

# Design Tables for Top- and Seat-Angle with Double Web-Angle Connections

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## ABSTRACT

This paper provides a set of design tables, based on the AISC/LRFD Specification (1994), for the selection of top- and seat-angle with double web-angle connections given beam sections and applied loads. These tables enable the engineer to rapidly select proper angle sizes and configurations as well as determine the moment-rotation curve ( $M-\theta$ ) for the connection. Design procedures and a comprehensive case study are also presented.

## 1. INTRODUCTION

The aim of the work described in this paper is to provide design tables for top- and seat-angle with double web-angle connections (Figure 1) which can be used in semi-rigid frame design. To this end, a set of tables has been developed for the rapid selection of angle sizes and configurations as well as the values of the three parameters of a power model describing the  $M-\theta$  curve of the connection (Figure 2).

The three-parameter power model was proposed by Richard (1961). They are: the initial connection stiffness  $R_{ki}$ , the ultimate moment capacity  $M_u$ , and the shape parameter  $n$ . The values  $R_{ki}$  and  $M_u$  can be determined in a simple procedure using an assumed failure mechanism (Kishi et al, 1993). The shape parameter  $n$  is determined as a linear function of  $\log_{10}\theta_o$  (Figure 3) (Kishi and Hasan et al., 1994a & 1994b) based on experimental data installed in the Program SCDB (Chen and Kishi, 1986), where  $\theta_o = M_u/R_{ki}$ .

Since hand calculations for these three parameters are cumbersome, simple design tables are provided for eight general cases and two simple design examples are presented to illustrate the use of these tables in the following discussion.

## 2. GENERAL DESIGN PROCEDURES

The design of beam-columns is an iterative procedure. The general procedure for the design of PR frames (Y. Kim and Chen, 1996) is outlined below:

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1. Preliminary member sizing.
2. Select beam-to-column connections using design tables that are provided in this paper [Appendix A].
3. Load application: one of six factored load combinations.
4. Get modified connection stiffness using three parameters [Y. Kim and Chen, 1996].
5. Carry out the first-order elastic analysis, considering the connection behavior as a spring element.
6. Check the stability of frames by the LRFD (H1-1a, b) and the strength limit states [Y. Kim and Chen, 1996].
7. Check for serviceability limit states to ensure adequate stiffness for functionality at service loads.
8. Return to Step 4 until the six factored combinations become satisfactory. If member sizing is required, then return to Step 1.

## 3. STUDY OF CONNECTION PARAMETERS

Nine connection parameters for the top- and seat-angle with double web-angle (Figure 1) are summarized in Table 1.

### BOLT

Two diameters of A325 bolts are included in the design tables:  $\frac{3}{4}$ -in. and  $\frac{7}{8}$ -in. Note that connections with  $\frac{3}{4}$ -in. bolts have a higher  $M-\theta$  curve than connections with  $\frac{7}{8}$ -in. bolts. This is because the failure mechanism is related to the width of the nut.

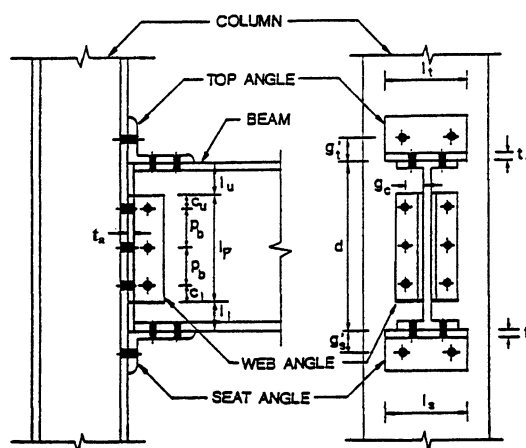


Fig. 1. Top- and seat-angle with double web-angle.

Table 1. Major Connection Parameters		
	Description	Symbol
BOLT	Nut's width across flat of bolt	$w$
BEAM	Nominal depth of beam	$d$
MATERIAL	Yield strength of beam	$F_y$
TOP- AND	Thickness Length	$t_t (= t_s)$ $l_t (= l_s)$
SEAT-ANGLE	Distance from heel to center of fastener hole on vertical leg	$g'_i$
WEB-ANGLE	Thickness Length Distance from heel to center of fastener hole	$t_a$ $l_p$ $g_c$

### BEAM

From a preliminary moment design, the beam depth ( $d$ ) is selected by estimating the required plastic section modulus.

Required plastic section modulus:

$$Z_x = \frac{M_{\text{maximum}}}{F_y} = \left( \frac{WL^2}{8} \right) \frac{1}{F_y} = \frac{WL^2}{8F_y} \quad (1)$$

where

- $W$  = uniformly distributed load
- $L$  = length of the beam
- $F_y$  = yield strength of materials

Increasing the depth of beam increases the moment capacity of the connection. The use of 50 ksi steel gives a higher  $M$ - $\theta_r$  curve than 36 ksi steel.

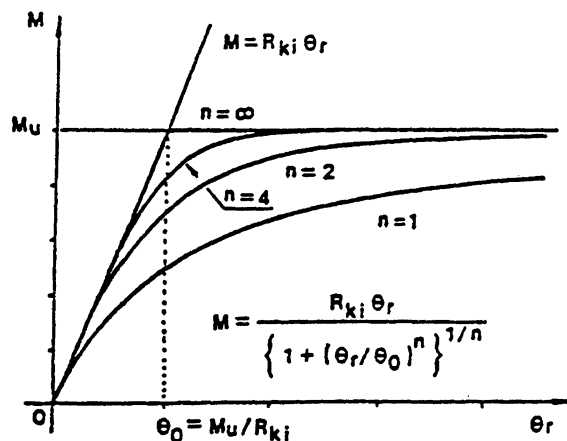


Fig. 2. General shape of the three-parameter power model.

### TOP- AND SEAT-ANGLE

Symmetry allows the seat-angle to be treated the same way as the top-angle. Six L6×4 angles for top- and seat-angles, with a decreasing distance from heel to center of fastener hole on vertical leg  $g'_i$  (Table 2), are used.

$$g'_i = (H1 + C1) + t_i \quad (2)$$

where  $g'_i$  should be increased to ¼-in. unit.  $H1$  and  $C1$  are given in "Entering and Tightening Clearances" in Table 8-4 of AISC/LRFD Manual Vol. II (1994). For example, for a ¾-in. dia. bolt and CASE 1 in Table 2,

$$g'_i = (H1 + C1) + t_i = (1\frac{1}{2}\text{-in.} + 1\frac{1}{4}\text{-in.}) + \frac{3}{4}\text{-in.} = 2.47 \text{ in.}$$

So, the final  $g'_i$  is 2½-in. Engineers can vary the length of top- and seat-angles by using "Staggered Bolts". Only 6-in. and 8-in. angles are used in these design tables. An increase in thickness and length of the angles results in a higher  $M$ - $\theta_r$  curve.

### WEB-ANGLE

From a preliminary shear design ( $WL/2$ ) using Table 9-2 of AISC/LRFD "All-Bolted Double-Angle Connections", engineers can select the thickness of the web-angles ( $t_a$ ) and the number of bolts ( $N$ ). For a given number of bolts, the length of web-angle ( $l_p$ ) can be calculated by

$$l_p = (N - 1) \times \text{Bolt spacing (3-in.)} + \text{Both edge distances (2.5-in. or 3-in.)} \quad (3)$$

Both edge distances are used: 2.5-in. for ¾-in. dia. bolts and 3-in. for 7/8-in. dia. bolts. Four 2 L4×3.5 angles are used for web-angles in these tables. Distance from heel to center of

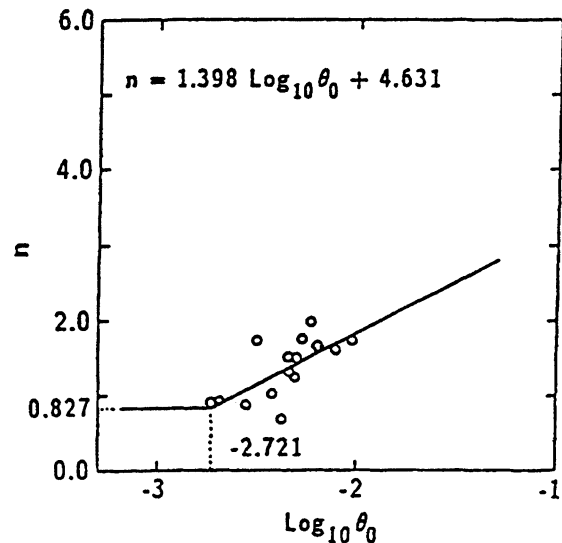


Fig. 3. Distribution of  $n$  (Kishi et al. 1994).

fastener hole  $g_c$  is tabulated in Table 3. Considering beam section and its possible number of bolts in the web-angle, the length of web-angle  $l_p$  is tabulated in Table 4.

$$g_c = (H1+C1) + t_a \quad (4)$$

where  $g_c$  should be increased to the nearest  $\frac{1}{4}$ -in.

### 3.1 Design Table

The design tables include 8 basic connection combinations. These combinations are summarized in Table 5.

## 4. MOMENT-ROTATION MODELING OF CONNECTIONS

The connection behavior is represented by its moment-rotation relationship. Extensive experimental work on connections has been performed, and a large body of moment-rotation data collected (Goverdhan 1983, Nethercot 1985, Kishi and Chen 1986 and Chen and Kishi 1989). Using this data base, researchers have developed several connection models including linear; polynomial; B-spline; power; and exponential models. A three-parameter power model proposed by Richard (1961) is used for the design tables and may be written as

$$\bar{m} = \frac{\bar{\theta}}{(1 + \bar{\theta}^n)^{1/n}} \quad (5)$$

where

- $\bar{m}$  = nondimensional connection moment =  $M/M_u$
- $\bar{\theta}$  = nondimensional relative rotation =  $\theta/\theta_o$
- $n$  = shape parameter
- $\theta_o$  = reference plastic rotation =  $M_u/R_{ki}$

A practical procedure (Kishi et al 1993) for determining the three connection parameters is summarized here.

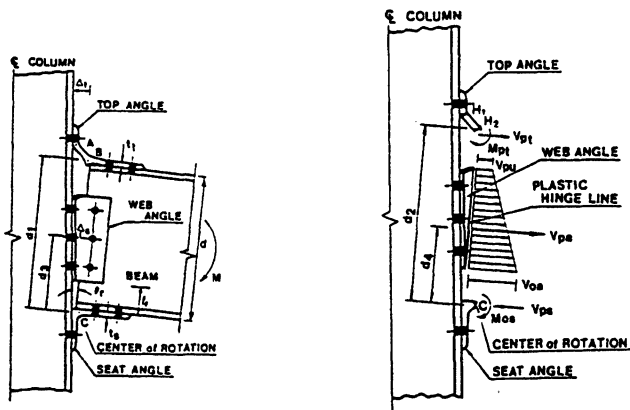


Fig. 4. Top- and seat-angle with web-angle connection (Kishi et al. 1993).

Top- and Seat-Angle	L6×4× $t_f$ × $k_f$	Bolt Diameter	
		$\frac{3}{4}$ -in.	$\frac{7}{8}$ -in.
CASE 1	L6×4× $\frac{3}{4}$ ×1 $\frac{1}{4}$	2 $\frac{1}{2}$ -in.	2 $\frac{3}{4}$ -in.
CASE 2	L6×4× $\frac{5}{8}$ ×1 $\frac{1}{8}$	2 $\frac{1}{2}$ -in.	2 $\frac{3}{4}$ -in.
CASE 3	L6×4× $\frac{9}{16}$ ×1 $\frac{1}{16}$	2 $\frac{1}{4}$ -in.	2 $\frac{3}{4}$ -in.
CASE 4	L6×4× $\frac{1}{2}$ ×1	2 $\frac{1}{4}$ -in.	2 $\frac{1}{2}$ -in.
CASE 5	L6×4× $\frac{7}{16}$ × $\frac{15}{16}$	2 $\frac{1}{4}$ -in.	2 $\frac{1}{2}$ -in.
CASE 6	L6×4× $\frac{3}{8}$ × $\frac{7}{8}$	2 $\frac{1}{4}$ -in.	2 $\frac{1}{2}$ -in.

### 4.1 Determination of the initial connection stiffness, $R_{ki}$

The following assumptions are made for the initial stiffness.

1. Connection rotates about the center (C) located on the seat-angle as shown, in Figure 4.
2. The leg of the angle connected to the column behaves linearly elastically and the leg of the angle connected to the beam behaves as a rigid body.
3. The top-angle acts as a cantilever beam in which the fixed support is assumed to be at the fastener-hole edge near the beam flange in the leg adjacent to the column face as shown in Figure 5.
4. The deformed pattern of the web-angle is similar to that of the top-angle (Figure 6).
5. The bearing pressure is uniformly distributed over the outstanding leg of the seat-angle (Figure 7).

Based on these assumptions and considering shear deformation, the initial stiffness can be formulated from simple elastic beam theory.

Initial stiffness contributed by the top-angle:

$$K_{it} = \frac{3EI_t(d_1)^2}{g_1(g_1^2 + 0.78t_f^2)}$$

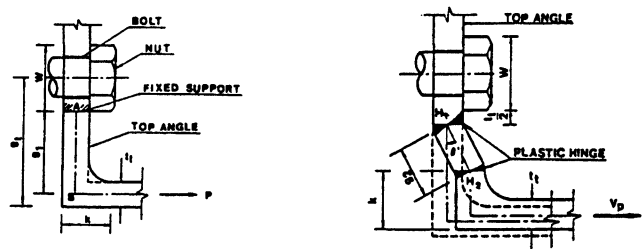


Fig. 5. Top-angle connection (Kishi et al. 1993).

Web-angle	2L4×3 $\frac{1}{2}$ × $t_a$ × $k_a$	Bolt Diameter	
		$\frac{3}{4}$ -in.	$\frac{7}{8}$ -in.
CASE 1	2L4×3 $\frac{1}{2}$ × $\frac{1}{2}$ × $\frac{15}{16}$	2 $\frac{1}{4}$ -in.	2 $\frac{1}{2}$ -in.
CASE 2	2L4×3 $\frac{1}{2}$ × $\frac{3}{8}$ × $\frac{13}{16}$	2 $\frac{1}{4}$ -in.	2 $\frac{1}{2}$ -in.
CASE 3	2L4×3 $\frac{1}{2}$ × $\frac{5}{16}$ × $\frac{3}{4}$	2-in.	2 $\frac{1}{2}$ -in.
CASE 4	2L4×3 $\frac{1}{2}$ × $\frac{1}{4}$ × $\frac{1}{16}$	2-in.	2 $\frac{1}{4}$ -in.

Initial stiffness contributed by the seat-angle:

$$K_{is} = \frac{4EI_s}{I_{so}}$$

Initial stiffness contributed by the web-angles:

$$K_{ia} = \frac{6EI_a(d_3)^2}{g_3(g_3^2 + 0.78t_a^2)}$$

where

Bending rigidity of the top-angle:

$$EI_t = 29,000 * I_t(t_t)^3 / 12$$

Bending rigidity of the seat-angles:

$$EI_s = 29,000 * I_s(t_s)^3 / 12$$

Bending rigidity of the web-angle:

$$EI_a = 29,000 * I_p(t_a)^3 / 12$$

The initial stiffness of the top- and seat-angle with double web-angles is

$$R_{ki} = K_{it} + K_{is} + K_{ia} \quad (6)$$

where

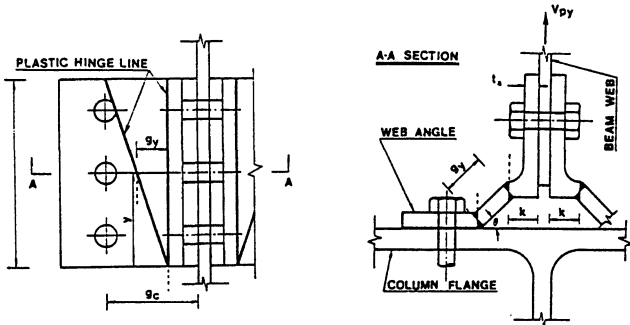


Fig. 6. Mechanism of web-angle connection of ultimate condition (Kishi et al. 1993).

$g_1$  = length of the vertical leg of the top-angle that acted as a cantilever beam

$$= g'_1 - w/2 - t_t/2$$

$g_3$  = length of the leg of the web-angle that acted as a cantilever beam

$$= g_c - w/2 - t_a/2$$

$d_1$  = distance from the center of rotation to the line of the pull force acted upon a top-angle

$$= d + t_s/2 + t_t/2$$

$l_{so}$  = distance from the critical section to the toe of the outstanding leg of the seat-angle

$$d_3 = d/2 + t_s/2$$

#### 4.2 Determination of the ultimate moment capacity, $M_u$

The mechanism moment capacity of a connection is reached when an idealized elastic-plastic collapse mechanism is developed. On the basis of experimental studies, the collapse mechanism of a connection may be modeled from the individual angles. The mechanism moment of a connection may be obtained by summation of the plastic moment capacities contributed by each angle. Herein, plastic beam theory considering the bending moment-shear interaction is used to derive the expression for the mechanism moment. The ultimate moment of the top- and seat-angle with double web-angles is

$$M_u = M_{os} + M_{pt} + V_{pt}d_2 + 2V_{pd}d_4 \quad (7)$$

where

$M_{pt} = V_{pt}g_2/2$  plastic moment in the top-angle ( $\sigma_y = F_y$ )

$M_{os} = \sigma_y I_s(t_s)^2/4$  plastic moment in the seat-angle

$V_{pt}$  = plastic shear force in vertical leg of the top-angle

$V_{pt}$  is determined by solving the following equation

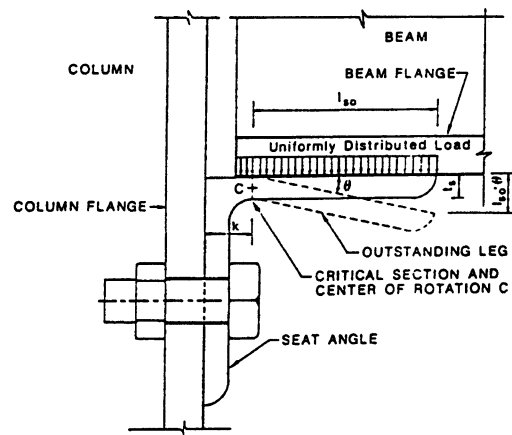


Fig. 7. Seat-angle connection (Kishi et al. 1993).

Table 4. Length of Web-angle [ $l_p$ ]								
Beam	2 row	3 row	4 row	5 row	6 row	7 row	8 row	9 row
W8	5½-in. or 6-in.	8½-in. or 9-in.	11½-in. or 12-in.	14½-in. or 15-in.	17½-in. or 18-in.	20½-in. or 21-in.	23½-in. or 24-in.	26½-in. or 27-in.
W10								
W12								
W14								
W16								
W18								
W21	11½-in. or 12-in.	8½-in. or 9-in.	14½-in. or 15-in.	17½-in. or 18-in.	20½-in. or 21-in.	23½-in. or 24-in.	26½-in. or 27-in.	
W24								
W27								
W30	17½-in. or 18-in.	20½-in. or 21-in.	23½-in. or 24-in.	26½-in. or 27-in.	17½-in. or 18-in.	20½-in. or 21-in.	23½-in. or 24-in.	26½-in. or 27-in.
W33								
W36								
W40								
W44								

Bold numbers are for ¾-in. dia. bolts and others are for 7/8-in. dia. bolts.

$$\left(\frac{V_{pt}}{V_{ot}}\right)^4 + \frac{g_2}{t_i} \left(\frac{V_{pt}}{V_{ot}}\right) - 1 = 0 \quad (8)$$

where

$$V_{ot} = \sigma_y l_s t_s / 2$$

$$g_2 = g'_t - k_t - w / 2 - t_t / 2$$

$d_2$  = distance from the center of rotation to the line of the force  $V_{pt}$  acted upon

$$= d + t_s / 2 + k_t$$

$V_{pa}$  = the resultant of plastic shear force in a single web-angle

$$= (V_{pu} + V_{oa}) l_p / 2$$

$V_{pu}$  is determined by solving the following equation

$$\left(\frac{V_{pu}}{V_{oa}}\right)^4 + \frac{g_y}{t_a} \left(\frac{V_{pu}}{V_{oa}}\right) - 1 = 0 \quad (9)$$

where

$$V_{oa} = \sigma_y t_a / 2$$

$$g_y = g_c - k_a$$

$d_4$  = distance from the center of rotation to the line of the force  $V_{pa}$  acted upon

$$= l_p (2V_{pu} + V_{oa}) / \{3(V_{pu} + V_{oa})\} + l_t + t_s / 2$$

### 4.3 Determination of the shape parameter, $n$

The following steps determine the shape parameter  $n$ :

1. The value of  $n$  is determined from experimental tests by applying least mean square technique using Equation 5.
2. Numerical values of  $n$  are then plotted against  $\log_{10}\theta_o$ .

