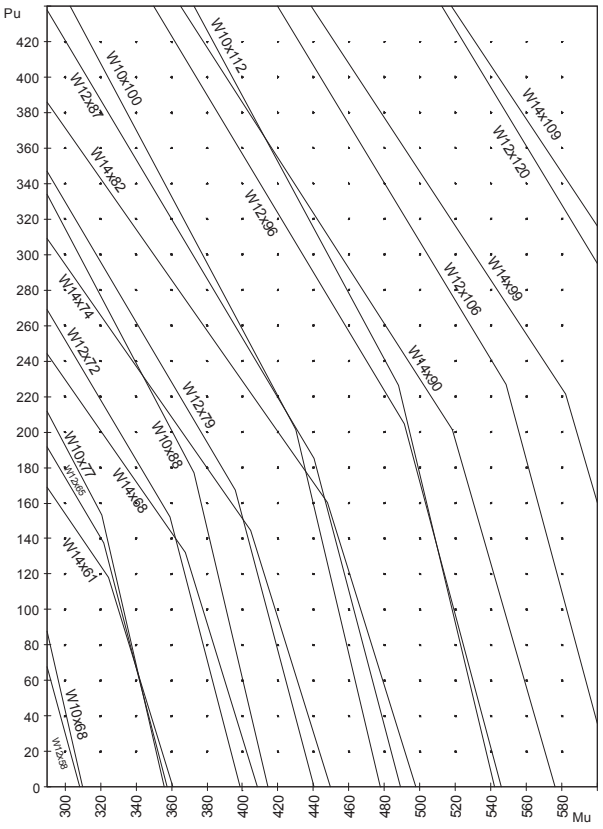



## APPENDIX D—STANDARD GRAPHS OF INTERACTION DIAGRAMS (cont'd)
## ($P_u$ in kips, $M_u$ in kip-ft)

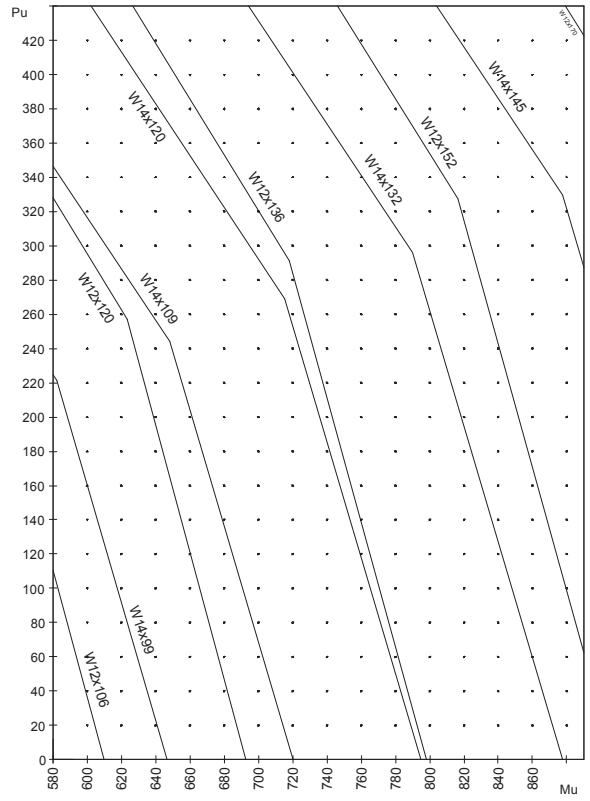


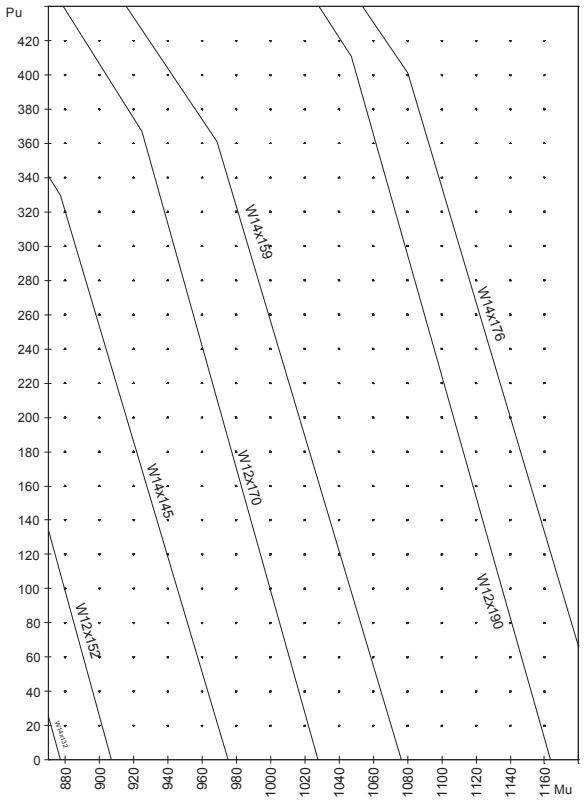



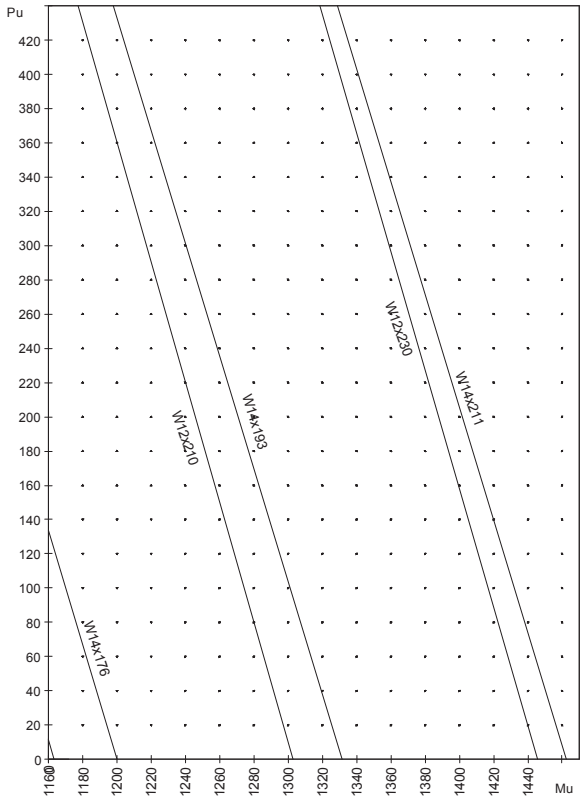



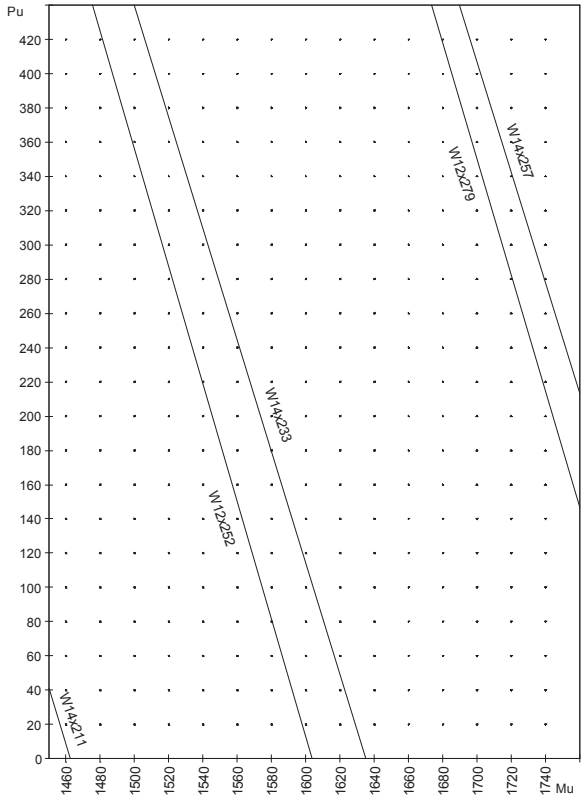



## APPENDIX D—STANDARD GRAPHS OF INTERACTION DIAGRAMS (cont'd)
## ($P_u$ in kips, $M_u$ in kip-ft)

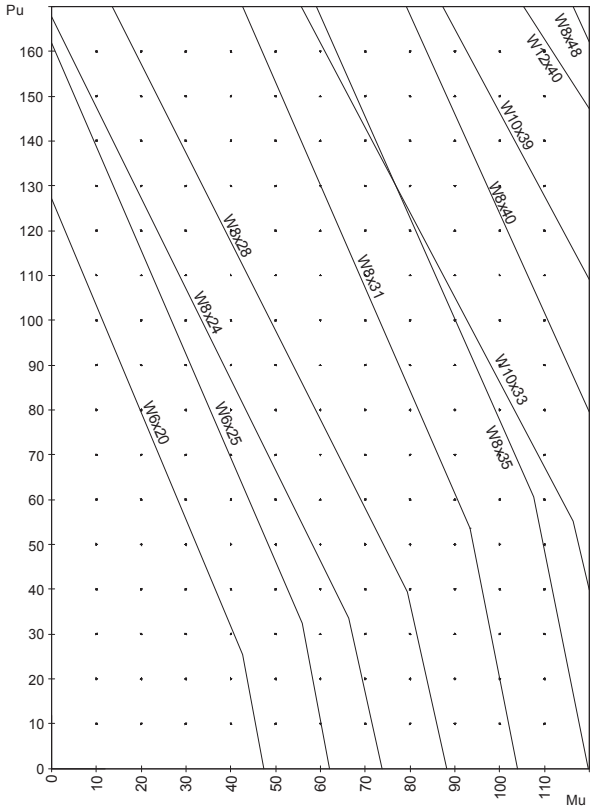


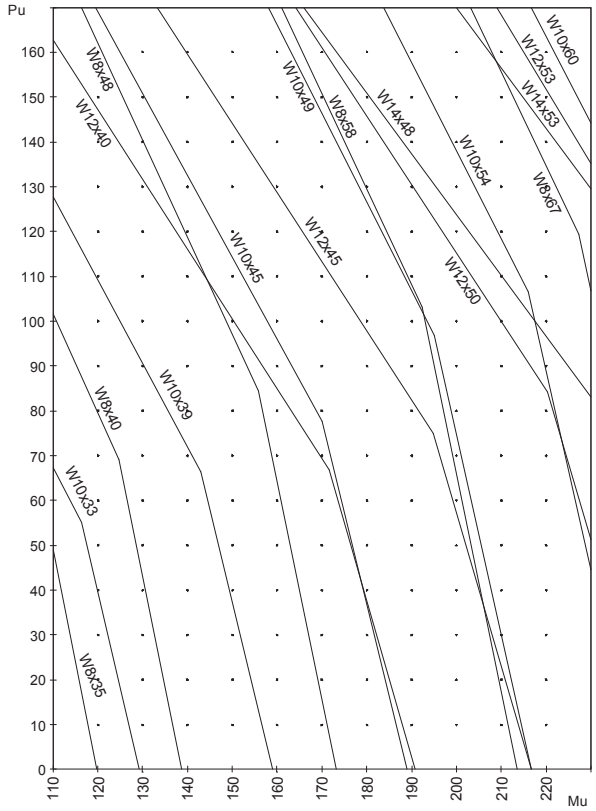



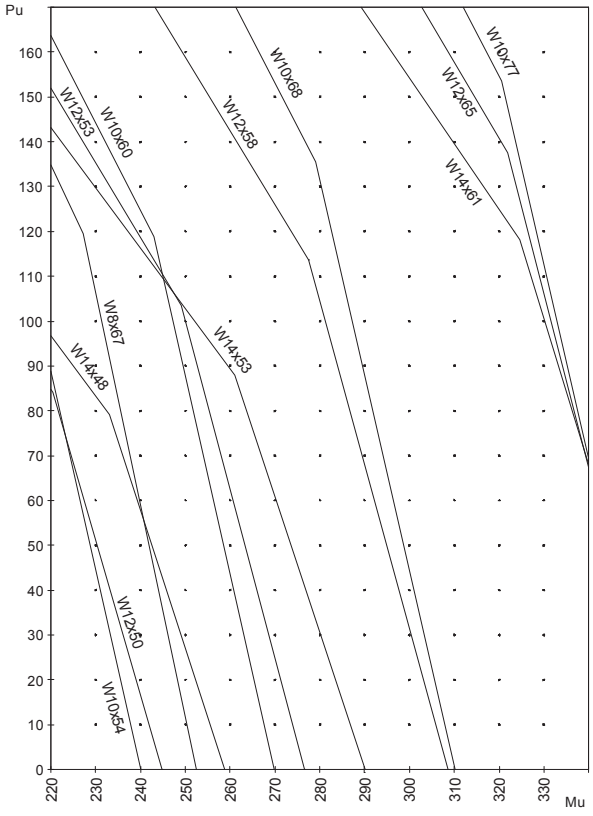



## APPENDIX D—STANDARD GRAPHS OF INTERACTION DIAGRAMS (cont'd)
## ($P_u$ in kips, $M_u$ in kip-ft)



## APPENDIX E—*Kl/r* VERIFICATIONS

| | *Kl/r* Calculations | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|
| | *KL* (ft) | | | | | | | | | | |
| Shape | 6.00 | 8.00 | 10.00 | 12.00 | 14.00 | 16.00 | 18.00 | 20.00 | 22.00 | 24.00 | 26.00 |
| W14x730 | 15.4 | 20.5 | 25.6 | 30.7 | 35.8 | 40.9 | 46.1 | 51.2 | 56.3 | 61.4 | 66.5 |
| W14x665 | 15.6 | 20.8 | 26.0 | 31.2 | 36.4 | 41.6 | 46.8 | 51.9 | 57.1 | 62.3 | 67.5 |
| W14x605 | 15.8 | 21.1 | 26.4 | 31.6 | 36.9 | 42.2 | 47.5 | 52.7 | 58.0 | 63.3 | 68.6 |
| W14x550 | 16.0 | 21.4 | 26.7 | 32.1 | 37.4 | 42.8 | 48.1 | 53.5 | 58.8 | 64.1 | 69.5 |
