

# Column Base Plate Design Table

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The column base plate design procedure given in AISC ASD Ninth Edition manual<sup>1</sup> differs considerably from the Eighth Edition manual.<sup>2</sup> Additionally, the procedure contained in the first printing of the Ninth Edition manual has been refined in the later printings of the manual to incorporate improvements proposed by Thornton.<sup>3,4</sup> These changes result in lighter base plates under certain conditions of loading and base plate geometry. The purpose of this paper is to provide a design table that includes AISC Ninth as well as Eighth Edition base plates, and to compare the two designs.

The basis for the design method contained in the AISC manual has been discussed in detail by others,<sup>3,4,5</sup> and will not be repeated here.

The table is generated for plate  $F_y$  of 36 ksi and concrete  $f'_c$  of 4.0 ksi. The concrete Bearing Area Factor in the table refers to the quantity  $\sqrt{A_2/A_1}$  in the AISC manual. Three values of this quantity are considered: 1.0, 1.5, and 2.0. The corresponding concrete allowable bearing stress ( $F_b$ ) is also given.

The table values are:

- base plate width  $B$  parallel to column flange,
- base plate width  $N$  parallel to column web,
- base plate thickness  $t_8$  in accordance with AISC Eighth Edition manual, and
- base plate thickness  $t_9$  in accordance with AISC Ninth Edition manual (latest printing).

Where plate thickness  $t_8$  differs from  $t_9$ , the table values are highlighted. Base plate widths  $B$  and  $N$  remain unchanged from Eighth to Ninth Editions of the manual. These widths are rounded to whole inches in the table. A minimum plate thickness of 1 in. has been used, as it is customary in industrial buildings due to heavier loads. Likewise a thickness increment of  $\frac{1}{4}$ -in. is used. In the interest of space, only the W14 sections are included in the table.

A study of this table shows that the AISC Ninth Edition method always produces the same or lighter base plate compared to the AISC Eighth Edition manual. It is also apparent

that lighter columns are more likely to produce savings in base plate thickness than the heavier columns. Similarly, savings are more likely at higher allowable concrete bearing stress  $F_b$  than at lower  $F_b$ .

For a given column, the savings in base plate thickness is more pronounced in the lower load range. In this load range the design is controlled by the bending stress of the plate inside the column footprint (Column  $b_f \times d$ ). The plate stress inside the foot-print is evaluated using either the Murray Stockwell equivalent static load method<sup>3,5</sup> or Thornton's yield line method<sup>3,4</sup> in the Ninth Edition manual. The Eighth Edition manual uses elastic analysis to calculate the same stress. The new methods used in the Ninth Edition manual account for the savings in plate thickness. The table shows that this saving can be quite significant in a number of cases. At higher loads, however, the base plate has to extend outside the column footprint to satisfy the concrete bearing stress limit. As a result plate cantilevers outside the column footprint (cantilever dimensions  $m$  and  $n$  in the AISC manual) control design, and therefore, the Ninth Edition manual leads to the same design as the Eighth Edition manual.