The shape parameter  $n$  is assumed to be a linear function of  $\log_{10}\theta_o$  (Figure 3), and is obtained by linear regression analysis from the  $n$ - $\log_{10}\theta_o$  curve. To avoid negative values of  $n$ , a horizontal segment is added to the inclined line as

$$n = 1.398 \log_{10}\theta_o + 4.631 \quad \log_{10}\theta_o > -2.721 \quad (10a)$$

$$n = 0.827 \quad \log_{10}\theta_o \leq -2.721 \quad (10b)$$

### 5. CASE STUDY-DESIGN EXAMPLE

A one-bay two-story frame (Y. Kim and Chen, 1996) is considered. The geometry, dimensions and applied loads of the frame are shown in Figure 8. All members are made of ASTM A36 steel. The angles are bolted to the structural members using high-strength bolts. All connections satisfy the design requirements in Sections J3.3, J3.4, J4, and J5.2 of the AISC/LRFD Specification (1994). All girders are adequately braced in the out-of-plane direction by the floor slabs. Member lengths are defined by centerline dimensions.

Table 5. Summary of Table			
	$l_t = l_s$	$F_y$	Bolt Dia.
CASE 1	6-in.	36 ksi	3/4-in.
CASE 2			7/8-in.
CASE 3		50 ksi	3/4-in.
CASE 4			7/8-in.
CASE 5	8-in.	36 ksi	3/4-in.
CASE 6			7/8-in.
CASE 7		50 ksi	3/4-in.
CASE 8			7/8-in.

### Roof Beam

Uniformly Distributed Load:

$$W = 0.0708 \text{ kip-in}$$

Maximum Moment:

$$M_u = WL^2/8 = (0.0708)(300)^2/8 = 796.5 \text{ kip-in}$$

Required Section Modulus:

$$Z_x = M_u/F_y = 796.5/36 = 22.13 \text{ in.}^3$$

Try W12x19 ( $Z_x = 24.7 \text{ in.}^3$ ).

Maximum Shear:

$$V_u = WL/2 = (0.0708)(300)/2 = 10.62 \text{ kips}$$

The required ultimate moment capacity of a semi-rigid connection is calculated using Equation 11. The required  $M_u$  for the roof connection is

$$M_{u \text{ required}} = M_p / 2 = (Z_x \times F_y) / 2 \quad (11)$$

$$= 444.6 \text{ kip-in}$$

For the shear design, Table 9-2 (AISC/LRFD 1994) for the selection of double web-angle connections can be used. For a given W12 beam section, 2 rows of 3/4-in. dia. bolts of A325-N and 1/4-in. thickness of web-angle, Table 9-2 gives 48.9 kips which is greater than 10.62 kips. Since the AISC/LRFD does not provide PR (partially restrained) moment connection tables, we shall use the design table developed in this paper (Figure 9), and find L6x4x3/8x6 of the top- and seat-angle with 2L4x3.5x1/4x5.5 web-angle connections. The three parameters are 588 kip-in for the ultimate moment, 219x10<sup>3</sup> kip-in/radian for the initial connection stiffness, and 0.87 for the shape parameter. The configuration of the final connection and its  $M-\theta$  curve together with EC3 classification boundaries (ECCS, 1991) are shown in Figures 10 and 11.

### Floor Beam

Uniformly Distributed Load:

$$W = 0.2117 \text{ kip-in}$$

Maximum Moment:

$$M_u = WL^2/8 = (0.2117)(300)^2/8 = 2,381.63 \text{ kip-in}$$

Required Section Modulus:

$$Z_x = M_u/F_y = 2,381.63/36 = 66.16 \text{ in.}^3$$

Try W16x40 ( $Z_x = 72.9 \text{ in.}^3$ )

Maximum Shear:

$$V_u = WL/2 = (0.2117)(300)/2 = 31.76 \text{ kips}$$

For the shear design with given W16 beam section, 3 Rows of 3/4-in. dia. bolts of A325-N and 1/4-in. thickness of web-angle (LRFD Table 9-7, p 9-40) gives 76.7 kips which is greater than 31.76 kips. Using Equation 11, the required  $M_u$  for the floor connections is 1,312.2 kip-in. Either L6x4x3/8x6 of the top- and seat-angle with 2L4x3.5x1/2x8.5 web-angles connection, or L6x4x3/8x6 of the top- and seat-angle with 2L4x3.5x1/4x8.5 web-angles connection can be used in Figure 9. For floor connections, the final configuration and its  $M-\theta$  curve with EC3 classification boundaries are shown in Figures 12 and 13.

## 6. SUMMARY

Design tables have been developed for rapid selection of top- and seat-angle with double web-angle connections when beam sections and applied loads are known. These tables enable the engineer to determine angle sizes, configurations and the  $M-\theta$  curve directly. A step-by-step design procedure

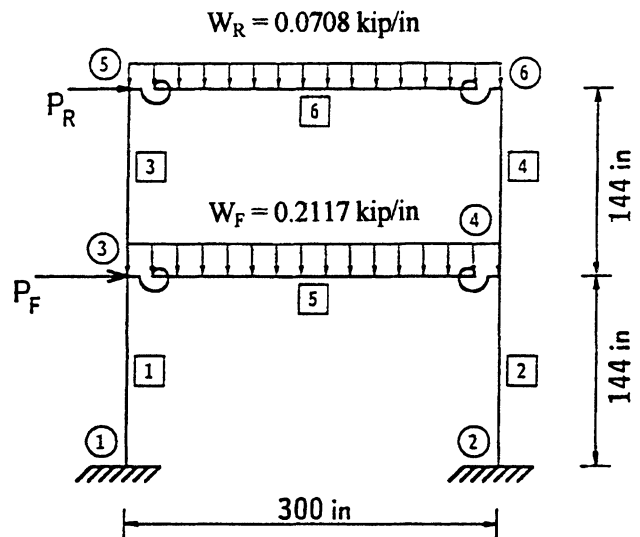


Fig. 8. One-bay two-story frame.

using these tables for the design of semi-rigid connections with LRFD has been presented. A one-bay two-story frame was also used to illustrate this procedure.

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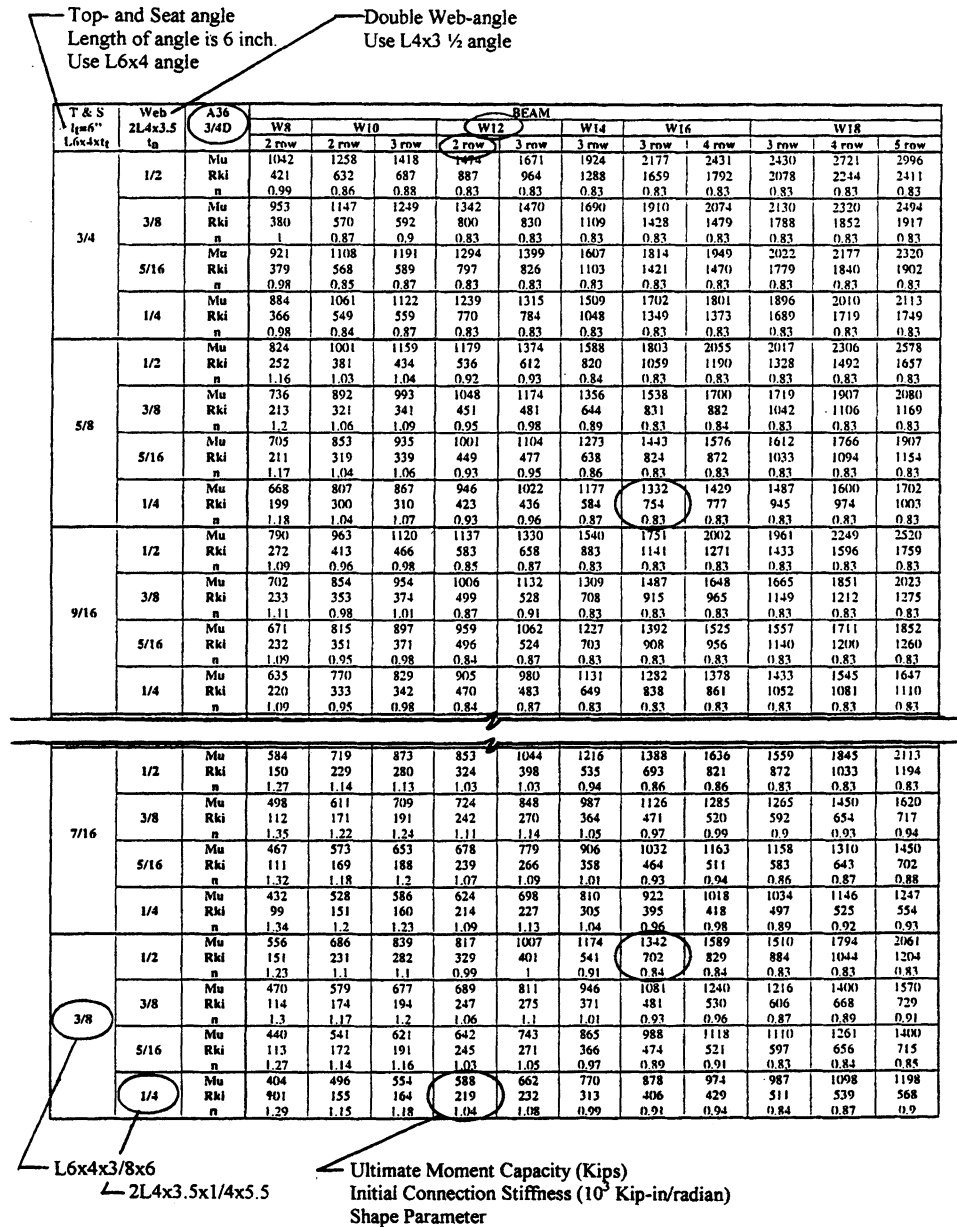


Fig. 9. Design table of semi-rigid connections.

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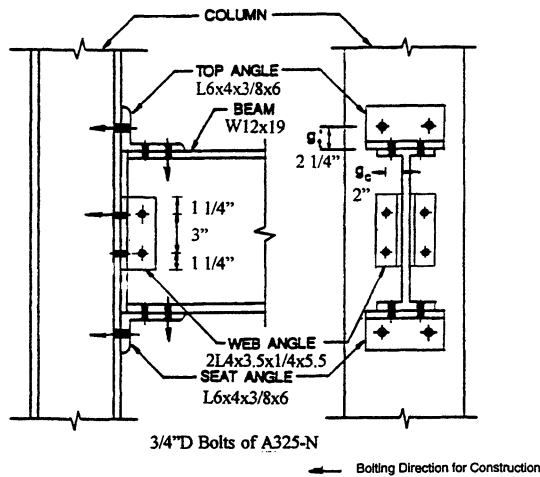


Fig. 10. Configuration of roof connections.

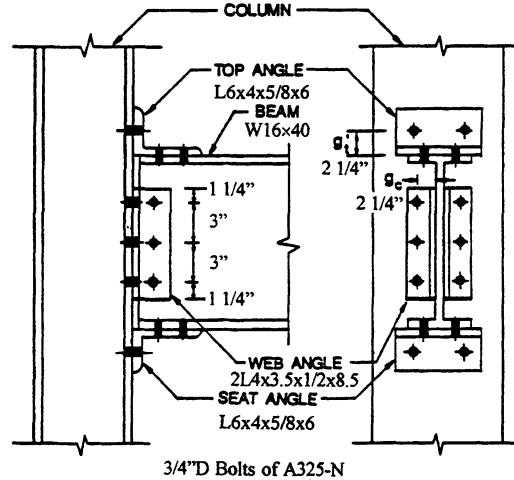


Fig. 12. Configuration of floor connections.

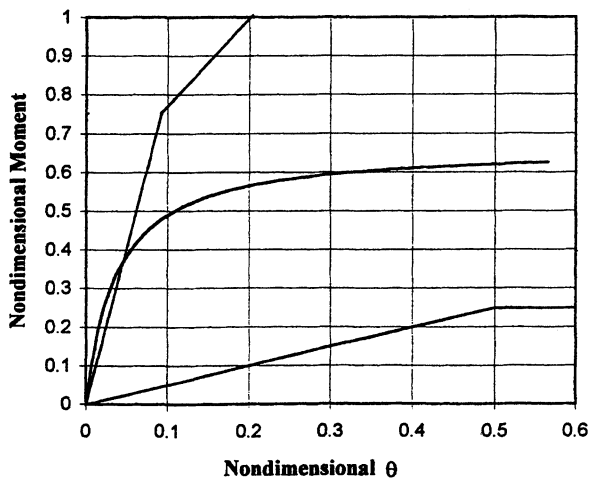


Fig. 11. Moment-rotation curve of roof connections.

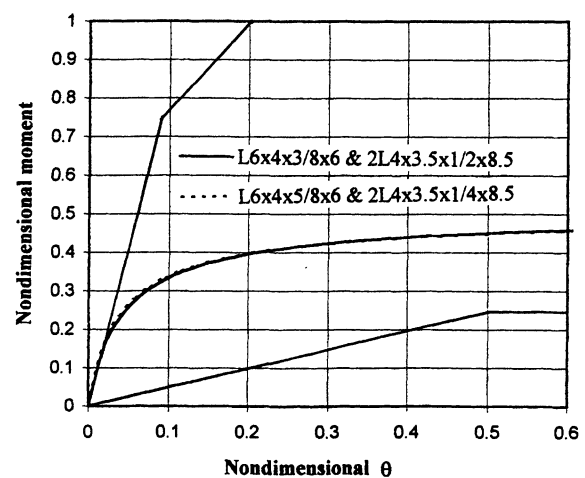


Fig. 13. Moment-Rotation curve of floor connections.



## APPENDIX 1. SOURCE FILE

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//*****
// Table.c: Table for three-parameter power
// model for Top- and Seat-angle with
// Double Web-angle
// Programmer: Yosuk Kim
// (yosuk@ce.ecn.purdue.edu)
// Last Modified: 10-26-97 (Sun)
//*****

#include <fstream.h>
#include <math.h>
#include <iomanip.h>
#include "section.h"

float g2, tt, gy, ta;
float Vot, Voa, Vpa, MU[24][43],
      RKI[24][43], NN[24][43];

float func1(float Vpt) {
float x=pow(Vpt/Vot,4)+(g2/tt)*(Vpt/Vot)-1;
return x;
}

float func2(float Vpy) {
float x=pow(Vpy/Voa,4)+(gy/ta)*(Vpy/Voa)-1;
return x;
}

float rtbis(int i, float x1, float x2){
int j=1, jmax=10000;
float dx, rt;
float fmid=(i==3)? func1(x2): func2(x2);
float f=(i==3)? func1(x1): func2(x1);
if(f<0.0) { rt=x1; dx=x2-x1; }
else { rt=x2; dx=x1-x2; }
do {
dx=0.5*dx;
float xmid=rt+dx;
fmid=(i==3)? func1(xmid): func2(xmid);
if(fmid<=0.0) rt=xmid;
if(fabs(dx)<0.00001 || fmid==0.0) return
xmid; } while(j<=jmax);
}

int main() { // Main program
int a,i,j,k,l,m,o,r,p,page,count;
float lso, ls, lt, d, lp, Sy, w, ka, gc,
      kt, ts, ks, gtt, moment[51];
float EIt, EIs, d1, g1, Mos, Vptmin,
      Vptmax, Vpt, Mpt, d2, ll, EIa, d3, g3;
float Rki, Vpymin, Vpymax, Vpu, d4, Mu,
      Theta_o, n;

// Top- and Seat-Angle used L6x4
lso=6.0; count=0;
cout<<"Type \"ls\" (6\" or 8\") : ";
cin>>ls;
cout<<"Type \"Fy\" (36 or 50 ksi) : ";
cin>>Sy;
cout<<"Type \"0\" (3/4\"D) or \" 1\"
(7/8\"D) : ";
cin>>l;

lt=ls; w=W[1];

for(i=0; i<=13; i++) {
d=BLp[i][0];
for(j=1; j<=rows[i]; j++) {
lp=(w==1.25)? BLp[i][j]:BLp[i][j]+0.5;
for(o=0; o<6; o++) {
tt=TS[o][0];
kt=TS[o][1];
ts=tt;
ks=kt;
gtt=TS[o][2+1];
for(m=0; m<4; m++) {
ta=web[m][0];
ka=web[m][1];
gc=web[m][2+1];

// Calculation for Mu and Rki
EIt=29000.0*lt*pow(tt,3)/12.0;
EIs=EIt;
d1 =d+ts/2.0+tt/2.0;
g1=gtt-w/2.0-tt/2.0;
Mos=Sy*ls*ts*ts/4.0;
Vot=Sy*lt*tt/2.0;
g2=gtt-kt-w/2.0-tt/2.0;
Vptmin=0.0;
Vptmax=Sy*lt*tt;
Vpt=rtbis(3, Vptmin, Vptmax);
Mpt=Sy*lt*tt*tt/4.0;
d2=d+ts/2.0+kt;
ll=(d-lp)/2.0;
EIa=29000.0*lp*pow(ta,3)/12.0;
d3=d/2.0+ts/2.0;
g3=gc-w/2.0-ta/2.0;
Rki=4*EIs/(lso-ks)+3.0*EIt*d1*d1/
(g1*(g1*g1+0.78*tt*tt))+6.0*EIa*d3*d3/
(g3*(g3*g3+0.78*ta*ta));
RKI[4*o+m][count]=ceil(Rki/1000);

Voa=Sy*ta/2.0;
gy=gc-ka;
Vpymin=0.0;
Vpymax=Sy*lp*ta;
Vpu=rtbis(4, Vpymin, Vpymax);
Vpa=0.5*(Vpu+Voa)*lp;
d4=lp/3.0*(2*Vpu+Voa)/(Vpu+Voa)+ll+ts/2.0;
Mu=Mos+Mpt+Vpt*d2+2*Vpa*d4;
MU[4*o+m][count]=ceil(Mu);

// Calculation for Shape parameter(n) =>
// Kishi's shape parameter
Theta_o=Mu/Rki;
if(log10(Theta_o)>-2.721)
n=1.398*log10(Theta_o)+4.631;
else n=0.827;
NN[4*o+m][count]=ceil(n*100)/100; } }
count=count+1; } }

// Print Table of summary
ofstream ofile;
ofile.open("table", ios::trunc);
for(page=0; page<4; page++) {
if(page!=3) {
ofile<<"_____
<<"_____ "<<page+1<<" page\n"<<setw(7)<<
Set[page][0]<<setw(7)