| W14x500 | 16.3 | 21.7 | 27.1 | 32.5 | 37.9 | 43.3 | 48.8 | 54.2 | 59.6 | 65.0 | 70.4 |
| W14x455 | 16.4 | 21.9 | 27.4 | 32.9 | 38.4 | 43.8 | 49.3 | 54.8 | 60.3 | 65.8 | 71.2 |
| W14x426 | 16.6 | 22.1 | 27.6 | 33.2 | 38.7 | 44.2 | 49.8 | 55.3 | 60.8 | 66.4 | 71.9 |
| W14x398 | 16.7 | 22.3 | 27.8 | 33.4 | 39.0 | 44.5 | 50.1 | 55.7 | 61.3 | 66.8 | 72.4 |
| W14x370 | 16.9 | 22.5 | 28.1 | 33.7 | 39.3 | 45.0 | 50.6 | 56.2 | 61.8 | 67.4 | 73.1 |
| W14x342 | 17.0 | 22.6 | 28.3 | 34.0 | 39.6 | 45.3 | 50.9 | 56.6 | 62.3 | 67.9 | 73.6 |
| W14x311 | 17.1 | 22.9 | 28.6 | 34.3 | 40.0 | 45.7 | 51.4 | 57.1 | 62.9 | 68.6 | 74.3 |
| W14x283 | 17.3 | 23.0 | 28.8 | 34.5 | 40.3 | 46.0 | 51.8 | 57.6 | 63.3 | 69.1 | 74.8 |
| W14x257 | 17.4 | 23.2 | 29.1 | 34.9 | 40.7 | 46.5 | 52.3 | 58.1 | 63.9 | 69.7 | 75.5 |
| W14x233 | 17.6 | 23.4 | 29.3 | 35.1 | 41.0 | 46.8 | 52.7 | 58.5 | 64.4 | 70.2 | 76.1 |
| W14x211 | 17.7 | 23.6 | 29.5 | 35.4 | 41.3 | 47.2 | 53.1 | 59.0 | 64.9 | 70.8 | 76.7 |
| W14x193 | 17.8 | 23.7 | 29.6 | 35.6 | 41.5 | 47.4 | 53.3 | 59.3 | 65.2 | 71.1 | 77.0 |
| W14x176 | 17.9 | 23.9 | 29.9 | 35.8 | 41.8 | 47.8 | 53.7 | 59.7 | 65.7 | 71.6 | 77.6 |
| W14x159 | 18.0 | 24.0 | 30.0 | 36.0 | 42.0 | 48.0 | 54.0 | 60.0 | 66.0 | 72.0 | 78.0 |