## REFERENCES

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Column Base Plate Design Table											$f_c' = 4.0 \text{ ksi}$	
For plates thicker than 8 in., $F_y$ of 32 ksi is used											Plate $F_y = 36 \text{ ksi}$	
Column Load (kips)	Bearing Area Factor (Allowable Bearing Stress)											
	1.0 ( $F_p = 1400 \text{ psi}$ )				1.5 ( $F_p = 2100 \text{ psi}$ )				2.0 ( $F_p = 2800 \text{ psi}$ )			
	B, in.	N, in.	$t_8$ , in.	$t_9$ , in.	B, in.	N, in.	$t_8$ , in.	$t_9$ , in.	B, in.	N, in.	$t_8$ , in.	$t_9$ , in.
<b>W14x730</b>												
6450	65	71	10 $\frac{3}{4}$	10 $\frac{3}{4}$	53	59	10	10	45	52	9 $\frac{1}{4}$	9 $\frac{1}{4}$
6000	63	69	10 $\frac{1}{4}$	10 $\frac{1}{4}$	51	57	9 $\frac{1}{2}$	9 $\frac{1}{2}$	43	50	8 $\frac{1}{2}$	8 $\frac{1}{2}$
5500	60	66	9 $\frac{3}{4}$	9 $\frac{3}{4}$	48	55	8 $\frac{3}{4}$	8 $\frac{3}{4}$	41	48	7 $\frac{1}{2}$	7 $\frac{1}{2}$
5000	57	63	9	9	46	52	8 $\frac{1}{4}$	8 $\frac{1}{4}$	39	46	7	7
4500	54	60	8	8	43	50	7	7	37	44	6 $\frac{1}{2}$	6 $\frac{1}{2}$
4250	52	59	7 $\frac{1}{2}$	7 $\frac{1}{2}$	42	49	6 $\frac{3}{4}$	6 $\frac{3}{4}$	36	43	6	6
4000	51	57	7 $\frac{1}{4}$	7 $\frac{1}{4}$	41	47	6 $\frac{1}{2}$	6 $\frac{1}{2}$	35	41	6	6
3750	49	55	7	7	39	46	6	6	34	40	5 $\frac{1}{2}$	5 $\frac{1}{2}$
3500	47	54	6 $\frac{1}{2}$	6 $\frac{1}{2}$	38	44	5 $\frac{3}{4}$	5 $\frac{3}{4}$	33	39	5 $\frac{1}{4}$	5 $\frac{1}{4}$
3250	45	52	6 $\frac{1}{4}$	6 $\frac{1}{4}$	36	43	5 $\frac{1}{4}$	5 $\frac{1}{4}$	31	38	4 $\frac{3}{4}$	4 $\frac{3}{4}$
3000	43	50	5 $\frac{3}{4}$	5 $\frac{3}{4}$	35	41	5	5	30	36	4 $\frac{1}{2}$	4 $\frac{1}{2}$
2750	41	48	5 $\frac{1}{2}$	5 $\frac{1}{2}$	33	40	4 $\frac{1}{2}$	4 $\frac{1}{2}$	29	35	4 $\frac{1}{4}$	4 $\frac{1}{4}$
2500	39	46	5	5	32	38	4 $\frac{1}{4}$	4 $\frac{1}{4}$	27	34	3 $\frac{1}{2}$	3 $\frac{1}{2}$