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<<Set [page] [1]<<setw(7)<<Set [page] [2]
  <<setw(7)<<Set [page] [3]<<setw(7)
<<Set [page] [4]<<setw(7)<<Set [page] [5]
  <<setw(7)<<Set [page] [6]<<setw(7)
<<Set [page] [7]<<setw(7)<<Set [page] [8]
  <<setw(7)<<Set [page] [9]<<setw(7)
<<Set [page] [10]<<"\n"<<"_____
<<"_____ \n";
for(r=0; r<24; r++) {
m=(r+1)%4;
p=11*page;
ofile<<setw(7)<<MU[r] [p]<<setw(7)<<MU[r] [p+1]
  <<setw(7)<<MU[r] [p+2]
<<setw(7)<<MU[r] [p+3]<<setw(7)<<MU[r] [p+4]
  <<setw(7)<<MU[r] [p+5]
<<setw(7)<<MU[r] [p+6]<<setw(7)<<MU[r] [p+7]
  <<setw(7)<<MU[r] [p+8]
<<setw(7)<<MU[r] [p+9]<<setw(7)<<MU[r] [p+10]
  <<"\n"<<setw(7)<<RKI[r] [p]
<<setw(7)<<RKI[r] [p+1]<<setw(7)<<RKI[r] [p+2]
  <<setw(7)<<RKI[r] [p+3]
<<setw(7)<<RKI[r] [p+4]<<setw(7)<<RKI[r] [p+5]
  <<setw(7)<<RKI[r] [p+6]
<<setw(7)<<RKI[r] [p+7]<<setw(7)<<RKI[r] [p+8]
  <<setw(7)<<RKI[r] [p+9]
<<setw(7)<<RKI[r] [p+10]<<"\n"<<setw(7)
  <<NN[r] [p]<<setw(7)<<NN[r] [p+1]
<<setw(7)<<NN[r] [p+2]<<setw(7)<<NN[r] [p+3]
  <<setw(7)<<NN[r] [p+4]
<<setw(7)<<NN[r] [p+5]<<setw(7)<<NN[r] [p+6]
  <<setw(7)<<NN[r] [p+7]
<<setw(7)<<NN[r] [p+8]<<setw(7)<<NN[r] [p+9]
  <<setw(7)<<NN[r] [p+10]
<<"\n"; } }

else {
ofile<<"_____
<<"_____ "<<page+1<<" page\n"<<setw(7)
  <<Set [page] [0]<<setw(7)
<<Set [page] [1]<<setw(7)<<Set [page] [2]
  <<setw(7)<<Set [page] [3]<<setw(7)
<<Set [page] [4]<<setw(7)<<Set [page] [5]
  <<setw(7)<<Set [page] [6]<<setw(7)
<<Set [page] [7]<<setw(7)<<Set [page] [8]
  <<setw(7)<<Set [page] [9]<<"\n"
<<"_____
<<"_____ \n";
for(r=0; r<24; r++) {
m=(r+1)%4;
p=11*page;
ofile<<setw(7)<<MU[r] [p]<<setw(7)
  <<MU[r] [p+1]<<setw(7)<<MU[r] [p+2]
<<setw(7)<<MU[r] [p+3]<<setw(7)<<MU[r] [p+4]
  <<setw(7)<<MU[r] [p+5]
<<setw(7)<<MU[r] [p+6]<<setw(7)<<MU[r] [p+7]
  <<setw(7)<<MU[r] [p+8]
<<setw(7)<<MU[r] [p+9]<<"\n"<<setw(7)
  <<RKI[r] [p]<<setw(7)<<RKI[r] [p+1]
<<setw(7)<<RKI[r] [p+2]<<setw(7)<<RKI[r] [p+3]
  <<setw(7)<<RKI[r] [p+4]
<<setw(7)<<RKI[r] [p+5]<<setw(7)<<RKI[r] [p+6]
  <<setw(7)<<RKI[r] [p+7]

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<<setw(7)<<RKI[r] [p+8]<<setw(7)<<RKI[r] [p+9]
  <<"\n"<<setw(7)<<NN[r] [p]
<<setw(7)<<NN[r] [p+1]<<setw(7)<<NN[r] [p+2]
  <<setw(7)<<NN[r] [p+3]
<<setw(7)<<NN[r] [p+4]<<setw(7)<<NN[r] [p+5]
  <<setw(7)<<NN[r] [p+6]
<<setw(7)<<NN[r] [p+7]<<setw(7)<<NN[r] [p+8]
  <<setw(7)<<NN[r] [p+9]
<<"\n"; } } }
ofile.close();
return 0;
}

//*****
// section.h: Beam and Angle information
// programmer: Yosuk Kim
// Last Modified: 2-19-97
//*****

// Bolt Diameter 3/4D or 7/8D
float W[2]={1.25,1.4375};

// Web-Angle L 4 x 3.5 x ta x ka gc(3/4D and 7/8D)
float web[4][4]={{0.5,0.9375,2.25,2.75},
{0.375,0.8125,2.25,2.5},
{0.3125,0.75,2.0,2.5},
{0.25,0.6875,2.0,2.25} };

// Top- and Seat-Angle L 6 x 4 x tt x kt gtt(3/4D and 7/8D)
float TS[6][4]={{0.75,1.25,2.5,2.75},
{0.625,1.125,2.5,2.75},
{0.5625,1.0625,2.25,2.75},
{0.5,1.0,2.25,2.5},
{0.4375,0.9375,2.25,2.5},
{0.375,0.875,2.0,2.5} };

// Beam depth and length of web-angle(lp)
float BLp[14][6]={{8.0,5.5},
{10.0,5.5,8.5},
{12.0,5.5,8.5},
{14.0,8.5},
{16.0,8.5,11.5},
{18.0,8.5,11.5,14.5},
{21.0,11.5,14.5,17.5},
{24.0,11.5,14.5,17.5,20.5},
{27.0,14.5,17.5,20.5,23.5},
{30.0,14.5,17.5,20.5,23.5,26.5},
{33.0,17.5,20.5,23.5,26.5},
{36.0,17.5,20.5,23.5,26.5},
{40.0,17.5,20.5,23.5,26.5},
{44.0,17.5,20.5,23.5,26.5} };

// Rows of web-angle
int rows[14]={1,2,2,1,2,3,3,4,4,5,4,4,4,4};

// Table setup
int Set[4][11]={{2,2,3,2,3,3,3,4,3,4,5},
{3,4,5,4,5,6,7,5,6,7,8},
{9,6,7,8,9,6,7,8,9,6,7},
{8,9,6,7,8,9,6,7,8,9} };

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APPENDIX II. DESIGN TABLE (8 CASES)

T & S t = 6-in. L6×4×t	Web 2L4×3.5 t <sub>a</sub>	A36 ¾-in. Dia.	Beam											
			W8		W10		W12		W14		W16		W18	
			2 row	3 row	2 row	3 row	2 row	3 row	2 row	3 row	2 row	3 row	2 row	3 row
¾	½	M <sub>U</sub>	1042	1258	1418	1474	1671	1924	2177	2431	2430	2721	2996	
		R <sub>KI</sub>	421	632	687	887	964	1288	1659	1792	2078	2244	2411	
		n	0.99	0.86	0.88	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	
	¾	M <sub>U</sub>	953	1147	1249	1342	1470	1690	1910	2074	2130	2320	2494	
		R <sub>KI</sub>	380	570	592	800	830	1109	1428	1479	1788	1852	1917	
		n	0.87	0.9	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	
	5/16	M <sub>U</sub>	921	1108	1191	1294	1399	1607	1814	1949	2022	2177	2320	
		R <sub>KI</sub>	379	568	589	797	826	1103	1421	1470	1779	1840	1902	
		n	0.98	0.85	0.87	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	
	¼	M <sub>U</sub>	884	1061	1122	1239	1315	1509	1702	1801	1896	2010	2113	
		R <sub>KI</sub>	366	549	559	774	784	1048	1349	1373	1689	1719	1749	
		n	0.98	0.84	0.87	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	
5/8	½	M <sub>U</sub>	824	1001	1159	1179	1374	1588	1803	2055	2017	2306	2578	
		R <sub>KI</sub>	252	381	434	536	612	820	1059	1190	1328	1492	1657	
		n	1.16	1.03	1.04	0.92	0.93	0.84	0.83	0.83	0.83	0.83	0.83	
	¾	M <sub>U</sub>	736	892	993	1048	1174	1356	1538	1700	1719	1907	2080	
		R <sub>KI</sub>	213	321	341	451	481	644	831	882	1042	1106	1169	
		n	1.2	1.06	1.09	0.95	0.98	0.89	0.83	0.84	0.83	0.83	0.83	
	5/16	M <sub>U</sub>	705	853	935	1001	1104	1273	1443	1576	1612	1766	1907	
		R <sub>KI</sub>	211	319	339	449	477	638	824	872	1033	1094	1154	
		n	1.17	1.04	1.06	0.93	0.95	0.86	0.83	0.83	0.83	0.83	0.83	
	¼	M <sub>U</sub>	668	807	867	946	1022	1177	1332	1429	1487	1600	1702	
		R <sub>KI</sub>	199	300	310	423	436	584	754	777	945	974	1003	
		n	1.18	1.04	1.07	0.93	0.96	0.87	0.83	0.83	0.83	0.83	0.83	
¾	½	M <sub>U</sub>	790	963	1120	1137	1330	1540	1751	2002	1961	2249	2520	
		R <sub>KI</sub>	272	413	466	583	658	883	1141	1271	1433	1596	1759	
		n	1.09	0.96	0.98	0.85	0.87	0.83	0.83	0.83	0.83	0.83	0.83	
	¾	M <sub>U</sub>	702	854	954	1006	1132	1309	1487	1648	1665	1851	2023	
		R <sub>KI</sub>	233	353	374	499	528	708	915	965	1149	1212	1275	
		n	1.11	0.98	1.01	0.87	0.91	0.83	0.83	0.83	0.83	0.83	0.83	
	5/16	M <sub>U</sub>	671	815	897	959	1062	1227	1392	1525	1557	1711	1852	
		R <sub>KI</sub>	232	351	371	496	524	703	908	956	1140	1200	1260	
		n	1.09	0.95	0.98	0.84	0.87	0.83	0.83	0.83	0.83	0.83	0.83	
	¼	M <sub>U</sub>	635	770	829	905	980	1131	1282	1378	1433	1545	1647	
		R <sub>KI</sub>	220	333	342	470	483	649	838	861	1052	1081	1110	
		n	1.09	0.95	0.98	0.84	0.87	0.83	0.83	0.83	0.83	0.83	0.83	
½	½	M <sub>U</sub>	686	840	995	994	1186	1377	1568	1818	1760	2046	2316	
		R <sub>KI</sub>	202	307	359	434	508	683	884	1013	1111	1273	1435	
		n	1.19	1.05	1.06	0.95	0.96	0.87	0.83	0.83	0.83	0.83	0.83	
	¾	M <sub>U</sub>	599	732	831	865	989	1147	1306	1466	1464	1650	1821	
		R <sub>KI</sub>	163	248	268	351	379	510	660	709	829	891	954	
		n	1.23	1.1	1.13	0.99	1.02	0.93	0.86	0.88	0.83	0.83	0.83	
	5/16	M <sub>U</sub>	568	693	774	818	920	1066	1211	1343	1357	1510	1650	
		R <sub>KI</sub>	162	246	265	348	375	504	653	700	820	880	939	
		n	1.21	1.07	1.09	0.96	0.99	0.9	0.83	0.84	0.83	0.83	0.83	
	¼	M <sub>U</sub>	532	648	707	763	838	970	1101	1197	1233	1345	1446	
		R <sub>KI</sub>	150	228	237	322	336	451	583	606	733	762	790	
		n	1.21	1.08	1.11	0.97	1	0.91	0.83	0.86	0.83	0.83	0.83	
7/16	½	M <sub>U</sub>	584	719	873	853	1044	1216	1388	1636	1559	1845	2113	
		R <sub>KI</sub>	150	229	280	324	398	535	693	821	872	1033	1194	
		n	1.27	1.14	1.13	1.03	1.03	0.94	0.86	0.86	0.83	0.83	0.83	
	¾	M <sub>U</sub>	498	611	709	724	848	987	1126	1285	1265	1450	1620	
		R <sub>KI</sub>	112	171	191	242	270	364	471	520	592	654	717	
		n	1.35	1.22	1.24	1.11	1.14	1.05	0.97	0.99	0.9	0.93	0.94	
	5/16	M <sub>U</sub>	467	573	653	678	779	906	1032	1163	1158	1310	1450	
		R <sub>KI</sub>	111	169	188	239	266	358	464	511	583	643	702	
		n	1.32	1.18	1.2	1.07	1.09	1.01	0.93	0.94	0.86	0.87	0.88	
	¼	M <sub>U</sub>	432	528	586	624	698	810	922	1018	1034	1146	1247	
		R <sub>KI</sub>	99	151	160	214	227	305	395	418	497	525	554	
		n	1.34	1.2	1.23	1.09	1.13	1.04	0.96	0.98	0.89	0.92	0.93	
¾	½	M <sub>U</sub>	556	686	839	817	1007	1174	1342	1589	1510	1794	2061	
		R <sub>KI</sub>	151	231	282	329	401	541	702	829	884	1044	1204	
		n	1.23	1.1	1.1	0.99	1	0.91	0.84	0.84	0.83	0.83	0.83	
	¾	M <sub>U</sub>	470	579	677	689	811	946	1081	1240	1216	1400	1570	
		R <sub>KI</sub>	114	174	194	247	275	371	481	530	606	668	729	
		n	1.3	1.17	1.2	1.06	1.1	1.01	0.93	0.96	0.87	0.89	0.91	
	5/16	M <sub>U</sub>	440	541	621	642	743	865	988	1118	1110	1261	1400	
		R <sub>KI</sub>	113	172	191	245	271	366	474	521	597	656	715	
		n	1.27	1.14	1.16	1.03	1.05	0.97	0.89	0.91	0.83	0.84	0.85	
	¼	M <sub>U</sub>	404	496	554	588	662	770	878	974	987	1098	1198	
		R <sub>KI</sub>	101	155	164	219	232	313	406	429	511	539	568	
		n	1.29	1.15	1.18	1.04	1.08	0.99	0.91	0.94	0.84	0.87	0.9	

T & S t = 6-in. L6×4×t	Web 2L4×3.5 t <sub>a</sub>	A36 ¾-in. Dia.	Beam										
			W21			W24				W27			
			3 row	4 row	5 row	3 row	4 row	5 row	6 row	7 row	5 row	6 row	7 row
¾	½	M <sub>U</sub>	3157	3487	3800	3592	3977	4346	4698	4468	4893	5300	5691
		R <sub>KI</sub>	3018	3242	3466	3906	4196	4487	4777	5274	5639	6004	6369
		n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
	¾	M <sub>U</sub>	2688	2901	3098	3057	3307	3543	3764	3714	3988	4247	4491
		R <sub>KI</sub>	2491	2577	2664	3223	3336	3448	3560	4192	4333	4474	4615
		n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
	5/16	M <sub>U</sub>	2520	2695	2856	2864	3069	3263	3443	3444	3669	3881	4081
		R <sub>KI</sub>	2474	2557	2639	3202	3309	3416	3523	4159	4293	4427	4562
		n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
	¼	M <sub>U</sub>	2324	2452	2568	2639	2790	2931	3060	3129	3293	3447	3590
		R <sub>KI</sub>	2311	2351	2391	3043	3094	3146	3248	3895	3954	4019	4119
		n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
5/8	½	M <sub>U</sub>	2684	3011	3322	3061	3444	3811	4160	3877	4300	4705	5093
		R <sub>KI</sub>	2011	2232	2454	2606	2894	3181	3468	3641	4002	4364	4726
		n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
	¾	M <sub>U</sub>	2218	2429	2625	2529	2778	3012	3231	3127	3399	3657	3899
		R <sub>KI</sub>	1490	1575	1661	1930	2042	2153	2264	2568	2708	2848	2988
		n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
	5/16	M <sub>U</sub>	2051	2224	2385	2337	2541	2733	2913	2858	3082	3293	3491
		R <sub>KI</sub>	1473	1555	1637	1910	2015	2121	2227	2535	2669	2832	2935
		n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
	¼	M <sub>U</sub>	1856	1983	2098	2113	2264	2403	2532	2544	2708	2861	3002
		R <sub>KI</sub>	1312	1352	1391	1700	1752	1803	1854	2203	2268	2332	2397
		n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
¾	½	M <sub>U</sub>	2621	2947	3257	2992	3374	3739	4088	3801	4222	4626	5013
		R <sub>KI</sub>	2153	2373	2593	2792	3078	3364	3650	3876	4236	4596	4956
		n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
	¾	M <sub>U</sub>	2156	2366	2561	2461	2709	2943	3161	3052			

T & S I <sub>t</sub> = 6-in. L6×4×t <sub>f</sub>	Web 2L4×3.5 t <sub>a</sub>	A36 ¾-in. Dia.	Beam													
			W27				W30				W33				W36	
			9 row	6 row	7 row	8 row	9 row	6 row	7 row	8 row	9 row	6 row	7 row	8 row	6 row	7 row
			M <sub>U</sub>	R <sub>KI</sub>	n	0.83	M <sub>U</sub>	R <sub>KI</sub>	n	0.83	M <sub>U</sub>	R <sub>KI</sub>	n	0.83	M <sub>U</sub>	R <sub>KI</sub>
¾	½	M <sub>U</sub>	4959	5439	5902	6348	6777	5985	6504	7006	7491	6532	7106			
		R <sub>KI</sub>	6475	6923	7371	7819	8267	8338	8878	9418	9958	9885	10526			
		n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	
	⅜	M <sub>U</sub>	4121	4433	4731	5013	5260	4878	5214	5535	5840	5324	5697			
		R <sub>KI</sub>	5146	5319	5493	5666	5839	6407	6616	6824	7033	7595	7843			
		n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	
	⅙	M <sub>U</sub>	3819	4075	4319	4550	4769	4482	4757	5020	5270	4888	5195			
		R <sub>KI</sub>	5105	5270	5435	5600	5765	6347	6546	6745	6943	7525	7760			
		n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	
	¼	M <sub>U</sub>	3467	3656	3834	4000	4156	4018	4220	4411	4591	4381	4607			
		R <sub>KI</sub>	4694	4774	4853	4933	5013	5749	5845	5941	6038	6816	6930			
		n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	
⅝	½	M <sub>U</sub>	4311	4788	5249	5693	6120	5277	5793	6293	6775	5766	6338			
		R <sub>KI</sub>	4474	4918	5363	5807	6252	5928	6464	7000	7536	7033	7668			
		n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	
	⅜	M <sub>U</sub>	3476	3787	4083	4363	4629	4174	4508	4827	5131	4562	4934			
		R <sub>KI</sub>	3156	3328	3500	3672	3844	4011	4218	4426	4633	4758	5004			
		n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	
	⅙	M <sub>U</sub>	3175	3431	3673	3903	4120	3779	4053	4315	4563	4128	4434			
		R <sub>KI</sub>	3115	3279	3442	3606	3770	3952	4149	4346	4544	4688	4922			
		n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	
	¼	M <sub>U</sub>	2825	3013	3189	3355	3510	3317	3518	3708	3887	3622	3847			
		R <sub>KI</sub>	2707	2786	2865	2945	3024	3358	3454	3549	3644	3984	4097			
		n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	
¾	½	M <sub>U</sub>	4228	4704	5164	5607	6033	5187	5702	6201	6682	5670	6241			
		R <sub>KI</sub>	4765	5207	5650	6093	6536	6279	6813	7347	7881	7452	8085			
		n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	
	⅜	M <sub>U</sub>	3395	3705	4000	4280	4545	4087	4420	4738	5041	4468	4839			
		R <sub>KI</sub>	3452	3624	3795	3966	4137	4369	4576	4782	4989	5185	5430			
		n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	
	⅙	M <sub>U</sub>	3095	3350	3592	3821	4037	3692	3966	4226	4475	4035	4340			
		R <sub>KI</sub>	3412	3575	3738	3901	4064	4311	4507	4703	4900	5115	5348			
		n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	
	¼	M <sub>U</sub>	2746	2933	3109	3274	3429	3231	3432	3621	3800	3530	3755			
		R <sub>KI</sub>	3006	3084	3163	3242	3321	3719	3814	3909	4004	4413	4526			
		n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	
½	½	M <sub>U</sub>	3908	4383	4841	5283	5708	4837	5351	5848	6328	5298	5860			
		R <sub>KI</sub>	3897	4338	4779	5220	5661	5233	5765	6297	6829	6212	6843			
		n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	
	⅜	M <sub>U</sub>	3077	3386	3680	3959	4223	3738	4070	4388	4690	4090	4461			
		R <sub>KI</sub>	2590	2761	2931	3102	3272	3330	3536	3742	3947	3953	4197			
		n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	
	⅙	M <sub>U</sub>	2777	3031	3272	3501	3717	3345	3617	3877	4125	3658	3962			
		R <sub>KI</sub>	2550	2712	2874	3037	3199	3271	3467	3663	3859	3883	4116			
		n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	
	¼	M <sub>U</sub>	2428	2615	2791	2956	3110	2885	3085	3274	3452	3154	3378			
		R <sub>KI</sub>	2145	2224	2302	2381	2459	2682	2777	2872	2966	3184	3296			
		n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	
⅞	½	M <sub>U</sub>	3588	4062	4519	4960	5383	4486	4999	5495	5974	4911	5479			
		R <sub>KI</sub>	3252	3692	4131	4570	5009	4455	4985	5515	6045	5290	5919			
		n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	
	⅜	M <sub>U</sub>	2759	3067	3360	3639	3902	3390	3722	4038	4340	3713	4083			
		R <sub>KI</sub>	1951	2121	2290	2460	2630	2559	2764	2969	3174	3038	3282			
		n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	
	⅙	M <sub>U</sub>	2460	2713	2954	3182	3397	2997	3270	3529	3776	3282	3585			
		R <sub>KI</sub>	1911	2072	2234	2395	2557	2501	2696	2891	3085	2969	3201			
		n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	
	¼	M <sub>U</sub>	2112	2298	2473	2638	2791	2538	2738	2926	3104	2779	3002			
		R <sub>KI</sub>	1508	1586	1664	1742	1820	1913	2008	2102	2196	2272	2384			
		n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	
¾	½	M <sub>U</sub>	3512	3985	4441	4881	5303	4404	4915	5410	5888	4822	5389			
		R <sub>KI</sub>	3288	3725	4162	4600	5037	4497	5025	5553	6081	5341	5969			
		n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	
	⅜	M <sub>U</sub>	2685	2992	3285	3562	3825	3309	3640	3956	4257	3627	3996			
		R <sub>KI</sub>	1991	2160	2330	2499	2668	2608	2812	3017	3221	3098	3340			
		n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	
	⅙	M <sub>U</sub>	2387	2639	2879	3106	3321	2918	3189	3448	3694	3193	3499			
		R <sub>KI</sub>	1951	2112	2273	2434	2595	2550	2744	2938	3133	3029	3260			
		n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	
	¼	M <sub>U</sub>	2039	2225	2400	2564	2717	2460	2658	2846	3023	2694	2917			
		R <sub>KI</sub>	1550	1628	1706	1784	1861	1965	2059	2153	2247	2334	2446			
		n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	