| W14x145 | 18.1 | 24.1 | 30.2 | 36.2 | 42.2 | 48.2 | 54.3 | 60.3 | 66.3 | 72.4 | 78.4 |
| W14x132 | 19.1 | 25.5 | 31.9 | 38.3 | 44.7 | 51.1 | 57.4 | 63.8 | 70.2 | 76.6 | 83.0 |
| W14x120 | 19.3 | 25.7 | 32.1 | 38.5 | 44.9 | 51.3 | 57.8 | 64.2 | 70.6 | 77.0 | 83.4 |
| W14x109 | 19.3 | 25.7 | 32.2 | 38.6 | 45.0 | 51.5 | 57.9 | 64.3 | 70.8 | 77.2 | 83.6 |
| W14x99 | 19.4 | 25.9 | 32.3 | 38.8 | 45.3 | 51.8 | 58.2 | 64.7 | 71.2 | 77.6 | 84.1 |
| W14x90 | 19.5 | 25.9 | 32.4 | 38.9 | 45.4 | 51.9 | 58.4 | 64.9 | 71.4 | 77.8 | 84.3 |
| W14x82 | 29.0 | 38.7 | 48.4 | 58.1 | 67.7 | 77.4 | 87.1 | 96.8 | 106.5 | 116.1 | 125.8 |
| W14x74 | 29.0 | 38.7 | 48.4 | 58.1 | 67.7 | 77.4 | 87.1 | 96.8 | 106.5 | 116.1 | 125.8 |
| W14x68 | 29.3 | 39.0 | 48.8 | 58.5 | 68.3 | 78.0 | 87.8 | 97.6 | 107.3 | 117.1 | 126.8 |
| W14x61 | 29.4 | 39.2 | 49.0 | 58.8 | 68.6 | 78.4 | 88.2 | 98.0 | 107.8 | 117.6 | 127.3 |
| W14x53 | 37.5 | 50.0 | 62.5 | 75.0 | 87.5 | 100.0 | 112.5 | 125.0 | 137.5 | 150.0 | 162.5 |
| W14x48 | 37.7 | 50.3 | 62.8 | 75.4 | 88.0 | 100.5 | 113.1 | 125.7 | 138.2 | 150.8 | 163.4 |
| W12x336 | 20.7 | 27.7 | 34.6 | 41.5 | 48.4 | 55.3 | 62.2 | 69.2 | 76.1 | 83.0 | 89.9 |
| W12x305 | 21.1 | 28.1 | 35.1 | 42.1 | 49.1 | 56.1 | 63.2 | 70.2 | 77.2 | 84.2 | 91.2 |