2250	37	44	4 $\frac{1}{2}$	4 $\frac{1}{2}$	30	36	4	4	26	32	3 $\frac{1}{4}$	3 $\frac{1}{4}$
2000	35	41	4 $\frac{1}{4}$	4 $\frac{1}{4}$	28	35	3 $\frac{1}{2}$	3 $\frac{1}{2}$	24	30	3 $\frac{1}{4}$	3
1750	33	39	3 $\frac{3}{4}$	3 $\frac{3}{4}$	26	33	3	3	22	29	3 $\frac{1}{4}$	3
1500	30	36	3 $\frac{1}{4}$	3 $\frac{1}{4}$	24	30	3	2 $\frac{1}{2}$	20	27	3 $\frac{1}{4}$	3
1250	27	34	2 $\frac{1}{2}$	2 $\frac{1}{2}$	22	28	2 $\frac{3}{4}$	2 $\frac{3}{4}$	20	25	3 $\frac{1}{4}$	2 $\frac{3}{4}$
1000	24	30	2 $\frac{1}{2}$	2	20	26	2 $\frac{3}{4}$	2 $\frac{3}{4}$	20	24	3	2 $\frac{1}{2}$
750	20	27	2 $\frac{1}{2}$	2	20	24	2 $\frac{1}{2}$	2 $\frac{1}{4}$	20	24	2 $\frac{1}{2}$	2
<b>W14x665</b>												
5880	62	68	10	10	50	56	9 $\frac{1}{4}$	9 $\frac{1}{4}$	43	49	8 $\frac{3}{4}$	8 $\frac{3}{4}$
5500	60	66	9 $\frac{3}{4}$	9 $\frac{3}{4}$	49	54	9	9	41	48	8 $\frac{1}{4}$	8 $\frac{1}{4}$
5000	57	63	9	9	46	52	8 $\frac{1}{4}$	8 $\frac{1}{4}$	39	46	7 $\frac{1}{4}$	7 $\frac{1}{4}$
4500	54	60	8	8	43	50	7 $\frac{1}{4}$	7 $\frac{1}{4}$	38	43	6 $\frac{3}{4}$	6 $\frac{3}{4}$
4250	53	58	7 $\frac{3}{4}$	7 $\frac{3}{4}$	43	48	7	7	37	42	6 $\frac{1}{2}$	6 $\frac{1}{2}$
4000	51	57	7 $\frac{1}{4}$	7 $\frac{1}{4}$	41	47	6 $\frac{1}{2}$	6 $\frac{1}{2}$	35	41	6	6
3750	49	55	7	7	39	46	6 $\frac{1}{4}$	6 $\frac{1}{4}$	34	40	5 $\frac{3}{4}$	5 $\frac{3}{4}$
3500	48	53	6 $\frac{3}{4}$	6 $\frac{3}{4}$	38	44	6	6	33	39	5 $\frac{1}{4}$	5 $\frac{1}{4}$
3250	45	52	6 $\frac{1}{4}$	6 $\frac{1}{4}$	36	43	5 $\frac{1}{2}$	5 $\frac{1}{2}$	32	37	5	5
3000	43	50	6	6	35	41	5 $\frac{1}{4}$	5 $\frac{1}{4}$	30	36	4 $\frac{1}{2}$	4 $\frac{1}{2}$
2750	41	48	5 $\frac{1}{2}$	5 $\frac{1}{2}$	33	40	4 $\frac{3}{4}$	4 $\frac{3}{4}$	29	35	4 $\frac{1}{4}$	4 $\frac{1}{4}$
2500	39	46	5 $\frac{1}{4}$	5 $\frac{1}{4}$	32	38	4 $\frac{1}{2}$	4 $\frac{1}{2}$	28	33	4	4