T & S I <sub>t</sub> = 6-in. L6×4×t <sub>f</sub>	Web 2L4×3.5 t <sub>a</sub>	A36 ¾-in. Dia.	Beam											
			W36			W40			W44					
			8 row	9 row	6 row	7 row	8 row	9 row	6 row	7 row	8 row	9 row		
			M <sub>U</sub>	R <sub>KI</sub>	n	M <sub>U</sub>	R <sub>KI</sub>	n	M <sub>U</sub>	R <sub>KI</sub>	n	M <sub>U</sub>	R <sub>KI</sub>	n
¾	½	M <sub>U</sub>	7664	8204	7260	7909	8540	9155	7989	8712	9417	10106		
		R <sub>KI</sub>	11166	11806	12153	12940	13728	14515	14655	15604	16554	17503		
		n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
	⅜	M <sub>U</sub>	6056	6400	5917	6342	6752	7147	6511	6986	7447	7893		
		R <sub>KI</sub>	8091	8338	9337	9642	9946	10251	11259	11626	11994	12361		
		n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
	⅙	M <sub>U</sub>	5490	5771	5430	5779	6116	6439	5972	6363	6742	7108		
		R <sub>KI</sub>	7996	8231	9251	9540	9830	10120	11155	11504	11853	12203		
		n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
	¼	M <sub>U</sub>	4822	5026	4864	5122	5370	5606	5347	5638	5917	6186		
		R <sub>KI</sub>	7044	7157	8379	8519	8659	8799	10103	10272	10441	10610		
		n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
⅝	½	M <sub>U</sub>	6893	7431	6417	7063	7693	8305	7069	7789	8493	9179		
		R <sub>KI</sub>	8304	8940	8652	9434	10217	10999	10439	11383	12327	13271		
		n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
	⅜	M <sub>U</sub>	5291	5633	5078	5501	5910	6303	5595	6069	6528	6972		
		R <sub>KI</sub>	5250	54										



T & S $t_f = 6\text{-in.}$ $L_6 \times 4 \times t_f$	Web $2L_4 \times 3.5$ $t_a$	A36 $\frac{3}{4}\text{-in.}$ Dia.	Beam										
			W27		W30			W33			W36		
			9 row	6 row	7 row	8 row	9 row	6 row	7 row	8 row	9 row	6 row	7 row
$\frac{3}{4}$	$\frac{1}{2}$	$M_U$	4654	5075	5476	5858	6221	5592	6046	6479	6893	6110	6615
		$R_{Kj}$	4370	4584	4798	5012	5227	5521	5779	6037	6295	6545	6851
		$n$	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
	$\frac{3}{8}$	$M_U$	3958	4252	4530	4792	5038	4683	4998	5297	5580	5113	5465
		$R_{Kj}$	3940	4069	4197	4326	4454	4900	5055	5210	5364	5809	5992
		$n$	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
	$\frac{5}{16}$	$M_U$	3609	3838	4054	4256	4444	4225	4471	4702	4920	4612	4888
		$R_{Kj}$	3654	3725	3796	3867	3938	4486	4572	4657	4743	5318	5419
		$n$	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
	$\frac{1}{4}$	$M_U$	3316	3494	3661	3817	3961	3843	4033	4212	4380	4192	4406
		$R_{Kj}$	3580	3637	3693	3749	3806	4380	4448	4516	4583	5192	5272
		$n$	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
$\frac{5}{8}$	$\frac{1}{2}$	$M_U$	4000	4419	4818	5198	5559	4878	5329	5761	6173	5338	5840
		$R_{Kj}$	2844	3057	3269	3482	3694	3684	3941	4197	4453	4371	4675
		$n$	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
	$\frac{3}{8}$	$M_U$	3308	3600	3876	4137	4382	3972	4286	4583	4865	4344	4695
		$R_{Kj}$	2419	2546	2673	2801	2928	3068	3222	3376	3529	3640	3822
		$n$	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
	$\frac{5}{16}$	$M_U$	2960	3188	3402	3603	3790	3517	3761	3991	4208	3845	4119
		$R_{Kj}$	2134	2205	2275	2346	2416	2657	2742	2827	2912	3152	3253
		$n$	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
	$\frac{1}{4}$	$M_U$	2668	2845	3011	3166	3309	3136	3325	3503	3670	3426	3639
		$R_{Kj}$	2061	2117	2173	2229	2285	2552	2619	2687	2754	3027	3107
		$n$	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
$\frac{3}{16}$	$\frac{1}{2}$	$M_U$	3678	4096	4495	4873	5233	4526	4976	5407	5818	4957	5458
		$R_{Kj}$	2310	2521	2733	2945	3156	3040	3295	3550	3806	3607	3910
		$n$	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
	$\frac{3}{8}$	$M_U$	2987	3279	3554	3814	4058	3622	3935	4232	4513	3965	4315
		$R_{Kj}$	1886	2012	2139	2266	2393	2426	2579	2732	2885	2879	3060
		$n$	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
	$\frac{5}{16}$	$M_U$	2640	2868	3082	3282	3468	3167	3411	3641	3857	3467	3740
		$R_{Kj}$	1602	1673	1743	1813	1883	2017	2101	2186	2271	2393	2493
		$n$	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
	$\frac{1}{4}$	$M_U$	2349	2526	2691	2846	2988	2787	2976	3154	3320	3049	3261
		$R_{Kj}$	1530	1586	1641	1697	1753	1912	1979	2046	2113	2268	2348
		$n$	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
$\frac{1}{2}$	$\frac{1}{2}$	$M_U$	3598	4015	4413	4790	5149	4439	4888	5318	5727	4864	5364
		$R_{Kj}$	2357	2567	2778	2989	3200	3097	3351	3605	3860	3676	3978
		$n$	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
	$\frac{3}{8}$	$M_U$	2909	3200	3475	3734	3977	3537	3849	4145	4425	3874	4223
		$R_{Kj}$	1934	2061	2187	2313	2440	2485	2638	2790	2943	2950	3131
		$n$	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
	$\frac{5}{16}$	$M_U$	2563	2790	3003	3202	3388	3083	3326	3555	3771	3377	3649
		$R_{Kj}$	1652	1722	1792	1862	1932	2077	2162	2246	2330	2466	2566
		$n$	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
	$\frac{1}{4}$	$M_U$	2272	2448	2614	2767	2910	2704	2892	3070	3236	2959	3171
		$R_{Kj}$	1580	1635	1691	1746	1802	1973	2040	2106	2173	2341	2421
		$n$	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
$\frac{7}{16}$	$\frac{1}{2}$	$M_U$	3286	3702	4098	4475	4832	4097	4545	4974	5382	4493	4992
		$R_{Kj}$	1885	2095	2305	2515	2725	2528	2781	3034	3288	3001	3302
		$n$	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
	$\frac{3}{8}$	$M_U$	2598	2888	3162	3421	3663	3197	3508	3803	4083	3505	3854
		$R_{Kj}$	1464	1590	1716	1842	1967	1919	2070	2222	2374	2278	2458
		$n$	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
	$\frac{5}{16}$	$M_U$	2253	2479	2692	2890	3075	2744	2986	3215	3429	3009	3281
		$R_{Kj}$	1183	1253	1323	1392	1462	1512	1596	1680	1764	1795	1895
		$n$	0.83	0.86	0.87	0.89	0.89	0.83	0.83	0.84	0.85	0.83	0.83
	$\frac{1}{4}$	$M_U$	1963	2139	2303	2456	2598	2365	2553	2730	2896	2592	2804
		$R_{Kj}$	1111	1167	1222	1277	1332	1408	1474	1541	1608	1671	1750
		$n$	0.83	0.83	0.83	0.84	0.85	0.83	0.83	0.83	0.83	0.83	0.83
$\frac{3}{8}$	$\frac{1}{2}$	$M_U$	3002	3416	3812	4187	4543	3786	4233	4660	5067	4155	4653
		$R_{Kj}$	1548	1757	1966	2175	2384	2121	2373	2625	2878	2519	2819
		$n$	0.84	0.85	0.84	0.84	0.83	0.83	0.83	0.83	0.83	0.83	0.83
	$\frac{3}{8}$	$M_U$	2315	2604	2878	3135	3377	2887	3197	3492	3771	3169	3517
		$R_{Kj}$	1129	1254	1379	1505	1630	1514	1665	1816	1968	1798	1978
		$n$	0.88	0.89	0.89	0.89	0.88	0.83	0.84	0.84	0.84	0.83	0.83
	$\frac{5}{16}$	$M_U$	1971	2196	2408	2606	2790	2435	2677	2905	3119	2674	2945
		$R_{Kj}$	849	918	988	1057	1127	1109	1192	1276	1360	1317	1416
		$n$	0.95	0.97	0.98	0.99	0.99	0.92	0.93	0.94	0.95	0.87	0.89
	$\frac{1}{4}$	$M_U$	1681	1857	2021	2173	2315	2057	2245	2421	2586	2258	2469
		$R_{Kj}$	777	832	887	942	997	1005	1071	1138	1204	1193	1272
		$n$	0.91	0.93	0.94	0.95	0.95	0.88	0.89	0.9	0.91	0.83	0.84

T & S $t_f = 6\text{-in.}$ $L_6 \times 4 \times t_f$	Web $2L_4 \times 3.5$ $t_a$	A36 $\frac{3}{4}\text{-in.}$ Dia.	Beam									
			W36		W40			W44				
			8 row	9 row	6 row	7 row	8 row	9 row	6 row	7 row	8 row	9 row
$\frac{3}{4}$	$\frac{1}{2}$	$M_U$	7100	7566	8000	7374	7928	8462	7490	8133	8756	9359
		$R_{Kj}$	7157	7463	8046	8422	8798	9175	9702	10156	10609	11063
		$n$	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
	$\frac{3}{8}$	$M_U$	5802	6122	5687	6089	6475	6845	6262	6713	7148	7568
		$R_{Kj}$	6176	6359	7141	7367	7592	7818	8611	8883	9155	9427
		$n$	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
	$\frac{5}{16}$	$M_U$	5149	5396	5128	5443	5744	6032	5644	5999	6340	6667
		$R_{Kj}$	5521	5622	6537	6662	6787	6912	7882	8033	8183	8334
		$n$	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
	$\frac{1}{4}$	$M_U$	4608	4800	4657	4902	5136	5359	5122	5399	5664	5918
		$R_{Kj}$	5353	5433	6382	6481	6580	6679	7696	7815	7934	8054
		$n$	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
$\frac{5}{8}$	$\frac{1}{2}$	$M_U$	6323	6787	5950	6521	7073	7606	6562	7203	7823	8424
		$R_{Kj}$	4978	5282	5377	5751	6125	6499	6487	6938	7389	7841
		$n$	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
	$\frac{3}{8}$	$M_U$	5030	5349								

T & S t <sub>r</sub> = 6-in. L6-x4-x <sub>t</sub>	Web 2L4-x3.5 t <sub>a</sub>	A36 3/4-in. Dia.	Beam											
			W8		W10		W12		W14		W16		W18	
			2 row	3 row	2 row	3 row	2 row	3 row	2 row	3 row	2 row	3 row	2 row	3 row
3/4	1/2	M <sub>U</sub>	1447	1747	1969	2047	2321	2672	3024	3377	3375	3780	4161	
		R <sub>KI</sub>	421	632	687	887	964	1288	1659	1792	2078	2244	2411	
		n	1.19	1.06	1.08	0.95	0.98	0.89	0.83	0.83	0.83	0.83	0.83	
	3/8	M <sub>U</sub>	1323	1593	1735	1864	2041	2347	2653	2880	2959	3221	3463	
		R <sub>KI</sub>	380	570	592	800	830	1109	1428	1479	1788	1852	1917	
		n	1.2	1.07	1.1	0.96	0.99	0.9	0.83	0.85	0.83	0.83	0.83	
	5/16	M <sub>U</sub>	1279	1538	1654	1797	1943	2231	2520	2706	2808	3024	3222	
		R <sub>KI</sub>	379	568	589	797	826	1103	1421	1470	1779	1840	1902	
		n	1.18	1.05	1.07	0.94	0.96	0.87	0.83	0.83	0.83	0.83	0.83	
	1/4	M <sub>U</sub>	1227	1474	1558	1720	1827	2096	2364	2501	2633	2792	2935	
		R <sub>KI</sub>	366	549	559	770	784	1048	1349	1373	1689	1719	1749	
		n	1.18	1.04	1.06	0.93	0.96	0.86	0.83	0.83	0.83	0.83	0.83	
5/8	1/2	M <sub>U</sub>	1144	1391	1610	1637	1908	2206	2504	2853	2802	3203	3581	
		R <sub>KI</sub>	252	381	434	536	612	820	1059	1190	1328	1492	1657	
		n	1.36	1.23	1.24	1.12	1.13	1.04	0.96	0.97	0.9	0.91	0.91	
	3/8	M <sub>U</sub>	1022	1239	1378	1456	1631	1883	2136	2361	2388	2649	2888	
		R <sub>KI</sub>	213	321	341	451	481	644	831	882	1042	1106	1169	
		n	1.4	1.26	1.29	1.15	1.18	1.09	1.02	1.04	0.95	0.97	0.99	
	5/16	M <sub>U</sub>	978	1184	1299	1390	1534	1769	2004	2188	2239	2452	2649	
		R <sub>KI</sub>	211	319	339	449	477	638	824	872	1033	1094	1154	
		n	1.37	1.24	1.26	1.13	1.15	1.06	0.98	1	0.91	0.93	0.95	
	1/4	M <sub>U</sub>	927	1120	1204	1313	1419	1634	1849	1984	2065	2222	2364	
		R <sub>KI</sub>	199	300	310	423	436	584	754	777	945	974	1003	
		n	1.38	1.24	1.27	1.13	1.16	1.07	0.99	1.01	0.92	0.94	0.96	
9/16	1/2	M <sub>U</sub>	1097	1337	1555	1578	1847	2139	2432	2780	2724	3124	3500	
		R <sub>KI</sub>	272	413	466	583	658	883	1141	1271	1433	1596	1759	
		n	1.29	1.16	1.17	1.05	1.07	0.98	0.9	0.92	0.83	0.85	0.86	
	3/8	M <sub>U</sub>	975	1186	1325	1398	1572	1818	2065	2289	2312	2571	2810	
		R <sub>KI</sub>	233	353	374	499	528	708	915	965	1149	1212	1275	
		n	1.31	1.18	1.21	1.07	1.11	1.01	0.94	0.97	0.87	0.9	0.92	
	5/16	M <sub>U</sub>	932	1132	1246	1332	1475	1704	1934	2117	2163	2376	2571	
		R <sub>KI</sub>	232	351	371	496	524	703	908	956	1140	1200	1260	
		n	1.29	1.15	1.18	1.04	1.07	0.98	0.9	0.92	0.83	0.86	0.88	
	1/4	M <sub>U</sub>	882	1069	1151	1256	1361	1570	1780	1914	1990	2146	2288	
		R <sub>KI</sub>	220	333	342	470	483	649	838	861	1052	1081	1110	
		n	1.29	1.15	1.18	1.04	1.07	0.98	0.9	0.93	0.83	0.86	0.88	
1/2	1/2	M <sub>U</sub>	952	1166	1382	1380	1647	1913	2178	2525	2444	2842	3216	
		R <sub>KI</sub>	202	307	359	434	508	683	884	1013	1111	1273	1435	
		n	1.39	1.25	1.26	1.14	1.16	1.07	0.99	1	0.92	0.93	0.93	
	3/8	M <sub>U</sub>	832	1016	1154	1201	1373	1593	1813	2036	2033	2291	2529	
		R <sub>KI</sub>	163	248	268	351	379	510	660	709	829	891	954	
		n	1.43	1.3	1.33	1.19	1.22	1.13	1.06	1.08	0.99	1.02	1.03	
	5/16	M <sub>U</sub>	789	962	1075	1135	1277	1480	1682	1865	1885	2097	2291	
		R <sub>KI</sub>	162	246	265	348	375	504	653	700	820	880	939	
		n	1.4	1.27	1.29	1.16	1.19	1.1	1.02	1.04	0.95	0.97	0.98	
	1/4	M <sub>U</sub>	739	899	981	1060	1164	1347	1529	1663	1712	1868	2008	
		R <sub>KI</sub>	150	228	237	322	336	451	583	606	733	762	790	
		n	1.41	1.28	1.3	1.17	1.2	1.11	1.03	1.05	0.96	0.99	1.01	
7/16	1/2	M <sub>U</sub>	811	998	1212	1185	1450	1689	1927	2272	2165	2562	2935	
		R <sub>KI</sub>	150	229	280	324	398	535	693	821	872	1033	1194	
		n	1.47	1.34	1.33	1.23	1.23	1.14	1.06	1.06	0.99	0.99	0.99	
	3/8	M <sub>U</sub>	691	849	985	1006	1178	1371	1563	1785	1756	2013	2250	
		R <sub>KI</sub>	112	171	191	242	270	364	471	520	592	654	717	
		n	1.55	1.42	1.44	1.31	1.34	1.25	1.17	1.19	1.1	1.12	1.14	
	5/16	M <sub>U</sub>	649	795	907	941	1082	1258	1433	1615	1608	1819	2013	
		R <sub>KI</sub>	111	169	188	239	266	358	464	511	583	643	702	
		n	1.52	1.38	1.4	1.27	1.29	1.2	1.13	1.14	1.06	1.07	1.08	
	1/4	M <sub>U</sub>	599	733	814	866	969	1125	1281	1413	1436	1591	1731	
		R <sub>KI</sub>	99	151	160	214	227	305	395	418	497	525	554	
		n	1.54	1.4	1.43	1.29	1.32	1.23	1.16	1.18	1.09	1.12	1.13	
3/8	1/2	M <sub>U</sub>	771	953	1165	1134	1398	1631	1864	2207	2096	2491	2863	
		R <sub>KI</sub>	151	231	282	329	401	541	702	829	884	1044	1204	
		n	1.43	1.3	1.3	1.19	1.2	1.11	1.04	1.04	0.97	0.97	0.97	
	3/8	M <sub>U</sub>	652	804	939	956	1127	1314	1501	1722	1689	1945	2180	
		R <sub>KI</sub>	114	174	194	247	275	371	481	530	606	668	729	
		n	1.5	1.37	1.4	1.26	1.3	1.21	1.13	1.16	1.06	1.09	1.11	
	5/16	M <sub>U</sub>	611	751	862	892	1032	1202	1372	1553	1541	1752	1944	
		R <sub>KI</sub>	113	172	191	245	271	366	474	521	597	656	715	
		n	1.47	1.34	1.36	1.23	1.25	1.16	1.09	1.11	1.02	1.04	1.05	
	1/4	M <sub>U</sub>	561	689	769	817	920	1070	1220	1352	1370	1524	1664	
		R <sub>KI</sub>	101	155	164	219	232	313	406	429	511	539	568	
		n	1.49	1.35	1.38	1.24	1.28	1.19	1.11	1.14	1.04	1.07	1.09	