| W12x279 | 21.3 | 28.4 | 35.5 | 42.6 | 49.7 | 56.8 | 63.9 | 71.0 | 78.1 | 85.2 | 92.3 |
| W12x252 | 21.6 | 28.7 | 35.9 | 43.1 | 50.3 | 57.5 | 64.7 | 71.9 | 79.0 | 86.2 | 93.4 |
| W12x230 | 21.8 | 29.0 | 36.3 | 43.5 | 50.8 | 58.0 | 65.3 | 72.5 | 79.8 | 87.0 | 94.3 |
| W12x210 | 22.0 | 29.3 | 36.6 | 43.9 | 51.2 | 58.5 | 65.9 | 73.2 | 80.5 | 87.8 | 95.1 |
| W12x190 | 22.2 | 29.5 | 36.9 | 44.3 | 51.7 | 59.1 | 66.5 | 73.8 | 81.2 | 88.6 | 96.0 |
| W12x170 | 22.4 | 29.8 | 37.3 | 44.7 | 52.2 | 59.6 | 67.1 | 74.5 | 82.0 | 89.4 | 96.9 |
| W12x152 | 22.6 | 30.1 | 37.6 | 45.1 | 52.7 | 60.2 | 67.7 | 75.2 | 82.8 | 90.3 | 97.8 |
| W12x136 | 22.8 | 30.4 | 38.0 | 45.6 | 53.2 | 60.8 | 68.4 | 75.9 | 83.5 | 91.1 | 98.7 |
| W12x120 | 23.0 | 30.7 | 38.3 | 46.0 | 53.7 | 61.3 | 69.0 | 76.7 | 84.3 | 92.0 | 99.7 |
| W12x106 | 23.2 | 30.9 | 38.6 | 46.3 | 54.0 | 61.7 | 69.5 | 77.2 | 84.9 | 92.6 | 100.3 |
| W12x96 | 23.3 | 31.1 | 38.8 | 46.6 | 54.4 | 62.1 | 69.9 | 77.7 | 85.4 | 93.2 | 101.0 |
| W12x87 | 23.5 | 31.3 | 39.1 | 46.9 | 54.7 | 62.5 | 70.4 | 78.2 | 86.0 | 93.8 | 101.6 |
| W12x79 | 23.6 | 31.5 | 39.3 | 47.2 | 55.1 | 63.0 | 70.8 | 78.7 | 86.6 | 94.4 | 102.3 |
| W12x72 | 23.7 | 31.6 | 39.5 | 47.4 | 55.3 | 63.2 | 71.1 | 78.9 | 86.8 | 94.7 | 102.6 |