2250	38	43	4 $\frac{3}{4}$	4 $\frac{3}{4}$	30	36	4	4	26	32	3 $\frac{1}{2}$	3 $\frac{1}{2}$
2000	35	41	4 $\frac{1}{4}$	4 $\frac{1}{4}$	29	34	3 $\frac{3}{4}$	3 $\frac{3}{4}$	24	30	3 $\frac{1}{4}$	2 $\frac{3}{4}$
1750	33	39	3 $\frac{3}{4}$	3 $\frac{3}{4}$	27	32	3 $\frac{1}{4}$	3 $\frac{1}{4}$	23	28	3 $\frac{1}{4}$	2 $\frac{3}{4}$
1500	30	36	3 $\frac{1}{4}$	3 $\frac{1}{4}$	24	30	3	2 $\frac{1}{2}$	20	27	3 $\frac{1}{4}$	2 $\frac{3}{4}$
1250	28	33	2 $\frac{3}{4}$	2 $\frac{3}{4}$	22	28	2 $\frac{3}{4}$	2 $\frac{3}{4}$	20	25	3 $\frac{1}{4}$	2 $\frac{3}{4}$
1000	24	30	2 $\frac{1}{2}$	2	20	25	2 $\frac{3}{4}$	2 $\frac{1}{2}$	20	24	3	2 $\frac{1}{2}$
750	20	27	2 $\frac{1}{2}$	2	20	24	2 $\frac{1}{2}$	2 $\frac{1}{4}$	20	24	2 $\frac{1}{2}$	2
<b>W14x605</b>												
5340	59	65	9 $\frac{1}{2}$	9 $\frac{1}{2}$	48	53	8 $\frac{3}{4}$	8 $\frac{3}{4}$	41	47	7 $\frac{3}{4}$	7 $\frac{3}{4}$
5000	57	63	9	9	46	52	8 $\frac{1}{4}$	8 $\frac{1}{4}$	40	45	7 $\frac{1}{4}$	7 $\frac{1}{4}$
4500	54	60	8	8	44	49	7 $\frac{1}{4}$	7 $\frac{1}{4}$	38	43	6 $\frac{3}{4}$	6 $\frac{3}{4}$
4250	53	58	7 $\frac{3}{4}$	7 $\frac{3}{4}$	43	48	7	7	37	42	6 $\frac{1}{2}$	6 $\frac{1}{2}$
4000	51	57	7 $\frac{1}{2}$	7 $\frac{1}{2}$	41	47	6 $\frac{3}{4}$	6 $\frac{3}{4}$	35	41	6	6
3750	49	55	7	7	40	45	6 $\frac{1}{2}$	6 $\frac{1}{2}$	34	40	5 $\frac{3}{4}$	5 $\frac{3}{4}$
3500	48	53	6 $\frac{3}{4}$	6 $\frac{3}{4}$	38	44	6	6	33	38	5 $\frac{1}{2}$	5 $\frac{1}{2}$
3250	46	51	6 $\frac{1}{2}$	6 $\frac{1}{2}$	37	42	5 $\frac{3}{4}$	5 $\frac{3}{4}$	32	37	5	5
3000	44	49	6	6	35	41	5 $\frac{1}{4}$	5 $\frac{1}{4}$	30	36	4 $\frac{1}{2}$	4 $\frac{1}{2}$
2750	42	47	5 $\frac{3}{4}$	5 $\frac{3}{4}$	34	39	5	5	29	34	4 $\frac{1}{4}$	4 $\frac{1}{4}$
Note: Shaded values indicate that Ninth Edition design differs from Eighth Edition.												