T & S t <sub>r</sub> = 6-in. L6-x4-x <sub>t</sub>	Web 2L4-x3.5 t <sub>a</sub>	A36 3/4-in. Dia.	Beam										
			W21			W24				W27			
			3 row	4 row	5 row	4 row	5 row	6 row	7 row	5 row	6 row	7 row	8 row
3/4	1/2	M <sub>U</sub>	4384	4842	5277	4988	5524	6036	6525	6206	6795	7361	7903
		R <sub>KI</sub>	3018	3242	3466	3906	4196	4487	4777	5274	5639	6004	6369
		n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
	3/8	M <sub>U</sub>	3733	4028	4303	4245	4593	4921	5227	5159	5539	5899	6238
		R <sub>KI</sub>	2491	2577	2664	3223	3336	3448	3560	4192	4333	4474	4615
		n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
	5/16	M <sub>U</sub>	3500	3743	3967	3977	4263	4531	4782	4783	5096	5390	5668
		R <sub>KI</sub>	2474	2557	2639	3202	3309	3416	3523	4159	4293	4427	4562
		n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
	1/4	M <sub>U</sub>	3228	3405	3567	3665	3875	4070	4250	4345	4574	4787	4986
		R <sub>KI</sub>	2311	2351	2391	2991	3043	3094	3146	3824	3889	3954	4019
		n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
5/8	1/2	M <sub>U</sub>	3727	4182	4614	4251	4784	5293	5778	5385	5971	6534	7073
		R <sub>KI</sub>	2011	2232	2454	2606	2894	3181	3468	3641	4002	4364	4726
		n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
	3/8	M <sub>U</sub>	3080	3373	3645	3512	3858	4183	4488	4343	4721	5079	5415
		R <sub>KI</sub>	1490	1575	1661	1930	2042	2153	2264	2568	2708	2848	2988
		n	0.88	0.9	0.92	0.83	0.83	0.85	0.86	0.83	0.83	0.83	0.83
	5/16	M <sub>U</sub>	2849	3089	3312	3245	3529	3796	4045	3970	4280	4573	4848
		R <sub>KI</sub>	1473	1555	1637	1910	2015	2121	2227	2535	2669	2802	2935
		n	0.84	0.86	0.87	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
	1/4	M <sub>U</sub>	2578	2754	2914	2935	3144	3337	3516	3533	3761	3973	4170
		R <sub>KI</sub>	1312	1352	1391	1700	1752	1803	1854	2203	2268	2332	2397
		n	0.85	0.87	0.89	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
9/16	1/2	M <sub>U</sub>	3639	4093	4523	4155	4686	5193	5677	5279	5864	6425	6962
		R <sub>KI</sub>	2153	2373	2593	2792	3078	3364	3650	3876	4236	4596	4956
		n	0.83	0.83	0.83								

T & S $t_f = 6\text{-in.}$ $L6 \times 4 \times t_f$	Web $2L4 \times 3.5$ $t_a$	A36 $\frac{3}{4}\text{-in.}$ Dia.	Beam														
			W27				W30				W33				W36		
			9 row	6 row	7 row	8 row	9 row	6 row	7 row	8 row	9 row	6 row	7 row	8 row	9 row	6 row	7 row
3/4	1/2	$M_U$	6887	7554	8197	8817	9413	8313	9033	9730	10404	9072	9869				
		$R_{K1}$	6475	6923	7371	7819	8267	8338	8878	9418	9958	9885	10526				
		$n$	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83			
	3/8	$M_U$	5724	6157	6570	6962	7333	6775	7241	7687	8111	7394	7913				
		$R_{K1}$	5146	5319	5493	5666	5839	6407	6616	6824	7033	7595	7843				
		$n$	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83			
	5/16	$M_U$	5304	5660	5999	6320	6623	6224	6607	6972	7319	6789	7215				
		$R_{K1}$	5105	5270	5435	5600	5765	6347	6546	6745	6943	7525	7760				
		$n$	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83			
	1/4	$M_U$	4815	5077	5324	5556	5773	5581	5861	6126	6376	6084	6398				
		$R_{K1}$	4694	4774	4853	4933	5013	5749	5845	5941	6038	6816	6930				
		$n$	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83			
5/8	1/2	$M_U$	5987	6650	7290	7906	8499	7329	8046	8740	9410	8008	8802				
		$R_{K1}$	4474	4918	5363	5807	6252	5928	6464	7000	7536	7033	7668				
		$n$	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83			
	3/8	$M_U$	4828	5259	5670	6060	6429	5797	6261	6704	7126	6335	6852				
		$R_{K1}$	3156	3328	3500	3672	3844	4011	4218	4426	4633	4758	5004				
		$n$	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83			
	5/16	$M_U$	4410	4764	5101	5420	5722	5249	5629	5992	6338	5733	6157				
		$R_{K1}$	3115	3279	3442	3606	3770	3952	4149	4346	4544	4688	4922				
		$n$	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83			
	1/4	$M_U$	3923	4184	4430	4660	4875	4607	4886	5150	5399	5031	5343				
		$R_{K1}$	2707	2786	2865	2945	3025	3358	3454	3549	3644	3984	4097				
		$n$	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83			
9/16	1/2	$M_U$	5872	6534	7172	7787	8378	7204	7920	8612	9280	7874	8667				
		$R_{K1}$	4765	5207	5650	6093	6536	6279	6813	7347	7881	7452	8085				
		$n$	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83			
	3/8	$M_U$	4716	5146	5555	5944	6312	5676	6138	6580	7001	6205	6721				
		$R_{K1}$	3452	3624	3795	3966	4137	4369	4576	4782	4989	5185	5430				
		$n$	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83			
	5/16	$M_U$	4299	4652	4988	5306	5607	5128	5508	5870	6214	5604	6027				
		$R_{K1}$	3412	3575	3738	3901	4064	4311	4507	4703	4900	5115	5348				
		$n$	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83			
	1/4	$M_U$	3813	4073	4318	4548	4762	4488	4766	5029	5277	4903	5215				
		$R_{K1}$	3006	3084	3163	3242	3321	3719	3814	3909	4004	4413	4526				
		$n$	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83			
1/2	1/2	$M_U$	5427	6087	6724	7337	7927	6717	7431	8122	8789	7347	8138				
		$R_{K1}$	3897	4338	4779	5220	5661	5233	5765	6297	6829	6212	6843				
		$n$	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83			
	3/8	$M_U$	4273	4702	5111	5498	5865	5192	5653	6094	6514	5681	6195				
		$R_{K1}$	2590	2761	2931	3102	3272	3330	3536	3742	3947	3953	4197				
		$n$	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83			
	5/16	$M_U$	3857	4210	4545	4862	5162	4645	5024	5385	5729	5080	5503				
		$R_{K1}$	2550	2712	2874	3037	3199	3271	3467	3663	3859	3883	4116				
		$n$	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83			
	1/4	$M_U$	3373	3632	3876	4105	4319	4006	4284	4546	4794	4381	4692				
		$R_{K1}$	2145	2224	2302	2381	2459	2682	2777	2872	2966	3184	3296				
		$n$	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83			
7/16	1/2	$M_U$	4983	5642	6277	6888	7476	6231	6943	7632	8298	6820	7610				
		$R_{K1}$	3252	3692	4131	4570	5009	4455	4985	5515	6045	5290	5919				
		$n$	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83			
	3/8	$M_U$	3832	4260	4667	5053	5419	4708	5169	5608	6027	5157	5670				
		$R_{K1}$	1951	2121	2290	2460	2630	2559	2764	2969	3174	3038	3282				
		$n$	0.85	0.87	0.87	0.88	0.88	0.83	0.83	0.83	0.83	0.83	0.83	0.83			
	5/16	$M_U$	3416	3768	4102	4419	4717	4163	4541	4901	5244	4558	4979				
		$R_{K1}$	1911	2072	2234	2395	2557	2501	2696	2891	3085	2969	3201				
		$n$	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83			
	1/4	$M_U$	2933	3192	3435	3663	3876	3525	3802	4064	4311	3859	4170				
		$R_{K1}$	1508	1586	1664	1742	1820	1913	2008	2102	2196	2272	2384				
		$n$	0.85	0.87	0.88	0.89	0.9	0.83	0.83	0.84	0.85	0.83	0.83	0.83			
3/8	1/2	$M_U$	4878	5535	6168	6778	7365	6116	6827	7514	8178	6697	7485				
		$R_{K1}$	3288	3725	4162	4600	5037	4497	5025	5553	6081	5341	5969				
		$n$	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83			
	3/8	$M_U$	3729	4156	4562	4948	5312	4596	5056	5494	5912	5037	5549				
		$R_{K1}$	1991	2160	2330	2499	2668	2608	2812	3017	3221	3098	3340				
		$n$	0.83	0.84	0.85	0.86	0.86	0.83	0.83	0.83	0.83	0.83	0.83	0.83			
	5/16	$M_U$	3315	3666	3999	4314	4612	4052	4429	4789	5130	4439	4860				
		$R_{K1}$	1951	2112	2273	2434	2595	2550	2744	2938	3133	3029	3260				
		$n$	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83			
	1/4	$M_U$	2832	3090	3333	3561	3773	3416	3692	3953	4199	3742	4051				
		$R_{K1}$	1550	1628	1706	1784	1861	1965	2059	2153	2247	2334	2446				
		$n$	0.83	0.83	0.85	0.86	0.87	0.83	0.83	0.83	0.83	0.83	0.83	0.83			

T & S $t_f = 6\text{-in.}$ $L6 \times 4 \times t_f$	Web $2L4 \times 3.5$ $t_a$	A36 $\frac{3}{4}\text{-in.}$ Dia.	Beam											
			W36			W40			W44					
			8 row	9 row	6 row	7 row	8 row	9 row	6 row	7 row	8 row	9 row		
3/4	1/2	$M_U$	10644	11394	10084	10984	11862	12715	11096	12099	13079	14036		
		$R_{K1}$	11166	11806	12153	12940	13728	14515	14655	15604	16554	17503		
		$n$	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
	3/8	$M_U$	8411	8889	8218									



T & S $t_f = 6\text{-in.}$ $L_6 \times 4 \times t_f$	Web $2L_4 \times 3.5$ $t_a$	A36 $\frac{3}{4}\text{-in.}$ Dia.	Beam																																						
			W8		W10		W12		W14		W16		W18																												
			2 row	3 row	2 row	3 row	2 row	3 row	2 row	3 row	2 row	3 row	2 row	3 row																											
3/4	1/2	$M_U$	1375	1663	1852	1952	2188	2524	2860	3165	3196	3549	3874	$R_{ki}$	307	460	487	645	682	911	1173	1237	1469	1549	1628	$n$	1.35	1.22	1.25	1.11	1.15	1.06	0.98	1.01	0.91	0.83	0.83	0.95	0.97		
		$M_U$	1268	1530	1660	1791	1955	2251	2547	2758	2842	3088	3311	$R_{ki}$	293	439	455	616	638	852	1097	1135	1373	1421	1469	$n$	1.33	1.2	1.23	1.09	1.12	1.03	0.95	0.98	0.88	0.91	0.83	0.83	0.94	0.94	
		$M_U$	1215	1463	1563	1710	1838	2114	2389	2553	2664	2856	3028	$R_{ki}$	284	425	434	596	608	812	1046	1067	1309	1336	1362	$n$	1.33	1.19	1.22	1.08	1.11	1.02	0.94	0.97	0.87	0.9	0.83	0.83	0.93	0.93	
	3/8	$M_U$	1170	1406	1484	1642	1742	2000	2257	2384	2515	2664	2797	$R_{ki}$	281	422	429	591	601	802	1033	1050	1293	1314	1335	$n$	1.31	1.17	1.2	1.06	1.09	1	0.92	0.94	0.85	0.87	0.89	0.89	0.89	0.89	
		$M_U$	1071	1305	1491	1539	1772	2054	2336	2638	2618	2968	3290	$R_{ki}$	178	269	294	378	414	554	715	778	897	976	1054	$n$	1.53	1.4	1.43	1.3	1.33	1.24	1.16	1.18	1.09	1.12	1.13	1.13	1.13	1.13	
		$M_U$	965	1173	1300	1380	1542	1784	2025	2234	2267	2510	2732	$R_{ki}$	165	248	263	349	371	496	640	678	802	850	897	$n$	1.52	1.39	1.41	1.28	1.31	1.22	1.14	1.17	1.07	1.1	1.12	1.12	1.12	1.12	
	5/16	$M_U$	869	1051	1127	1233	1331	1535	1738	1864	1942	2090	2221	$R_{ki}$	153	231	238	325	334	447	577	593	723	744	765	$n$	1.5	1.36	1.39	1.25	1.28	1.19	1.11	1.14	1.04	1.07	1.09	1.09	1.09	1.09	
		$M_U$	824	1013	1116	1211	1309	1485	1662	1809	1940	$R_{ki}$	142	218	225	312	321	434	564	580	710	731	752	$n$	1.48	1.35	1.38	1.22	1.25	1.16	1.08	1.11	1.01	1.04	1.06	1.06	1.06	1.06			
		$M_U$	724	879	955	1034	1132	1309	1485	1610	1662	1809	1940	$R_{ki}$	109	165	172	232	242	324	418	435	525	545	566	$n$	1.59	1.46	1.49	1.35	1.38	1.29	1.21	1.24	1.14	1.17	1.19	1.19	1.19	1.19	
	9/16	1/2	$M_U$	880	1082	1264	1283	1514	1763	2012	2311	2262	2609	2928	$R_{ki}$	136	206	231	291	327	439	568	629	713	791	868	$n$	1.58	1.45	1.48	1.34	1.37	1.29	1.21	1.23	1.14	1.17	1.18	1.18	1.18	1.18
			$M_U$	776	951	1077	1126	1286	1495	1704	1911	1913	2154	2374	$R_{ki}$	123	186	201	263	284	382	494	530	620	666	713	$n$	1.56	1.43	1.46	1.33	1.36	1.27	1.19	1.22	1.13	1.15	1.17	1.17	1.17	1.17
			$M_U$	724	886	983	1047	1171	1360	1549	1709	1738	1926	2095	$R_{ki}$	114	173	181	244	256	343	444	464	558	583	609	$n$	1.57	1.44	1.47	1.33	1.37	1.28	1.2	1.23	1.13	1.17	1.19	1.19	1.19	1.19
3/8		$M_U$	682	831	906	981	1077	1248	1420	1544	1591	1737	1867	$R_{ki}$	112	169	176	239	248	334	431	448	542	562	583	$n$	1.54	1.41	1.44	1.3	1.33	1.24	1.17	1.19	1.1	1.13	1.15	1.15	1.15	1.15	
		$M_U$	742	917	1098	1092	1321	1544	1767	2064	1990	2335	2653	$R_{ki}$	98	149	174	211	246	331	428	490	538	615	693	$n$	1.68	1.55	1.56	1.44	1.46	1.38	1.3	1.32	1.24	1.25	1.26	1.26	1.26	1.26	
		$M_U$	639	788	912	936	1095	1277	1460	1666	1642	1883	2101	$R_{ki}$	85	129	144	183	204	274	355	391	446	492	538	$n$	1.67	1.54	1.57	1.44	1.46	1.38	1.3	1.32	1.23	1.26	1.27	1.27	1.27	1.27	
5/16		$M_U$	588	722	818	857	981	1143	1306	1465	1468	1655	1823	$R_{ki}$	76	116	124	164	176	236	306	326	384	410	435	$n$	1.69	1.56	1.59	1.45	1.49	1.4	1.32	1.36	1.26	1.29	1.31	1.31	1.31	1.31	
		$M_U$	545	668	742	791	887	1032	1177	1300	1321	1467	1596	$R_{ki}$	74	112	119	159	168	226	293	309	368	388	409	$n$	1.66	1.53	1.56	1.42	1.45	1.36	1.29	1.32	1.22	1.25	1.27	1.27	1.27	1.27	
		$M_U$	618	769	949	920	1147	1346	1544	1840	1743	2087	2403	$R_{ki}$	71	108	133	154	188	254	329	390	414	491	567	$n$	1.76	1.63	1.64	1.53	1.54	1.46	1.38	1.38	1.32	1.32	1.32	1.32	1.32	1.32	
3/8		$M_U$	516	640	764	764	922	1080	1239	1443	1397	1636	1853	$R_{ki}$	58	89	103	126	147	198	256	292	322	368	414	$n$	1.77	1.64	1.66	1.54	1.56	1.47	1.4	1.41	1.33	1.35	1.35	1.35	1.35	1.35	
		$M_U$	465	575	670	686	809	947	1085	1244	1223	1409	1576	$R_{ki}$	50	76	84	107	119	160	207	227	261	286	311	$n$	1.8	1.68	1.71	1.57	1.61	1.52	1.45	1.47	1.38	1.41	1.43	1.43	1.43	1.43	
		$M_U$	423	521	595	620	715	836	956	1079	1077	1222	1351	$R_{ki}$	48	72	79	103	112	150	195	211	245	265	285	$n$	1.77	1.64	1.67	1.54	1.57	1.49	1.41	1.44	1.34	1.37	1.39	1.39	1.39	1.39	

T & S $t_f = 6\text{-in.}$ $L_6 \times 4 \times t_f$	Web $2L_4 \times 3.5$ $t_a$	A36 $\frac{3}{4}\text{-in.}$ Dia.	Beam																																				
			W21			W24				W27																													
			3 row	4 row	5 row	4 row	5 row	6 row	7 row	5 row	6 row	7 row	8 row																										
3/4	1/2	$M_U$	4124	4521	4891	4700	5169	5610	6025	5816	6329	6815	7274	$R_{ki}$	2082	2189	2296	2694	2833	2972	3110	3560	3734	3909	4083	$n$	0.86	0.88	0.9	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
		$M_U$	3583	3858	4111	4078	4404	4709	4992	4951	5307	5642	5954	$R_{ki}$	1910	1974	2038	2471	2555	2638	2721	3210	3315	3419	3524	$n$	0.83	0.85	0.87	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
		$M_U$	3311	3524	3719	3765	4020	4256	4473	4516	4793	5052	5290	$R_{ki}$	1795	1831	1866	2323	2369	2415	2461	2977	3035	3092	3150	$n$	0.83	0.84	0.86	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
	3/8	$M_U$	3083	3249	3399	3503	3701	3883	4050	4153	4368	4567	4751	$R_{ki}$	1766	1794	1822	2285	2321	2358	2394	2917	2963	3009	3055	$n$	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
		$M_U$	3462	3857	4224	3957	4423	4862	5273	4989	5499	5983	6439	$R_{ki}$	1314	1420	1526	1703	1840	1978	2115	2315	2488	2661	2834	$n$	1.03	1.05	1.06	0.95	0.97	0.99	1	0.91	0.92	0.93	0.94	0.94	0.94
		$M_U$	2924	3197	3448	3338	3663	3965	4246	4128	4483	4815	5125	$R_{ki}$	1144	1208	1271	1483	1565	1647	1730	1969	2072	2176	2279	$n$	1.01	1.03	1.05	0.93	0.96	0.98	0.99	0.89	0.91	0.92	0.93	0.93	0.93
	5/16	$M_U$	2654	2866	3058	3027	3281	3515	3730	3696	3971	4228	4465	$R_{ki}$	1031	1066	1101	1336	1381	1427	1472	1737	1795	1852	1909	$n$	1.02	1.04	1.06	0.94	0.97	0.99	1.01	0.9	0.92	0.94	0.96	0.96	0.96
		$M_U$	2428	2592	2741	2766	2963	3144	3310	3334	3548	3746	3928	$R_{ki}$	1002	1030	1057	1298	1334	1370	1406	1678	1732	1769	1814	$n$	0.98	1	1.02	0.9	0.93	0.95	0.96	0.86	0.88	0.9	0.91	0.91	0.91
		$M_U$	3138	3531	3896	3592	4057	4494	4904	4583	5091	5573	6028	$R_{ki}$	1046	1151	1256	1356	1493	1629	1766	1879	2051	2223	2395	$n$	1.11	1.12	1.13	1.03	1.05	1.06	1.06	0.98	0.99	1	1	1	1
	9/16	$M_U$	2602	2874	3124	2975	3299	3600	3880	3724	4077	4408	4718	$R_{ki}$	877	940	1003	1137	1219	1301	1383	1534	1637	1740	1844	$n$	1.1	1.12	1.13	1.03	1.05	1.06	1.07	0.98	1	1.01	1.01	1.01	1.01
		$M_U$	2332	2543	2735	2665	2918	3151	3365	3292	3567	3823	4059	$R_{ki}$	764	799	834	991	1036	1081	1127	1304	1361	1418	1475	$n$	1.12	1.15	1.16	1.04	1.07	1.09	1.11	1	1.03	1.04	1.06	1.06	1.06
		$M_U$	2107	2271	2418	2405	2601	2782	2946	2932	3145	3342	3524	$R_{ki}$	735	763	791	953	989	1025	1061	1245	1290	1335	1381	$n$	1.08												