| W12x65 | 23.8 | 31.8 | 39.7 | 47.7 | 55.6 | 63.6 | 71.5 | 79.5 | 87.4 | 95.4 | 103.3 |
| W12x58 | 28.7 | 38.2 | 47.8 | 57.4 | 66.9 | 76.5 | 86.1 | 95.6 | 105.2 | 114.7 | 124.3 |
| W12x53 | 29.0 | 38.7 | 48.4 | 58.1 | 67.7 | 77.4 | 87.1 | 96.8 | 106.5 | 116.1 | 125.8 |
| W12x50 | 36.7 | 49.0 | 61.2 | 73.5 | 85.7 | 98.0 | 110.2 | 122.4 | 134.7 | 146.9 | 159.2 |
| W12x45 | 37.1 | 49.5 | 61.9 | 74.2 | 86.6 | 99.0 | 111.3 | 123.7 | 136.1 | 148.5 | 160.8 |
| W12x40 | 37.3 | 49.7 | 62.2 | 74.6 | 87.0 | 99.5 | 111.9 | 124.4 | 136.8 | 149.2 | 161.7 |
| W10x112 | 26.9 | 35.8 | 44.8 | 53.7 | 62.7 | 71.6 | 80.6 | 89.6 | 98.5 | 107.5 | 116.4 |
| W10x100 | 27.2 | 36.2 | 45.3 | 54.3 | 63.4 | 72.5 | 81.5 | 90.6 | 99.6 | 108.7 | 117.7 |
| W10x88 | 27.4 | 36.5 | 45.6 | 54.8 | 63.9 | 73.0 | 82.1 | 91.3 | 100.4 | 109.5 | 118.6 |
| W10x77 | 27.7 | 36.9 | 46.2 | 55.4 | 64.6 | 73.8 | 83.1 | 92.3 | 101.5 | 110.8 | 120.0 |
| W10x68 | 27.8 | 37.1 | 46.3 | 55.6 | 64.9 | 74.1 | 83.4 | 92.7 | 101.9 | 111.2 | 120.5 |
| W10x60 | 28.0 | 37.4 | 46.7 | 56.0 | 65.4 | 74.7 | 84.0 | 93.4 | 102.7 | 112.1 | 121.4 |
| W10x54 | 28.1 | 37.5 | 46.9 | 56.3 | 65.6 | 75.0 | 84.4 | 93.8 | 103.1 | 112.5 | 121.9 |
| W10x49 | 28.3 | 37.8 | 47.2 | 56.7 | 66.1 | 75.6 | 85.0 | 94.5 | 103.9 | 113.4 | 122.8 |