Column Base Plate Design Table (cont.)											$f'_C = 4.0 \text{ ksi}$	
For plates thicker than 8 in., $F_y$ of 32 ksi is used											Plate $F_y = 36 \text{ ksi}$	
Column Load (kips)	Bearing Area Factor (Allowable Bearing Stress)											
	1.0 ( $F_p = 1400 \text{ psi}$ )				1.5 ( $F_p = 2100 \text{ psi}$ )				2.0 ( $F_p = 2800 \text{ psi}$ )			
	$B$ , in.	$N$ , in.	$t_8$ , in.	$t_9$ , in.	$B$ , in.	$N$ , in.	$t_8$ , in.	$t_9$ , in.	$B$ , in.	$N$ , in.	$t_8$ , in.	$t_9$ , in.
2500	40	45	$5\frac{1}{4}$	$5\frac{1}{4}$	32	38	$4\frac{1}{2}$	$4\frac{1}{2}$	28	33	4	4
2250	38	43	$4\frac{3}{4}$	$4\frac{3}{4}$	30	36	4	4	26	31	$3\frac{1}{2}$	$3\frac{1}{2}$
2000	35	41	$4\frac{1}{4}$	$4\frac{1}{4}$	29	34	$3\frac{3}{4}$	$3\frac{3}{4}$	24	30	$3\frac{1}{4}$	3
1750	33	38	4	4	27	32	$3\frac{1}{4}$	$3\frac{1}{4}$	23	28	$3\frac{1}{4}$	$2\frac{3}{4}$
1500	30	36	$3\frac{1}{4}$	$3\frac{1}{4}$	24	30	3	$2\frac{1}{2}$	21	26	$3\frac{1}{4}$	$2\frac{3}{4}$
1250	28	33	$2\frac{3}{4}$	$2\frac{3}{4}$	22	28	$2\frac{1}{4}$	$2\frac{1}{4}$	19	24	$3\frac{1}{4}$	$2\frac{3}{4}$
1000	24	30	$2\frac{1}{2}$	2	20	25	$2\frac{1}{4}$	$2\frac{1}{4}$	19	23	3	$2\frac{1}{2}$
750	21	26	$2\frac{1}{2}$	2	19	23	$2\frac{1}{4}$	$2\frac{1}{4}$	19	23	$2\frac{1}{4}$	2
W14X550												
4860	56	62	9	9	46	51	$8\frac{1}{4}$	$8\frac{1}{4}$	40	44	$7\frac{1}{2}$	$7\frac{1}{2}$
4500	55	59	$8\frac{3}{4}$	$8\frac{3}{4}$	44	49	$7\frac{1}{2}$	$7\frac{1}{2}$	38	43	$6\frac{3}{4}$	$6\frac{3}{4}$
4250	53	58	$7\frac{3}{4}$	$7\frac{3}{4}$	43	48	7	7	37	42	$6\frac{1}{2}$	$6\frac{1}{2}$
4000	52	56	$7\frac{1}{2}$	$7\frac{1}{2}$	42	46	7	7	35	41	$6\frac{1}{4}$	$6\frac{1}{4}$
3750	49	55	$7\frac{1}{4}$	$7\frac{1}{4}$	40	45	$6\frac{1}{2}$	$6\frac{1}{2}$	35	39	6	6
3500	48	53	$6\frac{3}{4}$	$6\frac{3}{4}$	38	44	6	6	33	38	$5\frac{1}{2}$	$5\frac{1}{2}$
3250	46	51	$6\frac{1}{2}$	$6\frac{1}{2}$	37	42	$5\frac{3}{4}$	$5\frac{3}{4}$	32	37	$5\frac{1}{4}$	$5\frac{1}{4}$
3000	44	49	6	6	35	41	$5\frac{1}{4}$	$5\frac{1}{4}$	30	36	$4\frac{3}{4}$	$4\frac{3}{4}$
2750	42	47	$5\frac{3}{4}$	$5\frac{3}{4}$	34	39	5	5	29	34	$4\frac{1}{4}$	$4\frac{1}{4}$
2500	40	45	$5\frac{1}{4}$	$5\frac{1}{4}$	33	37	$4\frac{3}{4}$	$4\frac{3}{4}$	28	33	4	4
2250	38	43	$4\frac{3}{4}$	$4\frac{3}{4}$	30	36	$4\frac{1}{4}$	$4\frac{1}{4}$	26	31	$3\frac{1}{2}$	$3\frac{1}{2}$
2000	35	41	$4\frac{1}{2}$	$4\frac{1}{2}$	29	34	$3\frac{3}{4}$	$3\frac{3}{4}$	24	30	$3\frac{1}{4}$	3
1750	33	38	4	4	27	32	$3\frac{1}{4}$	$3\frac{1}{4}$	23	28	$3\frac{1}{4}$	$2\frac{3}{4}$
1500	30	36	$3\frac{1}{2}$	$3\frac{1}{2}$	24	30	3	$2\frac{3}{4}$	21	26	$3\frac{1}{4}$	$2\frac{3}{4}$