T & S t <sub>f</sub> = 6-in. L6×4×t <sub>f</sub>	Web 2L4×3.5 t <sub>w</sub>	A36 ¾-in. Dia.	Beam																																					
			W8		W10		W12		W14		W16		W18																											
			2 row	3 row	2 row	3 row	2 row	3 row	2 row	3 row	2 row	3 row	2 row	3 row																										
¾	½	M <sub>U</sub>	1300	1565	1725	1830	2027	2330	2632	2886	2934	3226	3500	R <sub>KI</sub>	538	809	864	1135	1212	1620	2086	2219	2612	2779	2946	n	0.98	0.84	0.86	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83		
		¾	M <sub>U</sub>	1210	1454	1556	1698	1826	2095	2365	2529	2635	2824	2998	R <sub>KI</sub>	498	747	769	1048	1078	1440	1855	1907	2323	2387	2452	n	0.98	0.85	0.87	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	
			5/16	M <sub>U</sub>	1179	1414	1498	1650	1755	2012	2269	2403	2526	2681	2824	R <sub>KI</sub>	496	745	766	1046	1074	1435	1848	1897	2314	2375	2437	n	0.97	0.83	0.85	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
	¼			M <sub>U</sub>	1141	1368	1429	1595	1672	1914	2157	2255	2400	2514	2618	R <sub>KI</sub>	484	726	736	1019	1032	1379	1777	1800	2224	2254	2284	n	0.96	0.83	0.84	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
		½		M <sub>U</sub>	1010	1224	1382	1438	1633	1884	2135	2387	2386	2675	2947	R <sub>KI</sub>	315	475	529	669	744	998	1288	1419	1615	1779	1944	n	1.15	1.02	1.03	0.91	0.92	0.83	0.83	0.83	0.83	0.83	0.83	0.83
			¾	M <sub>U</sub>	922	1115	1215	1307	1433	1652	1870	2032	2088	2276	2448	R <sub>KI</sub>	275	415	436	584	613	821	1060	1111	1329	1393	1457	n	1.18	1.04	1.07	0.93	0.96	0.87	0.83	0.83	0.83	0.83	0.83	0.83
	5/16			M <sub>U</sub>	891	1075	1158	1260	1364	1569	1775	1908	1981	2135	2276	R <sub>KI</sub>	274	413	433	581	609	816	1053	1101	1321	1381	1442	n	1.16	1.02	1.04	0.91	0.93	0.84	0.83	0.83	0.83	0.83	0.83	0.83
				¼	M <sub>U</sub>	854	1030	1089	1205	1281	1472	1664	1761	1855	1969	2073	R <sub>KI</sub>	261	394	404	555	568	761	983	1006	1232	1261	1291	n	1.16	1.03	1.04	0.91	0.94	0.84	0.83	0.83	0.83	0.83	0.83
			¾		M <sub>U</sub>	965	1174	1330	1382	1576	1821	2067	2318	2313	2600	2871	R <sub>KI</sub>	341	518	571	731	806	1082	1398	1528	1756	1919	2082	n	1.07	0.94	0.96	0.83	0.85	0.83	0.83	0.83	0.83	0.83	0.83
	5/16				M <sub>U</sub>	878	1065	1165	1252	1377	1590	1803	1964	2016	2203	2374	R <sub>KI</sub>	302	458	479	647	676	907	1173	1223	1472	1535	1598	n	1.09	0.95	0.98	0.84	0.87	0.83	0.83	0.83	0.83	0.83	0.83
		¼		M <sub>U</sub>	847	1026	1108	1205	1308	1508	1708	1841	1909	2062	2203	R <sub>KI</sub>	301	457	476	644	672	902	1166	1213	1463	1523	1583	n	1.07	0.93	0.96	0.83	0.85	0.83	0.83	0.83	0.83	0.83	0.83	0.83
				½	M <sub>U</sub>	810	980	1040	1150	1226	1412	1598	1694	1784	1897	1998	R <sub>KI</sub>	289	438	448	618	632	848	1096	1119	1375	1404	1433	n	1.07	0.93	0.95	0.83	0.84	0.83	0.83	0.83	0.83	0.83	0.83
½	M <sub>U</sub>				828	1010	1165	1193	1385	1605	1825	2074	2045	2331	2601	R <sub>KI</sub>	248	377	429	533	607	816	1056	1185	1327	1490	1652	n	1.17	1.04	1.05	0.93	0.94	0.85	0.83	0.83	0.83	0.83	0.83	0.83
	¾	M <sub>U</sub>			741	902	1001	1064	1188	1375	1562	1722	1749	1935	2106	R <sub>KI</sub>	209	318	338	450	479	643	832	882	1045	1108	1171	n	1.21	1.08	1.1	0.96	0.99	0.9	0.83	0.85	0.83	0.83	0.83	0.83
		5/16	M <sub>U</sub>	710	863	944	1017	1119	1293	1468	1599	1642	1795	1935	R <sub>KI</sub>	208	316	336	447	475	638	825	873	1037	1096	1156	n	1.19	1.05	1.07	0.94	0.96	0.87	0.83	0.83	0.83	0.83	0.83	0.83	
			¼	M <sub>U</sub>	674	818	877	962	1037	1197	1358	1454	1518	1630	1731	R <sub>KI</sub>	196	298	308	422	435	584	756	779	949	978	1007	n	1.19	1.06	1.08	0.94	0.97	0.88	0.83	0.83	0.83	0.83	0.83	0.83
	¾			M <sub>U</sub>	693	849	1003	1006	1197	1391	1585	1833	1778	2064	2333	R <sub>KI</sub>	179	273	325	387	461	620	803	932	1010	1172	1333	n	1.26	1.13	1.13	1.02	1.02	0.93	0.85	0.85	0.83	0.83	0.83	0.83
		5/16		M <sub>U</sub>	606	742	840	877	1001	1162	1323	1483	1484	1669	1839	R <sub>KI</sub>	141	215	235	305	333	449	581	630	730	793	855	n	1.33	1.19	1.22	1.08	1.11	1.02	0.94	0.96	0.87	0.89	0.91	0.91
¼			M <sub>U</sub>	576	703	784	831	932	1081	1229	1360	1377	1529	1669	R <sub>KI</sub>	140	214	233	302	329	443	574	621	722	781	840	n	1.3	1.17	1.18	1.06	1.07	0.98	0.9	0.92	0.83	0.85	0.86	0.86	
			½	M <sub>U</sub>	540	658	717	776	851	985	1119	1215	1254	1365	1466	R <sub>KI</sub>	128	196	205	277	290	390	505	528	635	664	692	n	1.32	1.18	1.2	1.07	1.1	1	0.93	0.95	0.86	0.88	0.9	0.9
		¾		M <sub>U</sub>	655	807	959	958	1148	1336	1525	1772	1713	1998	2265	R <sub>KI</sub>	181	277	328	394	466	629	816	943	1027	1187	1347	n	1.22	1.09	1.09	0.98	0.99	0.9	0.83	0.83	0.83	0.83	0.83	0.83
5/16				M <sub>U</sub>	569	700	797	830	953	1108	1264	1423	1420	1604	1774	R <sub>KI</sub>	144	220	240	312	340	459	595	644	749	811	873	n	1.28	1.15	1.17	1.04	1.07	0.98	0.9	0.92	0.83	0.83	0.83	0.83
	¼		M <sub>U</sub>	539	661	741	783	884	1027	1171	1301	1314	1465	1604	R <sub>KI</sub>	143	218	237	310	336	454	588	635	740	799	858	n	1.25	1.12	1.14	1.01	1.03	0.94	0.86	0.88	0.83	0.83	0.83	0.83	
			½	M <sub>U</sub>	504	617	675	730	804	932	1061	1157	1190	1302	1402	R <sub>KI</sub>	131	200	209	285	297	401	520	542	654	683	711	n	1.26	1.13	1.15	1.01	1.05	0.95	0.88	0.9	0.83	0.83	0.83	0.85

T & S t <sub>f</sub> = 6-in. L6×4×t <sub>f</sub>	Web 2L4×3.5 t <sub>w</sub>	A36 ¾-in. Dia.	Beam																																				
			W21				W27																																
			3 row	4 row	5 row	4 row	5 row	6 row	7 row	5 row	6 row	7 row	8 row																										
¾	½	M <sub>U</sub>	3735	4065	4378	4244	4630	4998	5350	5194	5619	6026	6417	R <sub>KI</sub>	3737	3961	4185	4837	5127	5418	5708	6444	6809	7174	7539	n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83		
		¾	M <sub>U</sub>	3266	3479	3676	3709	3960	4195	4416	4440	4714	4973	5217	R <sub>KI</sub>	3210	3297	3383	4154	4267	4379	4491	5362	5503	5644	5785	n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	
			5/16	M <sub>U</sub>	3099	3273	3435	3516	3722	3915	4095	4170	4395	4607	4807	R <sub>KI</sub>	3194	3276	3359	4133	4240	4347	4454	5328	5463	5597	5731	n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
	¼			M <sub>U</sub>	2903	3030	3146	3291	3442	3583	3712	3855	4019	4173	4316	R <sub>KI</sub>	3030	3070	3110	3922	3974	4025	4077	4993	5058	5123	5188	n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
		½		M <sub>U</sub>	3107	3435	3746	3539	3923	4289	4638	4410	4832	5238	5626	R <sub>KI</sub>	2397	2619	2841	3107	3395	3682	3970	4271	4633	4995	5357	n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
			¾	M <sub>U</sub>	2641	2852	3048	3007	3256	3490	3709	3660	3932	4190	4432	R <sub>KI</sub>	1876	1962	2048	2432	2543	2654	2765	3199	3339	3479	3619	n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
	5/16			M <sub>U</sub>	2475	2648	2808	2815	3020	3211	3391	3391	3615	3826	4024	R <sub>KI</sub>	1860	1942	2023	2411	2517	2622	2728	3166	3299	3432	3565	n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
				¼	M <sub>U</sub>	2280	2406	2522	2591	2742	2881	3010	3077	3241	3393	3535	R <sub>KI</sub>	1699	1738	1778	2202	2253	2304	2355	2834	2896	2963	3027	n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
			¾		M <sub>U</sub>	3024	3351	3661	3448	3831	4196	4544	4310	4731	5135	5522	R <sub>KI</sub>	2588	2809	3029	3358	3644	3930	4216	4587	4947	5307	5668	n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
	5/16				M <sub>U</sub>	2560	2770	2965	2918	3166	3399	3618	3562	3833	4090	4331	R <sub>KI</sub>	2070	2155	2241	2685	2796	2907	3017	3520	3659	3798	3938	n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
		¼		M <sub>U</sub>	2394	2566	2726</																																





T & S I <sub>t</sub> = 6-in. L6x4x $t_f$	Web 2L4x3.5 $t_a$	A36 3/4-in. Dia.	Beam																																					
			W27				W30				W33				W36																									
			9 row	6 row	7 row	8 row	9 row	6 row	7 row	8 row	9 row	6 row	7 row	8 row	6 row	7 row																								
3/4	1/2	M <sub>U</sub>	5405	5826	6227	6609	6972	6413	6866	7300	7714	7000	7505			R <sub>KI</sub>	5469	5683	5897	6112	6326	6845	7103	7361	7619	8114	8420	n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
		M <sub>U</sub>	4709	5003	5281	5543	5789	5503	5818	6117	6401	6003	6355				R <sub>KI</sub>	5040	5168	5296	5425	5553	6224	6379	6534	6688	7378		7562	n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
	3/8	M <sub>U</sub>	4360	4589	4805	5007	5195	5046	5291	5523	5740	5502	5777			R <sub>KI</sub>	4753	4824	4895	4966	5037	5810	5895	5981	6067	6887	6989	n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	
		M <sub>U</sub>	4067	4245	4412	4568	4712	4663	4854	5033	5201	5081	5295			R <sub>KI</sub>	4680	4736	4792	4849	4905	5704	5771	5839	5907	6761	6842	n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	
	5/16	M <sub>U</sub>	4537	4956	5355	5735	6095	5465	5916	6347	6759	5974	6477			R <sub>KI</sub>	3438	3651	3863	4076	4288	4400	4656	4912	5169	5219	5523	n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	
		M <sub>U</sub>	3844	4137	4413	4674	4918	4559	4872	5170	5452	4981	5331			R <sub>KI</sub>	3012	3140	3267	3394	3522	3784	3938	4091	4245	4489	4671	n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	
	5/8	M <sub>U</sub>	3496	3725	3939	4140	4326	4103	4347	4578	4794	4482	4756			R <sub>KI</sub>	2728	2799	2869	2940	3010	3373	3458	3543	3628	4001	4101	n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	
		M <sub>U</sub>	3204	3382	3548	3703	3846	3722	3912	4090	4257	4063	4276			R <sub>KI</sub>	2655	2711	2767	2823	2879	3267	3335	3402	3470	3876	3956	n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	
	1/4	M <sub>U</sub>	4109	4527	4926	5305	5664	4998	5448	5878	6289	5468	5970			R <sub>KI</sub>	2727	2938	3150	3362	3573	3543	3798	4053	4308	4204	4507	n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	
		M <sub>U</sub>	3419	3710	3986	4246	4490	4094	4406	4703	4984	4477	4827			R <sub>KI</sub>	2302	2429	2556	2683	2810	2929	3082	3235	3388	3475	3657	n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	
	9/16	M <sub>U</sub>	3072	3299	3513	3713	3899	3639	3882	4112	4328	3979	4252			R <sub>KI</sub>	2019	2090	2160	2230	2300	2519	2604	2689	2773	2989	3090	n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	
		M <sub>U</sub>	2780	2957	3123	3277	3420	3259	3448	3626	3792	3560	3783			R <sub>KI</sub>	1947	2002	2058	2114	2170	2414	2481	2549	2616	2864	2944	n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	
1/2	M <sub>U</sub>	4005	4422	4819	5197	5555	4884	5333	5762	6172	5346	5847			R <sub>KI</sub>	2791	3001	3212	3423	3634	3620	3875	4129	4383	4297	4599	n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83		
	M <sub>U</sub>	3316	3606	3881	4140	4383	3982	4293	4590	4870	4357	4706			R <sub>KI</sub>	2368	2495	2621	2747	2874	3009	3161	3314	3466	3572	3753	n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83		
5/8	M <sub>U</sub>	2969	3196	3409	3609	3794	3528	3771	4000	4215	3859	4132			R <sub>KI</sub>	2086	2156	2226	2296	2366	2601	2685	2770	2854	3087	3187	n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83		
	M <sub>U</sub>	2679	2855	3020	3174	3316	3148	3337	3514	3680	3442	3654			R <sub>KI</sub>	2014	2069	2125	2180	2236	2496	2563	2630	2697	2963	3042	n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83		
7/16	M <sub>U</sub>	3590	4006	4402	4779	5136	4430	4878	5306	5715	4854	5354			R <sub>KI</sub>	2163	2373	2583	2793	3003	2863	3117	3370	3623	3400	3701	n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83		
	M <sub>U</sub>	2903	3192	3466	3725	3967	3529	3841	4136	4416	3867	4215			R <sub>KI</sub>	1742	1868	1994	2120	2246	2254	2406	2558	2710	2677	2857	n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83		
5/16	M <sub>U</sub>	2557	2783	2996	3194	3379	3077	3319	3548	3762	3370	3642			R <sub>KI</sub>	1462	1531	1601	1671	1740	1848	1932	2016	2100	2194	2293	n	0.83	0.83	0.83	0.84	0.85	0.83	0.83	0.83	0.83	0.83	0.83		
	M <sub>U</sub>	2267	2443	2607	2761	2902	2698	2886	3063	3228	2954	3165			R <sub>KI</sub>	1390	1445	1500	1555	1611	1743	1810	1877	1943	2070	2149	n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83		
3/8	M <sub>U</sub>	3213	3627	4023	4398	4754	4017	4464	4891	5298	4406	4904			R <sub>KI</sub>	1715	1924	2133	2342	2551	2323	2575	2827	3080	2759	3058	n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83		
	M <sub>U</sub>	2527	2816	3089	3346	3588	3118	3428	3723	4002	3420	3768			R <sub>KI</sub>	1296	1421	1547	1672	1797	1716	1867	2018	2169	2038	2217	n	0.85	0.86	0.86	0.86	0.86	0.83	0.83	0.83	0.83	0.83	0.83		
5/16	M <sub>U</sub>	2182	2407	2619	2817	3001	2666	2908	3136	3350	2925	3196			R <sub>KI</sub>	1016	1086	1155	1224	1294	1310	1394	1478	1562	1556	1656	n	0.91	0.93	0.94	0.95	0.95	0.87	0.89	0.9	0.91	0.83	0.84		
	M <sub>U</sub>	1892	2068	2232	2384	2526	2288	2476	2652	2817	2509	2720			R <sub>KI</sub>	945	1000	1055	1110	1165	1207	1273	1339	1406	1433	1512	n	0.86	0.88	0.9	0.91	0.91	0.83	0.85	0.86	0.86	0.83	0.83		

T & S I <sub>t</sub> = 6-in. L6x4x $t_f$	Web 2L4x3.5 $t_a$	A36 3/4-in. Dia.	Beam																																		
			W36			W40			W44																												
			8 row	9 row	6 row	7 row	8 row	9 row	6 row	7 row	8 row	9 row																									
3/4	1/2	M <sub>U</sub>	7990	8455	7782	8356	8910	9444	8565	9207	9830	10434	R <sub>KI</sub>	8726	9032	9975	10351	10728	11104	12028	12482	12935	13389	n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83		
		M <sub>U</sub>	6691	7012	6669	7071	7457	7827	7336	7787	8222	8642				R <sub>KI</sub>	7745	7929	9070	9296	9521	9747	10937		11209	11481	11753	n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
	3/8	M <sub>U</sub>	6039	6286	6110	6425	6726	7014	6719	7073	7414	7741			R <sub>KI</sub>	7090	7192	8466	8591	8716	8841	10208	10359	10510	10660	n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
		M <sub>U</sub>	5498	5689	5639	5884	6118	6341	6197	6473	6738	6992			R <sub>KI</sub>	6922	7003	8311	8411	8510	8609	10022	10141	10261	10380	n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
	5/16	M <sub>U</sub>	6960	7423	6653	7224	7776	8309	7332	7972	8593	9194			R <sub>KI</sub>	5827	6131	6421	6795	7169	7543	7746	8198	8649	9100	n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
		M <sub>U</sub>	5666	5985	5544	5944	6328	6697	6107	6556	6990	7408			R <sub>KI</sub>	4853	5035	5522	5746	5970	6194	6661	6932	7202	7473	n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
	5/8	M <sub>U</sub>	5016	5262	4986	5300	5600	5886	5491	5844	6184	6510			R <sub>KI</sub>	4202	4303	4921	5045	5169	5293	5937	6087	6236	6386	n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
		M <sub>U</sub>	4477	4668	4517	4761	4994	5216	4970	5246	5510	5763			R <sub>KI</sub>	4036	4115	4767	4866	4964	5063	5751	5870	5989	6108	n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
	1/4	M <sub>U</sub>	6452	6914	6095	6666	7217	7748	6723	7362	7982	8582			R <sub>KI</sub>	4810	5112	5173	5546	5919	6291	6243	6693	7143	7593	n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
		M <sub>U</sub>	5161	5479	4988	5387	5771	6139	5499	5948	6381	6798			R <sub>KI</sub>	3838	4020	4277	4500	4723	4947	5161	5431	5700	5970	n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
	9/16	M <sub>U</sub>	4512	4757	4432	4745																															