| W10x45 | 35.8 | 47.8 | 59.7 | 71.6 | 83.6 | 95.5 | 107.5 | 119.4 | 131.3 | 143.3 | 155.2 |
| W10x39 | 36.4 | 48.5 | 60.6 | 72.7 | 84.8 | 97.0 | 109.1 | 121.2 | 133.3 | 145.5 | 157.6 |
| W10x33 | 37.1 | 49.5 | 61.9 | 74.2 | 86.6 | 99.0 | 111.3 | 123.7 | 136.1 | 148.5 | 160.8 |
| W8x67 | 34.0 | 45.3 | 56.6 | 67.9 | 79.2 | 90.6 | 101.9 | 113.2 | 124.5 | 135.8 | 147.2 |
| W8x58 | 34.3 | 45.7 | 57.1 | 68.6 | 80.0 | 91.4 | 102.9 | 114.3 | 125.7 | 137.1 | 148.6 |
| W8x48 | 34.6 | 46.2 | 57.7 | 69.2 | 80.8 | 92.3 | 103.8 | 115.4 | 126.9 | 138.5 | 150.0 |
| W8x40 | 35.3 | 47.1 | 58.8 | 70.6 | 82.4 | 94.1 | 105.9 | 117.6 | 129.4 | 141.2 | 152.9 |
| W8x35 | 35.5 | 47.3 | 59.1 | 70.9 | 82.8 | 94.6 | 106.4 | 118.2 | 130.0 | 141.9 | 153.7 |
| W8x31 | 35.6 | 47.5 | 59.4 | 71.3 | 83.2 | 95.0 | 106.9 | 118.8 | 130.7 | 142.6 | 154.5 |
| W8x28 | 44.4 | 59.3 | 74.1 | 88.9 | 103.7 | 118.5 | 133.3 | 148.1 | 163.0 | 177.8 | 192.6 |
| W8x24 | 44.7 | 59.6 | 74.5 | 89.4 | 104.3 | 119.3 | 134.2 | 149.1 | 164.0 | 178.9 | 193.8 |
| W6x25 | 47.4 | 63.2 | 78.9 | 94.7 | 110.5 | 126.3 | 142.1 | 157.9 | 173.7 | 189.5 | 205.3 |
| W6x20 | 48.0 | 64.0 | 80.0 | 96.0 | 112.0 | 128.0 | 144.0 | 160.0 | 176.0 | 192.0 | 208.0 |