1250	28	33	3	3	23	27	$2\frac{1}{4}$	$2\frac{1}{4}$	19	24	$3\frac{1}{4}$	$2\frac{3}{4}$
1000	24	30	$2\frac{1}{2}$	$2\frac{1}{4}$	20	25	$2\frac{1}{4}$	$2\frac{1}{4}$	19	22	3	$2\frac{1}{2}$
750	21	26	$2\frac{1}{2}$	2	19	22	$2\frac{1}{4}$	$2\frac{1}{4}$	19	22	$2\frac{1}{4}$	$2\frac{1}{4}$
500	19	22	$2\frac{1}{2}$	$1\frac{3}{4}$	19	22	$2\frac{1}{4}$	$1\frac{3}{4}$	19	22	$2\frac{1}{4}$	$1\frac{1}{2}$
W14X500												
4410	54	59	8	8	44	48	$7\frac{1}{2}$	$7\frac{1}{2}$	38	42	7	7
4250	53	58	$7\frac{3}{4}$	$7\frac{3}{4}$	43	48	$7\frac{1}{4}$	$7\frac{1}{4}$	37	42	$6\frac{1}{2}$	$6\frac{1}{2}$
4000	52	56	$7\frac{1}{2}$	$7\frac{1}{2}$	42	46	7	7	36	40	$6\frac{1}{4}$	$6\frac{1}{4}$
3750	50	54	$7\frac{1}{4}$	$7\frac{1}{4}$	40	45	$6\frac{1}{2}$	$6\frac{1}{2}$	35	39	6	6
3500	48	53	$6\frac{3}{4}$	$6\frac{3}{4}$	39	43	$6\frac{1}{4}$	$6\frac{1}{4}$	33	38	$5\frac{1}{2}$	$5\frac{1}{2}$
3250	46	51	$6\frac{1}{2}$	$6\frac{1}{2}$	37	42	$5\frac{3}{4}$	$5\frac{3}{4}$	32	37	$5\frac{1}{4}$	$5\frac{1}{4}$
3000	44	49	6	6	36	40	$5\frac{1}{2}$	$5\frac{1}{2}$	31	35	5	5
2750	42	47	$5\frac{3}{4}$	$5\frac{3}{4}$	34	39	5	5	29	34	$4\frac{1}{2}$	$4\frac{1}{2}$
2500	40	45	$5\frac{1}{4}$	$5\frac{1}{4}$	33	37	$4\frac{3}{4}$	$4\frac{3}{4}$	28	32	$4\frac{1}{4}$	$4\frac{1}{4}$
2250	38	43	5	5	31	35	$4\frac{1}{4}$	$4\frac{1}{4}$	26	31	$3\frac{1}{2}$	$3\frac{1}{2}$
2000	36	40	$4\frac{1}{2}$	$4\frac{1}{2}$	29	33	$3\frac{3}{4}$	$3\frac{3}{4}$	25	29	$3\frac{1}{4}$	$3\frac{1}{4}$
1750	33	38	4	4	27	31	$3\frac{1}{4}$	$3\frac{1}{4}$	23	28	$3\frac{1}{4}$	$2\frac{3}{4}$
1500	31	35	$3\frac{1}{2}$	$3\frac{1}{2}$	25	29	3	$2\frac{3}{4}$	21	26	$3\frac{1}{4}$	$2\frac{3}{4}$
1250	28	32	3	3	23	27	$2\frac{1}{4}$	$2\frac{1}{4}$	19	24	$3\frac{1}{4}$	$2\frac{3}{4}$
1000	25	29	$2\frac{1}{2}$	$2\frac{1}{4}$	20	24	3	$2\frac{1}{4}$	19	22	3	$2\frac{1}{2}$
750	21	26	$2\frac{1}{2}$	2	19	22	$2\frac{1}{4}$	$2\frac{1}{4}$	19	22	$2\frac{1}{4}$	$2\frac{1}{4}$
500	19	22	$2\frac{1}{2}$	$1\frac{3}{4}$	19	22	$2\frac{1}{4}$	$1\frac{3}{4}$	19	22	$2\frac{1}{4}$	$1\frac{1}{2}$
W14X455												
4020	52	56	$7\frac{3}{4}$	$7\frac{3}{4}$	42	46	7	7	36	40	$6\frac{1}{2}$	$6\frac{1}{2}$
4000	52	56	$7\frac{3}{4}$	$7\frac{3}{4}$	42	46	7	7	36	40	$6\frac{1}{2}$	$6\frac{1}{2}$
3750	50	54	$7\frac{1}{4}$	$7\frac{1}{4}$	40	45	$6\frac{1}{2}$	$6\frac{1}{2}$	35	39	6	6
3500	49	52	7	7	39	43	$6\frac{1}{4}$	$6\frac{1}{4}$	33	38	$5\frac{3}{4}$	$5\frac{3}{4}$
3250	46	51	$6\frac{1}{2}$	$6\frac{1}{2}$	37	42	6	6	33	36	$5\frac{1}{2}$	$5\frac{1}{2}$
3000	44	49	$6\frac{1}{4}$	$6\frac{1}{4}$	36	40	$5\frac{1}{2}$	$5\frac{1}{2}$	31	35	5	5