T & S I <sub>t</sub> = 6-in. L <sub>6</sub> × 4 × I <sub>t</sub>	Web 2L4 × 3.5 I <sub>a</sub>	A36 3/4-in. Dia.	Beam											
			W8		W10		W12		W14		W16		W18	
			2 row	3 row	2 row	3 row	2 row	3 row	2 row	3 row	2 row	3 row	2 row	3 row
3/4	1/2	M <sub>U</sub>	1805	2174	2396	2542	2816	3235	3655	4008	4075	4480	4861	
		R <sub>KI</sub>	538	809	864	1135	1212	1620	2086	2219	2612	2779	2946	
		n	1.18	1.04	1.06	0.93	0.95	0.86	0.83	0.83	0.83	0.83	0.83	
	3/8	M <sub>U</sub>	1681	2020	2161	2359	2536	2910	3285	3512	3659	3922	4164	
		R <sub>KI</sub>	498	747	769	1048	1078	1440	1855	1907	2323	2387	2452	
		n	1.18	1.05	1.07	0.93	0.96	0.87	0.83	0.83	0.83	0.83	0.83	
	5/16	M <sub>U</sub>	1637	1964	2081	2292	2438	2794	3151	3338	3508	3724	3922	
		R <sub>KI</sub>	496	745	766	1046	1074	1435	1848	1897	2314	2375	2437	
		n	1.17	1.03	1.05	0.92	0.94	0.85	0.83	0.83	0.83	0.83	0.83	
	1/4	M <sub>U</sub>	1585	1900	1984	2215	2322	2659	2996	3132	3333	3492	3635	
		R <sub>KI</sub>	484	726	736	1019	1032	1379	1777	1800	2224	2254	2284	
		n	1.16	1.03	1.04	0.91	0.93	0.84	0.83	0.83	0.83	0.83	0.83	
5/8	1/2	M <sub>U</sub>	1403	1700	1919	1997	2268	2616	2965	3315	3314	3715	4093	
		R <sub>KI</sub>	315	475	529	669	744	998	1288	1419	1615	1779	1944	
		n	1.35	1.22	1.23	1.11	1.12	1.03	0.95	0.96	0.88	0.89	0.89	
	3/8	M <sub>U</sub>	1280	1548	1688	1816	1991	2294	2597	2822	2900	3161	3400	
		R <sub>KI</sub>	275	415	436	584	613	821	1060	1111	1329	1393	1457	
		n	1.38	1.24	1.26	1.13	1.16	1.07	0.99	1.01	0.92	0.94	0.96	
	5/16	M <sub>U</sub>	1237	1493	1608	1750	1894	2179	2465	2650	2751	2965	3161	
		R <sub>KI</sub>	274	413	433	581	609	816	1053	1101	1321	1381	1442	
		n	1.36	1.22	1.24	1.11	1.13	1.04	0.96	0.98	0.89	0.91	0.92	
	1/4	M <sub>U</sub>	1186	1430	1513	1673	1779	2045	2311	2446	2577	2734	2876	
		R <sub>KI</sub>	261	394	404	555	568	761	983	1006	1232	1261	1291	
		n	1.36	1.22	1.24	1.11	1.13	1.04	0.96	0.98	0.89	0.91	0.93	
9/16	1/2	M <sub>U</sub>	1340	1630	1847	1920	2188	2530	2871	3219	3212	3611	3988	
		R <sub>KI</sub>	341	518	571	731	806	1082	1398	1528	1756	1919	2082	
		n	1.27	1.14	1.16	1.03	1.05	0.96	0.88	0.89	0.83	0.83	0.84	
	3/8	M <sub>U</sub>	1219	1479	1617	1739	1913	2209	2504	2728	2800	3059	3298	
		R <sub>KI</sub>	302	458	479	647	676	907	1173	1223	1472	1535	1598	
		n	1.29	1.15	1.18	1.04	1.07	0.98	0.9	0.93	0.83	0.86	0.88	
	5/16	M <sub>U</sub>	1176	1425	1538	1674	1816	2094	2373	2556	2651	2864	3059	
		R <sub>KI</sub>	301	457	476	644	672	902	1166	1213	1463	1523	1583	
		n	1.27	1.13	1.15	1.02	1.05	0.95	0.87	0.89	0.83	0.83	0.84	
	1/4	M <sub>U</sub>	1125	1361	1444	1597	1702	1961	2219	2353	2477	2634	2775	
		R <sub>KI</sub>	289	438	448	618	632	848	1096	1119	1375	1404	1433	
		n	1.27	1.13	1.15	1.02	1.04	0.95	0.87	0.89	0.83	0.83	0.84	
1/2	1/2	M <sub>U</sub>	1149	1403	1619	1657	1924	2229	2534	2881	2839	3238	3612	
		R <sub>KI</sub>	248	377	429	533	607	816	1056	1185	1327	1490	1652	
		n	1.37	1.24	1.25	1.13	1.14	1.05	0.97	0.98	0.9	0.91	0.92	
	3/8	M <sub>U</sub>	1028	1253	1390	1477	1650	1909	2169	2392	2429	2687	2925	
		R <sub>KI</sub>	209	318	338	450	479	643	832	882	1045	1108	1171	
		n	1.41	1.27	1.3	1.16	1.19	1.1	1.02	1.05	0.95	0.98	1	
	5/16	M <sub>U</sub>	986	1199	1311	1412	1554	1796	2038	2221	2280	2493	2687	
		R <sub>KI</sub>	208	316	336	447	475	638	825	873	1037	1096	1156	
		n	1.39	1.25	1.27	1.14	1.16	1.07	0.99	1.01	0.92	0.94	0.95	
	1/4	M <sub>U</sub>	936	1136	1218	1336	1440	1663	1885	2019	2108	2264	2404	
		R <sub>KI</sub>	196	298	308	422	435	584	756	779	949	978	1007	
		n	1.39	1.25	1.28	1.14	1.17	1.08	1	1.02	0.93	0.95	0.97	
7/16	1/2	M <sub>U</sub>	962	1179	1393	1397	1662	1932	2201	2546	2470	2866	3239	
		R <sub>KI</sub>	179	273	325	387	461	620	803	932	1010	1172	1333	
		n	1.46	1.33	1.33	1.22	1.22	1.13	1.05	1.05	0.98	0.99	0.98	
	3/8	M <sub>U</sub>	842	1030	1166	1218	1390	1613	1837	2059	2061	2318	2554	
		R <sub>KI</sub>	141	215	235	305	333	449	581	630	730	793	855	
		n	1.53	1.39	1.41	1.28	1.31	1.22	1.14	1.16	1.07	1.09	1.11	
	5/16	M <sub>U</sub>	800	977	1088	1153	1294	1501	1707	1889	1913	2124	2318	
		R <sub>KI</sub>	140	214	233	302	329	443	574	621	722	781	840	
		n	1.5	1.37	1.38	1.26	1.27	1.18	1.1	1.12	1.03	1.05	1.06	
	1/4	M <sub>U</sub>	750	914	995	1078	1182	1368	1554	1687	1741	1896	2036	
		R <sub>KI</sub>	128	196	205	277	290	390	505	528	635	664	692	
		n	1.52	1.38	1.4	1.27	1.3	1.2	1.12	1.15	1.05	1.08	1.1	
3/8	1/2	M <sub>U</sub>	910	1120	1332	1330	1594	1856	2118	2461	2380	2775	3146	
		R <sub>KI</sub>	181	277	328	394	466	629	816	943	1027	1187	1347	
		n	1.42	1.29	1.29	1.18	1.19	1.1	1.02	1.02	0.95	0.96	0.96	
	3/8	M <sub>U</sub>	791	972	1107	1152	1323	1539	1756	1976	1972	2228	2463	
		R <sub>KI</sub>	144	220	240	312	340	459	595	644	749	811	873	
		n	1.48	1.35	1.37	1.24	1.27	1.18	1.1	1.12	1.03	1.06	1.07	
	5/16	M <sub>U</sub>	749	918	1029	1088	1228	1427	1626	1807	1825	2035	2228	
		R <sub>KI</sub>	143	218	237	310	336	454	588	635	740	799	858	
		n	1.45	1.32	1.33	1.21	1.23	1.14	1.06	1.08	0.99	1.01	1.02	
	1/4	M <sub>U</sub>	700	856	937	1013	1116	1295	1474	1606	1653	1808	1947	
		R <sub>KI</sub>	131	200	209	285	297	401	520	542	654	683	711	
		n	1.46	1.33	1.35	1.21	1.25	1.15	1.08	1.1	1.01	1.03	1.05	

T & S I <sub>t</sub> = 6-in. L <sub>6</sub> × 4 × I <sub>t</sub>	Web 2L4 × 3.5 I <sub>a</sub>	A36 3/4-in. Dia.	Beam										
			W21		W24			W27					
			3 row	4 row	5 row	4 row	5 row	6 row	7 row	5 row	6 row	7 row	8 row
3/4	1/2	M <sub>U</sub>	5187	5645	6080	5894	6430	6942	7430	7214	7803	8369	8912
		R <sub>KI</sub>	3737	3961	4185	4837	5127	5418	5708	6444	6809	7174	7539
		n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
	3/8	M <sub>U</sub>	4536	4831	5106	5151	5499	5827	6133	6167	6547	6907	7246
		R <sub>KI</sub>	3210	3297	3383	4154	4267	4379	4491	5362	5503	5644	5785
		n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
	5/16	M <sub>U</sub>	4303	4545	4770	4883	5169	5437	5688	5792	6104	6399	6676
		R <sub>KI</sub>	3194	3276	3359	4133	4240	4347	4454	5328	5463	5597	5731
		n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
	1/4	M <sub>U</sub>	4031	4208	4370	4570	4781	4976	5156	5354	5582	5796	5994
		R <sub>KI</sub>	3030	3070	3110	3922	3974	4025	4077	4993	5058	5123	5188
		n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
5/8	1/2	M <sub>U</sub>	4315	4770	5202	4915	5448	5957	6442	6125	6712	7274	7813
		R <sub>KI</sub>	2397	2619	2841	3107	3395	3682	3970	4271	4633	4995	5357
		n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
	3/8	M <sub>U</sub>	3668	3961	4233	4176	4522	4847	5152	5083	5461	5819	6156
		R <sub>KI</sub>	1876	1962	2048	2432	2543	2654	2765	3199	3339	3479	3619
		n	0.85	0.87	0.88	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
	5/16	M <sub>U</sub>	3437	36									

T & S t <sub>f</sub> = 6-in. L6x4x <sub>t</sub>	Web 2L4x3.5 t <sub>a</sub>	A36 3/4-in. Dia.	Beam											
			W27			W30			W33			W36		
			9 row	6 row	7 row	8 row	9 row	6 row	7 row	8 row	9 row	6 row	7 row	8 row
3/4	1/2	M <sub>U</sub>	7998	8665	9308	9928	10524	9527	10247	10944	11617	10388	11186	
		R <sub>KI</sub>	7910	8359	8807	9255	9703	10068	10608	11148	11687	11936	12576	
	n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	
	3/8	M <sub>U</sub>	6835	7268	7681	8073	8445	7989	8455	8901	9325	8710	9230	
		R <sub>KI</sub>	6582	6755	6929	7102	7275	7479	7575	7671	7767	7866	8890	
	n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	
	5/16	M <sub>U</sub>	6415	6771	7110	7431	7734	7438	7821	8186	8533	8106	8532	
		R <sub>KI</sub>	6541	6706	6871	7036	7201	7366	7531	7696	7861	8026	8191	
	n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	
	1/4	M <sub>U</sub>	5926	6188	6435	6667	6884	6795	7075	7340	7590	7401	7715	
		R <sub>KI</sub>	6130	6209	6289	6369	6449	6529	6609	6689	6769	6849	6929	
	n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	
5/8	1/2	M <sub>U</sub>	6803	7466	8106	8723	9316	8221	8938	9632	10302	8976	9770	
		R <sub>KI</sub>	5248	5693	6138	6582	7027	6862	7398	7934	8470	8140	8776	
	n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83		
	3/8	M <sub>U</sub>	5644	6076	6486	6876	7245	6690	7153	7596	8018	7304	7821	
		R <sub>KI</sub>	3931	4103	4275	4446	4618	4945	5152	5359	5567	5866	6112	
	n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83		
	5/16	M <sub>U</sub>	5226	5581	5917	6237	6538	6141	6522	6885	7230	6701	7126	
		R <sub>KI</sub>	3890	4054	4217	4381	4544	4866	5083	5280	5477	5796	6030	
	n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83		
	1/4	M <sub>U</sub>	4740	5000	5246	5476	5691	5500	5779	6043	6291	5999	6311	
		R <sub>KI</sub>	3482	3561	3640	3719	3799	4292	4387	4483	4578	5091	5204	
	n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83		
9/16	1/2	M <sub>U</sub>	6653	7314	7953	8567	9159	8058	8773	9465	10134	8801	9594	
		R <sub>KI</sub>	5639	6082	6525	6968	7410	7334	7868	8402	8936	8703	9337	
	n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83		
	3/8	M <sub>U</sub>	5496	5927	6336	6725	7093	6529	6992	7434	7855	7132	7648	
		R <sub>KI</sub>	4327	4498	4670	4841	5012	5424	5631	5837	6044	6436	6682	
	n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83		
	5/16	M <sub>U</sub>	5079	5433	5769	6087	6388	5982	6361	6724	7068	6531	6954	
		R <sub>KI</sub>	4287	4450	4612	4775	4938	5365	5562	5758	5955	6367	6600	
	n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83		
	1/4	M <sub>U</sub>	4594	4854	5099	5328	5543	5342	5620	5883	6131	5830	6142	
		R <sub>KI</sub>	3880	3959	4038	4117	4195	4774	4969	4964	5059	5665	5777	
	n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83		
1/2	1/2	M <sub>U</sub>	6062	6722	7359	7972	8562	7412	8126	8816	9483	8101	8893	
		R <sub>KI</sub>	4486	4926	5367	5808	6249	5943	6475	7007	7539	7054	7686	
	n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83		
	3/8	M <sub>U</sub>	4908	5337	5746	6133	6500	5886	6348	6788	7208	6435	6950	
		R <sub>KI</sub>	3179	3349	3520	3690	3861	4040	4246	4451	4657	4795	5040	
	n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83		
	5/16	M <sub>U</sub>	4492	4844	5179	5497	5797	5340	5718	6080	6423	5835	6257	
		R <sub>KI</sub>	3138	3301	3463	3625	3787	3981	4177	4373	4568	4726	4958	
	n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83		
	1/4	M <sub>U</sub>	4007	4267	4511	4740	4954	4701	4979	5241	5488	5135	5446	
		R <sub>KI</sub>	2734	2812	2891	2969	3047	3392	3487	3581	3676	4026	4139	
	n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83		
7/16	1/2	M <sub>U</sub>	5472	6131	6766	7378	7966	6767	7479	8168	8833	7402	8192	
		R <sub>KI</sub>	3629	4068	4507	4946	5385	4909	5439	5969	6499	5829	6458	
	n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83		
	3/8	M <sub>U</sub>	4321	4749	5156	5543	5909	5244	5704	6144	6563	5739	6252	
		R <sub>KI</sub>	2327	2497	2667	2837	3007	3013	3218	3423	3628	3578	3821	
	n	0.83	0.83	0.84	0.85	0.85	0.83	0.83	0.83	0.83	0.83	0.83		
	5/16	M <sub>U</sub>	3906	4257	4592	4908	5207	4698	5076	5437	5780	5139	5561	
		R <sub>KI</sub>	2287	2449	2610	2772	2933	2955	3150	3345	3540	3508	3740	
	n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83		
	1/4	M <sub>U</sub>	3422	3681	3924	4153	4366	4061	4338	4600	4846	4441	4752	
		R <sub>KI</sub>	1884	1962	2040	2119	2197	2368	2462	2556	2651	2811	2923	
	n	0.83	0.83	0.84	0.85	0.86	0.83	0.83	0.83	0.83	0.83	0.83		
3/8	1/2	M <sub>U</sub>	5335	5992	6625	7235	7822	6616	7327	8014	8678	7241	8029	
		R <sub>KI</sub>	3679	4116	4553	4991	5428	4969	5497	6025	6553	5902	6529	
	n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83		
	3/8	M <sub>U</sub>	4186	4613	5019	5405	5769	5097	5556	5995	6412	5581	6093	
		R <sub>KI</sub>	2382	2552	2721	2890	3059	3080	3284	3489	3693	3659	3901	
	n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83		
	5/16	M <sub>U</sub>	3772	4122	4456	4771	5069	4552	4930	5289	5631	4982	5403	
		R <sub>KI</sub>	2343	2503	2664	2825	2986	3022	3216	3411	3605	3590	3820	
	n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83		
	1/4	M <sub>U</sub>	3289	3547	3790	4018	4230	3916	4193	4454	4700	4285	4595	
		R <sub>KI</sub>	1941	2019	2097	2175	2252	2437	2531	2625	2719	2895	3006	
	n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83		

T & S t <sub>f</sub> = 6-in. L6x4x <sub>t</sub>	Web 2L4x3.5 t <sub>a</sub>	A36 3/4-in. Dia.	Beam											
			W36			W40			W44					
			8 row	9 row	6 row	7 row	8 row	9 row	6 row	7 row	8 row	9 row		
3/4	1/2	M <sub>U</sub>	11960	12711	11537	12438	13315	14169	12686	13690	14670	15627		
		R <sub>KI</sub>	13216	13856	14674	15461	16248	17035	17694	18643	19593	20542		
	n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83			
	3/8	M <sub>U</sub>	9728	10205	9672	10262	10831	11379	10633	11294	11934	12553		
		R <sub>KI</sub>	10141	10388	11858	12162	12467	12771	14298	14666	15033	15400		
	n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83			
	5/16	M <sub>U</sub>	8941	9332	8995	9480	9947	10397	9884	10428	10954	11462		
		R <sub>KI</sub>	10046	10282	11771	12061	12350	12640	14194	14543	14892	15242		
	n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83			
	1/4	M <sub>U</sub>	8014	8297	8209	8568	8911	9239	9018	9421	9809	10181		
		R <sub>KI</sub>	9094	9208	10899	11039	11179	11319	13142	13311	13480	13649		
	n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83			
5/8	1/2	M <sub>U</sub>	10541	11289	9982	10880	11754	12604	10989	11989	12966	13920		
		R <sub>KI</sub>	9412	10048	10014	10797	11579	12361	12083	13027	13971	14915		
	n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83			
	3/8	M <sub>U</sub>	8317	8792	8122	8710	9277	9823	8941	9600	10238	10855		
		R <sub>KI</sub>	6358	6603	7216	7518	7821	8124	8706	9071	9436	9801		