Note: Shading indicates *Kl/r* greater than 200.

## APPENDIX E—*Kl/r* VERIFICATIONS (cont'd)

| | *Kl/r* Calculations | | | | | |
|---|---|---|---|---|---|---|
| | *KL* (ft) | | | | | |
| Shape | 28.00 | 30.00 | 32.00 | 34.00 | 36.00 | 38.00 |
| W14x730 | 71.6 | 76.8 | 81.9 | 87.0 | 92.1 | 97.2 |
| W14x665 | 72.7 | 77.9 | 83.1 | 88.3 | 93.5 | 98.7 |
| W14x605 | 73.8 | 79.1 | 84.4 | 89.7 | 94.9 | 100.2 |
| W14x550 | 74.8 | 80.2 | 85.5 | 90.9 | 96.2 | 101.6 |
| W14x500 | 75.8 | 81.3 | 86.7 | 92.1 | 97.5 | 102.9 |
| W14x455 | 76.7 | 82.2 | 87.7 | 93.2 | 98.6 | 104.1 |
| W14x426 | 77.4 | 82.9 | 88.5 | 94.0 | 99.5 | 105.1 |
| W14x398 | 78.0 | 83.5 | 89.1 | 94.7 | 100.2 | 105.8 |
| W14x370 | 78.7 | 84.3 | 89.9 | 95.6 | 101.2 | 106.8 |
| W14x342 | 79.2 | 84.9 | 90.6 | 96.2 | 101.9 | 107.5 |
| W14x311 | 80.0 | 85.7 | 91.4 | 97.1 | 102.9 | 108.6 |
| W14x283 | 80.6 | 86.3 | 92.1 | 97.8 | 103.6 | 109.4 |
| W14x257 | 81.4 | 87.2 | 93.0 | 98.8 | 104.6 | 110.4 |
| W14x233 | 82.0 | 87.8 | 93.7 | 99.5 | 105.4 | 111.2 |
| W14x211 | 82.6 | 88.5 | 94.3 | 100.2 | 106.1 | 112.0 |
| W14x193 | 83.0 | 88.9 | 94.8 | 100.7 | 106.7 | 112.6 |
| W14x176 | 83.6 | 89.6 | 95.5 | 101.5 | 107.5 | 113.4 |
| W14x159 | 84.0 | 90.0 | 96.0 | 102.0 | 108.0 | 114.0 |
| W14x145 | 84.4 | 90.5 | 96.5 | 102.5 | 108.5 | 114.6 |
| W14x132 | 89.4 | 95.7 | 102.1 | 108.5 | 114.9 | 121.3 |
| W14x120 | 89.8 | 96.3 | 102.7 | 109.1 | 115.5 | 121.9 |
| W14x109 | 90.1 | 96.5 | 102.9 | 109.4 | 115.8 | 122.3 |
| W14x99 | 90.6 | 97.0 | 103.5 | 110.0 | 116.4 | 122.9 |
| W14x90 | 90.8 | 97.3 | 103.8 | 110.3 | 116.8 | 123.2 |
| W14x82 | 135.5 | 145.2 | 154.8 | 164.5 | 174.2 | 183.9 |
| W14x74 | 135.5 | 145.2 | 154.8 | 164.5 | 174.2 | 183.9 |
| W14x68 | 136.6 | 146.3 | 156.1 | 165.9 | 175.6 | 185.4 |
| W14x61 | 137.1 | 146.9 | 156.7 | 166.5 | 176.3 | 186.1 |
| W14x53 | 175.0 | 187.5 | 200.0 | 212.5 | 225.0 | 237.5 |
| W14x48 | 175.9 | 188.5 | 201.0 | 213.6 | 226.2 | 238.7 |
| W12x336 | 96.8 | 103.7 | 110.7 | 117.6 | 124.5 | 131.4 |
| W12x305 | 98.2 | 105.3 | 112.3 | 119.3 | 126.3 | 133.3 |
| W12x279 | 99.4 | 106.5 | 113.6 | 120.7 | 127.8 | 134.9 |
| W12x252 | 100.6 | 107.8 | 115.0 | 122.2 | 129.3 | 136.5 |
| W12x230 | 101.5 | 108.8 | 116.0 | 123.3 | 130.5 | 137.8 |
| W12x210 | 102.4 | 109.8 | 117.1 | 124.4 | 131.7 | 139.0 |
| W12x190 | 103.4 | 110.8 | 118.2 | 125.5 | 132.9 | 140.3 |
| W12x170 | 104.3 | 111.8 | 119.3 | 126.7 | 134.2 | 141.6 |
| W12x152 | 105.3 | 112.9 | 120.4 | 127.9 | 135.4 | 142.9 |
| W12x136 | 106.3 | 113.9 | 121.5 | 129.1 | 136.7 | 144.3 |
| W12x120 | 107.3 | 115.0 | 122.7 | 130.4 | 138.0 | 145.7 |
| W12x106 | 108.0 | 115.8 | 123.5 | 131.2 | 138.9 | 146.6 |
| W12x96 | 108.7 | 116.5 | 124.3 | 132.0 | 139.8 | 147.6 |
| W12x87 | 109.4 | 117.3 | 125.1 | 132.9 | 140.7 | 148.5 |
| W12x79 | 110.2 | 118.0 | 125.9 | 133.8 | 141.6 | 149.5 |
| W12x72 | 110.5 | 118.4 | 126.3 | 134.2 | 142.1 | 150.0 |
| W12x65 | 111.3 | 119.2 | 127.2 | 135.1 | 143.0 | 151.0 |
| W12x58 | 133.9 | 143.4 | 153.0 | 162.5 | 172.1 | 181.7 |
| W12x53 | 135.5 | 145.2 | 154.8 | 164.5 | 174.2 | 183.9 |
| W12x50 | 171.4 | 183.7 | 195.9 | 208.2 | 220.4 | 232.7 |
| W12x45 | 173.2 | 185.6 | 197.9 | 210.3 | 222.7 | 235.1 |
| W12x40 | 174.1 | 186.5 | 199.0 | 211.4 | 223.8 | 236.3 |
| W10x112 | 125.4 | 134.3 | 143.3 | 152.2 | 161.2 | 170.1 |
| W10x100 | 126.8 | 135.8 | 144.9 | 154.0 | 163.0 | 172.1 |
| W10x88 | 127.8 | 136.9 | 146.0 | 155.1 | 164.3 | 173.4 |
| W10x77 | 129.2 | 138.5 | 147.7 | 156.9 | 166.2 | 175.4 |
| W10x68 | 129.7 | 139.0 | 148.3 | 157.5 | 166.8 | 176.1 |
| W10x60 | 130.7 | 140.1 | 149.4 | 158.8 | 168.1 | 177.4 |
| W10x54 | 131.3 | 140.6 | 150.0 | 159.4 | 168.8 | 178.1 |
| W10x49 | 132.3 | 141.7 | 151.2 | 160.6 | 170.1 | 179.5 |
| W10x45 | 167.2 | 179.1 | 191.0 | 203.0 | 214.9 | 226.9 |
| W10x39 | 169.7 | 181.8 | 193.9 | 206.1 | 218.2 | 230.3 |
| W10x33 | 173.2 | 185.6 | 197.9 | 210.3 | 222.7 | 235.1 |
| W8x67 | 158.5 | 169.8 | 181.1 | 192.5 | 203.8 | 215.1 |
| W8x58 | 160.0 | 171.4 | 182.9 | 194.3 | 205.7 | 217.1 |
| W8x48 | 161.5 | 173.1 | 184.6 | 196.2 | 207.7 | 219.2 |
| W8x40 | 164.7 | 176.5 | 188.2 | 200.0 | 211.8 | 223.5 |
| W8x35 | 165.5 | 177.3 | 189.2 | 201.0 | 212.8 | 224.6 |
| W8x31 | 166.3 | 178.2 | 190.1 | 202.0 | 213.9 | 225.7 |
| W8x28 | 207.4 | 222.2 | 237.0 | 251.9 | 266.7 | 281.5 |
| W8x24 | 208.7 | 223.6 | 238.5 | 253.4 | 268.3 | 283.2 |
| W6x25 | 221.1 | 236.8 | 252.6 | 268.4 | 284.2 | 300.0 |
| W6x20 | 224.0 | 240.0 | 256.0 | 272.0 | 288.0 | 304.0 |

Note: Shading indicates *Kl/r* greater than 200.