T & S $t_f = 6\text{-in.}$ $L_6 \times 4 \times t_f$	Web $2L_4 \times 3.5$ $t_a$	A36 $\frac{3}{4}\text{-in.}$ Dia.	Beam																																			
			W8			W10			W12			W14			W16			W18																				
			2 row	3 row	4 row	2 row	3 row	4 row	2 row	3 row	4 row	2 row	3 row	4 row	2 row	3 row	4 row	2 row	3 row	4 row																		
$\frac{3}{4}$	$\frac{1}{2}$	$M_U$	1712	2065	2253	2417	2654	3054	3454	3759	3854	4207	4532	$R_{ki}$	398	596	622	836	873	1165	1501	1564	1879	1958	2038	$n$	1.33	1.2	1.22	1.09	1.12	1.03	0.95	0.97	0.88	0.91	0.93	
		$M_U$	1605	1931	2061	2256	2421	2781	3140	3351	3500	3746	3969	$R_{ki}$	384	575	591	806	828	1106	1424	1462	1783	1831	1878	$n$	1.31	1.18	1.2	1.07	1.09	1	0.92	0.95	0.85	0.88	0.9	
		$M_U$	1552	1864	1964	2176	2304	2643	2983	3147	3322	3514	3686	$R_{ki}$	374	561	570	787	799	1067	1373	1394	1719	1745	1772	$n$	1.31	1.17	1.19	1.06	1.09	0.99	0.91	0.94	0.84	0.87	0.88	
		$M_U$	1507	1808	1885	2108	2207	2529	2851	2978	3173	3322	3455	$R_{ki}$	372	558	565	782	791	1056	1360	1377	1703	1724	1744	$n$	1.29	1.16	1.17	1.04	1.07	0.97	0.89	0.91	0.83	0.84	0.86	
		$M_U$	1308	1588	1774	1869	2102	2430	2758	3060	3066	3436	3759	$R_{ki}$	226	341	367	480	516	691	891	954	1117	1196	1274	$n$	1.51	1.38	1.4	1.27	1.3	1.21	1.13	1.15	1.06	1.08	1.1	
		$M_U$	1203	1456	1584	1710	1872	2160	2448	2657	2735	2979	3200	$R_{ki}$	213	320	336	451	472	632	816	853	1023	1070	1117	$n$	1.5	1.36	1.38	1.25	1.28	1.19	1.11	1.13	1.04	1.06	1.08	
	$\frac{5}{8}$	$\frac{1}{2}$	$M_U$	1150	1390	1489	1630	1756	2024	2291	2453	2559	2749	2919	$R_{ki}$	204	307	315	431	443	593	765	786	960	986	1012	$n$	1.49	1.36	1.39	1.25	1.28	1.19	1.11	1.13	1.04	1.06	1.09
			$M_U$	1106	1335	1411	1563	1661	1911	2161	2286	2411	2558	2690	$R_{ki}$	201	303	310	426	436	583	753	769	943	964	985	$n$	1.48	1.34	1.36	1.23	1.25	1.16	1.08	1.1	1.01	1.03	1.05
			$M_U$	1010	1227	1354	1445	1606	1858	2110	2318	2362	2604	2824	$R_{ki}$	154	232	248	327	349	468	604	641	758	805	851	$n$	1.59	1.45	1.47	1.34	1.37	1.28	1.2	1.22	1.13	1.16	1.17
		$\frac{5}{16}$	$M_U$	957	1161	1259	1365	1491	1722	1954	2115	2186	2375	2544	$R_{ki}$	145	219	227	308	320	429	554	575	695	721	747	$n$	1.59	1.46	1.48	1.35	1.38	1.29	1.21	1.23	1.14	1.17	1.19
			$M_U$	914	1106	1182	1299	1396	1610	1824	1949	2038	2185	2316	$R_{ki}$	143	215	222	303	313	419	541	558	679	700	720	$n$	1.57	1.44	1.46	1.33	1.35	1.26	1.18	1.2	1.11	1.13	1.15
			$M_U$	1056	1293	1476	1530	1760	2045	2330	2629	2614	2961	3281	$R_{ki}$	170	258	283	365	400	537	695	757	873	951	1028	$n$	1.55	1.42	1.45	1.31	1.34	1.25	1.18	1.2	1.11	1.13	1.15
$\frac{1}{2}$	$\frac{1}{2}$	$M_U$	952	1162	1288	1372	1532	1777	2021	2228	2266	2507	2726	$R_{ki}$	157	238	253	336	357	480	621	658	780	826	873	$n$	1.54	1.41	1.43	1.3	1.33	1.24	1.16	1.18	1.09	1.12	1.13	
		$M_U$	900	1097	1194	1293	1418	1642	1866	2027	2090	2279	2447	$R_{ki}$	148	225	233	317	329	442	571	592	718	743	769	$n$	1.54	1.41	1.44	1.3	1.33	1.24	1.16	1.19	1.09	1.12	1.15	
		$M_U$	857	1042	1117	1227	1324	1530	1737	1861	1943	2089	2220	$R_{ki}$	146	221	228	312	322	432	559	575	702	722	743	$n$	1.52	1.38	1.41	1.27	1.3	1.21	1.13	1.16	1.06	1.09	1.11	
		$M_U$	873	1074	1256	1276	1505	1755	2004	2301	2253	2599	2917	$R_{ki}$	119	182	207	257	293	394	510	571	641	718	795	$n$	1.65	1.52	1.54	1.41	1.44	1.35	1.27	1.29	1.21	1.22	1.23	
		$M_U$	770	945	1070	1120	1279	1488	1697	1903	1906	2146	2364	$R_{ki}$	107	162	177	229	250	337	436	473	548	594	640	$n$	1.65	1.51	1.54	1.41	1.43	1.34	1.27	1.29	1.2	1.22	1.24	
		$M_U$	719	880	976	1041	1165	1354	1542	1702	1731	1919	2086	$R_{ki}$	98	149	157	211	222	299	387	407	486	512	537	$n$	1.65	1.52	1.55	1.41	1.45	1.36	1.28	1.31	1.21	1.24	1.27	
	$\frac{7}{16}$	$\frac{1}{2}$	$M_U$	676	826	900	975	1071	1242	1413	1537	1585	1730	1860	$R_{ki}$	96	145	152	206	215	289	374	390	470	491	511	$n$	1.63	1.5	1.52	1.39	1.42	1.33	1.25	1.27	1.18	1.21	1.23
			$M_U$	708	878	1057	1047	1275	1492	1709	2005	1926	2270	2586	$R_{ki}$	84	128	152	182	216	291	378	439	475	552	628	$n$	1.74	1.61	1.62	1.51	1.52	1.43	1.36	1.37	1.29	1.3	1.3
			$M_U$	607	749	872	891	1049	1226	1403	1608	1580	1819	2036	$R_{ki}$	71	108	123	154	175	235	305	341	383	429	475	$n$	1.75	1.62	1.63	1.51	1.53	1.45	1.37	1.38	1.3	1.32	1.33
		$\frac{5}{16}$	$M_U$	555	684	779	813	936	1093	1249	1406	1406	1592	1759	$R_{ki}$	63	95	104	135	147	198	256	276	322	347	373	$n$	1.77	1.64	1.67	1.53	1.57	1.48	1.41	1.43	1.34	1.37	1.38
			$M_U$	513	630	704	748	843	982	1121	1244	1260	1404	1533	$R_{ki}$	60	92	99	130	140	188	243	259	306	326	347	$n$	1.74	1.61	1.64	1.5	1.54	1.45	1.37	1.39	1.3	1.33	1.35

T & S $t_f = 6\text{-in.}$ $L_6 \times 4 \times t_f$	Web $2L_4 \times 3.5$ $t_a$	A36 $\frac{3}{4}\text{-in.}$ Dia.	Beam																																			
			W21			W24			W27																													
			3 row	4 row	5 row	3 row	4 row	5 row	6 row	7 row	5 row	6 row	7 row	8 row	5 row	6 row	7 row	8 row																				
$\frac{3}{4}$	$\frac{1}{2}$	$M_U$	4878	5276	5646	5550	6019	6461	6875	6763	7276	7762	8221	$R_{ki}$	2633	2740	2847	3407	3546	3684	3823	4455	4630	4804	4979	$n$	0.83	0.84	0.86	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
		$M_U$	4337	4612	4865	4928	5255	5560	5843	5898	6254	6589	6901	$R_{ki}$	2461	2525	2589	3184	3267	3351	3434	4106	4210	4315	4419	$n$	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	
		$M_U$	4065	4278	4473	4616	4871	5107	5323	5463	5740	5998	6237	$R_{ki}$	2346	2382	2417	3036	3082	3128	3174	3872	3930	3988	4046	$n$	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	
		$M_U$	3837	4003	4153	4353	4551	4734	4901	5100	5315	5514	5698	$R_{ki}$	2317	2345	2373	2998	3034	3071	3107	3812	3858	3904	3950	$n$	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	
		$M_U$	4000	4394	4761	4564	5030	5468	5880	5665	6176	6659	7115	$R_{ki}$	1610	1716	1822	2087	2224	2362	2499	2798	2971	3144	3317	$n$	0.99	1.01	1.03	0.92	0.94	0.95	0.96	0.87	0.89	0.9	0.91	
		$M_U$	3462	3735	3986	3945	4270	4572	4853	4804	5159	5491	5801	$R_{ki}$	1441	1504	1568	1867	1949	2031	2114	2452	2556	2659	2763	$n$	0.97	0.99	1.01	0.9	0.92	0.93	0.95	0.85	0.87	0.88	0.89	
	$\frac{5}{8}$	$\frac{1}{2}$	$M_U$	3191	3403	3596	3634	3888	4122	4337	4372	4647	4904	5141	$R_{ki}$	1327	1362	1398	1720	1765	1811	1857	2278	2335	2393	$n$	0.97	1	1.02	0.9	0.92	0.94	0.96	0.85	0.87	0.89	0.91	
			$M_U$	2966	3130	3278	3373	3570	3751	3917	4101	4224	4422	4604	$R_{ki}$	1298	1326	1354	1682	1718	1754	1791	2110	2207	2252	2298	$n$	0.94	0.96	0.98	0.86	0.89	0.9	0.92	0.83	0.84	0.85	0.86
			$M_U$	3570	3962	4328	4080	4544	4981	5391	5126	5635	6116	6571	$R_{ki}$	1253	1359	1464	1626	1762	1899	2036	2218	2390	2562	2735	$n$	1.08	1.09	1.1	1	1.02	1.03	1.03	0.95	0.96	0.97	0.97
		$\frac{5}{16}$	$M_U$	3033	3305	3555	3463	3786	4088	4367	4267	4620	4951	5261	$R_{ki}$	1085	1148	1211	1406	1488	1570	1652	1873	1976	2080	2183	$n$	1.07	1.08	1.1	0.99	1.02	1.02	1.03	0.94	0.96	0.97	0.98
			$M_U$	2764	2975	3167	3153	3405	3638	3852	3836	4110	4366	4602	$R_{ki}$	972	1007	1042	1260	1305	1351	1396	1643	1700	1757	1814	$n$	1.08	1.1	1.12	1	1.02	1.04	1.06	0.96	0.98	0.99	1.01
			$M_U$	2538	2702	2850	2892	3088	3269	3434	3475</																											

T & S t <sub>f</sub> = 6-in. L6x4x <sub>t</sub>	Web 2L4x3.5 t <sub>a</sub>	A36 3/4-in. Dia.	Beam																	
			W27					W30					W33				W36			
			9 row	6 row	7 row	8 row	9 row	6 row	7 row	8 row	9 row	6 row	7 row	8 row	9 row	6 row	7 row			
3/4	1/2	M <sub>U</sub>	7506	8091	8649	9180	9683	8906	9536	10138	10713	9722	10423							
		R <sub>KI</sub>	5469	5683	5897	6112	6326	6845	7103	7361	7619	8114	8420							
		n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83							
	3/8	M <sub>U</sub>	6541	6948	7334	7699	8041	7643	8080	8496	8890	8337	8826							
		R <sub>KI</sub>	5040	5168	5296	5425	5553	6224	6379	6534	6688	7378	7562							
		n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83							
	5/16	M <sub>U</sub>	6055	6374	6673	6954	7215	7008	7349	7670	7973	7641	8024							
		R <sub>KI</sub>	4753	4824	4895	4966	5037	5810	5895	5981	6067	6887	6989							
		n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83							
	1/4	M <sub>U</sub>	5648	5895	6127	6344	6544	6476	6741	6990	7223	7057	7354							
		R <sub>KI</sub>	4680	4736	4792	4849	4905	5704	5771	5839	5907	6761	6842							
		n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83							
5/8	1/2	M <sub>U</sub>	6301	6883	7438	7965	8466	7590	8216	8816	9388	8297	8995							
		R <sub>KI</sub>	3438	3651	3863	4076	4288	4400	4656	4912	5169	5219	5523							
		n	0.83	0.83	0.84	0.85	0.85	0.83	0.83	0.83	0.83	0.83	0.83							
	3/8	M <sub>U</sub>	5339	5745	6129	6491	6831	6331	6767	7180	7572	6918	7405							
		R <sub>KI</sub>	3012	3140	3267	3394	3522	3784	3938	4091	4245	4489	4671							
		n	0.83	0.83	0.83	0.84	0.84	0.83	0.83	0.83	0.83	0.83	0.83							
	5/16	M <sub>U</sub>	4856	5173	5471	5749	6009	5699	6038	6358	6658	6224	6605							
		R <sub>KI</sub>	2728	2799	2869	2940	3010	3373	3458	3543	3628	4001	4101							
		n	0.83	0.83	0.83	0.85	0.86	0.83	0.83	0.83	0.83	0.83	0.83							
	1/4	M <sub>U</sub>	4450	4697	4927	5142	5341	5170	5433	5680	5912	5642	5938							
		R <sub>KI</sub>	2655	2711	2767	2823	2879	3267	3335	3402	3470	3876	3956							
		n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83							
9/16	1/2	M <sub>U</sub>	5707	6288	6841	7367	7866	6941	7566	8164	8735	7595	8291							
		R <sub>KI</sub>	2727	2938	3150	3362	3573	3543	3798	4053	4308	4204	4507							
		n	0.89	0.9	0.91	0.92	0.92	0.85	0.86	0.87	0.87	0.83	0.83							
	3/8	M <sub>U</sub>	4748	5153	5536	5896	6235	5685	6120	6532	6923	6218	6704							
		R <sub>KI</sub>	2302	2429	2556	2683	2810	2929	3082	3235	3388	3475	3657							
		n	0.88	0.9	0.91	0.92	0.93	0.84	0.86	0.87	0.88	0.83	0.83							
	5/16	M <sub>U</sub>	4266	4582	4879	5157	5415	5054	5392	5711	6011	5526	5905							
		R <sub>KI</sub>	2019	2090	2160	2230	2300	2519	2604	2689	2773	2989	3090							
		n	0.9	0.92	0.94	0.95	0.96	0.86	0.88	0.9	0.91	0.83	0.84							
	1/4	M <sub>U</sub>	3861	4107	4337	4551	4749	4526	4788	5035	5266	4945	5240							
		R <sub>KI</sub>	1947	2002	2058	2114	2170	2414	2481	2549	2616	2864	2944							
		n	0.86	0.88	0.89	0.91	0.92	0.83	0.84	0.86	0.87	0.83	0.83							
1/2	1/2	M <sub>U</sub>	5562	6141	6693	7218	7715	6783	7407	8003	8572	7425	8120							
		R <sub>KI</sub>	2791	3001	3212	3423	3634	3620	3875	4129	4383	4297	4599							
		n	0.86	0.88	0.89	0.89	0.9	0.83	0.84	0.84	0.85	0.83	0.83							
	3/8	M <sub>U</sub>	4605	5008	5390	5750	6088	5530	5963	6374	6764	6051	6536							
		R <sub>KI</sub>	2368	2495	2621	2747	2874	3009	3161	3314	3466	3572	3753							
		n	0.85	0.87	0.88	0.89	0.9	0.83	0.83	0.84	0.85	0.83	0.83							
	5/16	M <sub>U</sub>	4124	4439	4735	5012	5269	4900	5237	5555	5854	5360	5739							
		R <sub>KI</sub>	2086	2156	2226	2296	2366	2601	2685	2770	2854	3087	3187							
		n	0.86	0.88	0.9	0.92	0.93	0.83	0.85	0.86	0.88	0.83	0.83							
	1/4	M <sub>U</sub>	3720	3965	4194	4408	4606	4373	4635	4881	5111	4780	5075							
		R <sub>KI</sub>	2014	2069	2125	2180	2236	2496	2563	2630	2697	2963	3042							
		n	0.83	0.84	0.85	0.87	0.88	0.83	0.83	0.83	0.83	0.83	0.83							
7/16	1/2	M <sub>U</sub>	4986	5564	6114	6637	7133	6153	6775	7370	7937	6742	7436							
		R <sub>KI</sub>	2163	2373	2583	2793	3003	2863	3117	3370	3623	3400	3701							
		n	0.95	0.96	0.97	0.97	0.97	0.91	0.91	0.92	0.92	0.86	0.87							
	3/8	M <sub>U</sub>	4031	4434	4814	5173	5510	4902	5334	5744	6133	5370	5854							
		R <sub>KI</sub>	1742	1868	1994	2120	2246	2254	2406	2558	2710	2677	2857							
		n	0.95	0.97	0.98	0.98	0.99	0.91	0.93	0.93	0.94	0.86	0.88							
	5/16	M <sub>U</sub>	3551	3865	4161	4437	4693	4273	4610	4927	5225	4681	5059							
		R <sub>KI</sub>	1462	1531	1601	1671	1740	1848	1932	2016	2100	2194	2293							
		n	0.98	1	1.02	1.04	1.04	0.95	0.97	0.98	1	0.9	0.92							
	1/4	M <sub>U</sub>	3148	3392	3621	3834	4031	3747	4008	4254	4484	4102	4396							
		R <sub>KI</sub>	1390	1445	1500	1555	1611	1743	1810	1877	1943	2070	2149							
		n	0.94	0.96	0.98	0.99	1	0.91	0.92	0.94	0.95	0.86	0.88							
3/8	1/2	M <sub>U</sub>	4462	5038	5587	6108	6603	5579	6199	6792	7359	6119	6811							
		R <sub>KI</sub>	1715	1924	2133	2342	2551	2323	2575	2827	3080	2759	3058							
		n	1.02	1.03	1.03	1.02	1.02	0.97	0.98	0.97	0.97	0.93	0.93							
	3/8	M <sub>U</sub>	3509	3910	4290	4648	4983	4330	4761	5170	5558	4750	5233							
		R <sub>KI</sub>	1296	1421	1547	1672	1797	1716	1867	2018	2169	2038	2217							
		n	1.05	1.06	1.06	1.06	1.06	1	1.01	1.01	1.01	0.96	0.96							
	5/16	M <sub>U</sub>	3030	3343	3638	3913	4169	3703	4038	4355	4652	4062	4439							
		R <sub>KI</sub>	1016	1086	1155	1224	1294	1310	1394	1478	1562	1556	1656							
		n	1.11	1.13	1.14	1.15	1.15	1.07	1.09	1.1	1.1	1.02	1.04							
	1/4	M <sub>U</sub>	2628	2872	3099	3312	3508	3178	3438	3683	3912	3484	3777							
		R <sub>KI</sub>	945	1000	1055	1110	1165	1207	1273	1339	1406	1433	1512							
		n	1.06	1.08	1.1	1.11	1.11	1.03	1.05	1.06	1.06	0.98	1							

T & S t <sub>f</sub> = 6-in. L6x4x <sub>t</sub>	Web 2L4x3.5 t <sub>a</sub>	A36 3/4-in. Dia.	Beam											
			W36				W40				W44			
			8 row	9 row	6 row	7 row	8 row	9 row	6 row	7 row	8 row	9 row	6 row	7 row
3/4	1/2	M <sub>U</sub>	11097	11743	10809	11605	12375	13117	11895	12788	13653	14491		
		R <sub>KI</sub>	8726	9032	9975	10351	10728	11104	12028	12482	12935	13389		
		n	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83		
	3/8	M <sub>U</sub>	9293	9739	9263	9821	10357	10871	10189	10815	11420	12003		
		R <sub>KI</sub>	7745	7929	9070	9296	9521	9747	10937	11209	11481	11753		
		n	0.83	0.83	0.83	0.83	0							