Note: Shaded values indicate that Ninth Edition design differs from Eighth Edition.

Column Base Plate Design Table (cont.)											$f'_c = 4.0 \text{ ksi}$	
For plates thicker than 8 in., $F_y$ of 32 ksi is used											Plate $F_y = 36 \text{ ksi}$	
Column Load (kips)	Bearing Area Factor (Allowable Bearing Stress)											
	1.0 ( $F_p = 1400 \text{ psi}$ )				1.5 ( $F_p = 2100 \text{ psi}$ )				2.0 ( $F_p = 2800 \text{ psi}$ )			
	B, in.	N, in.	$t_8$ , in.	$t_9$ , in.	B, in.	N, in.	$t_8$ , in.	$t_9$ , in.	B, in.	N, in.	$t_8$ , in.	$t_9$ , in.
2750	42	47	5 $\frac{3}{4}$	5 $\frac{3}{4}$	34	39	5 $\frac{1}{4}$	5 $\frac{1}{4}$	29	34	4 $\frac{1}{2}$	4 $\frac{1}{2}$
2500	40	45	5 $\frac{1}{2}$	5 $\frac{1}{2}$	33	37	4 $\frac{3}{4}$	4 $\frac{3}{4}$	28	32	4 $\frac{1}{4}$	4 $\frac{1}{4}$
2250	39	42	5	5	31	35	4 $\frac{1}{4}$	4 $\frac{1}{4}$	26	31	3 $\frac{3}{4}$	3 $\frac{3}{4}$
2000	36	40	4 $\frac{1}{2}$	4 $\frac{1}{2}$	29	33	3 $\frac{3}{4}$	3 $\frac{3}{4}$	25	29	3 $\frac{1}{4}$	3 $\frac{1}{4}$
1750	33	38	4	4	27	31	3 $\frac{1}{2}$	3 $\frac{1}{2}$	24	27	3 $\frac{1}{4}$	3
1500	31	35	3 $\frac{1}{2}$	3 $\frac{1}{2}$	25	29	3	3	21	26	3 $\frac{1}{4}$	2 $\frac{1}{2}$
1250	28	32	3	3	23	27	2 $\frac{3}{4}$	2 $\frac{1}{2}$	19	24	3 $\frac{1}{4}$	2 $\frac{1}{2}$
1000	25	29	2 $\frac{1}{2}$	2 $\frac{1}{2}$	20	24	3	2 $\frac{1}{4}$	19	21	3 $\frac{1}{4}$	2 $\frac{1}{2}$
750	21	26	2 $\frac{1}{2}$	1 $\frac{3}{4}$	19	21	2 $\frac{3}{4}$	2 $\frac{1}{4}$	19	21	2 $\frac{3}{4}$	2 $\frac{1}{4}$
500	19	21	2 $\frac{1}{4}$	1 $\frac{3}{4}$	19	21	2 $\frac{1}{4}$	1 $\frac{3}{4}$	19	21	2 $\frac{1}{4}$	1 $\frac{1}{2}$
<b>W14x426</b>												
3750	50	54	7 $\frac{1}{4}$	7 $\frac{1}{4}$	40	45	6 $\frac{3}{4}$	6 $\frac{3}{4}$	35	39	6	6
3500	49	52	7	7	39	43	6 $\frac{1}{4}$	6 $\frac{1}{4}$	33	38	5 $\frac{3}{4}$	5 $\frac{3}{4}$
3250	47	50	6 $\frac{3}{4}$	6 $\frac{3}{4}$	37	42	6	6	33	36	5 $\frac{1}{2}$	5 $\frac{1}{2}$
3000	44	49	6 $\frac{1}{4}$	6 $\frac{1}{4}$	36	40	5 $\frac{1}{2}$	5 $\frac{1}{2}$	31	35	5	5
2750	42	47	6	6	35	38	5 $\frac{1}{4}$	5 $\frac{1}{4}$	29	34	4 $\frac{3}{4}$	4 $\frac{3}{4}$
2500	40	45	5 $\frac{1}{2}$	5 $\frac{1}{2}$	33	37	4 $\frac{3}{4}$	4 $\frac{3}{4}$	28	32	4 $\frac{1}{4}$	4 $\frac{1}{4}$
2250	39	42	5 $\frac{1}{4}$	5 $\frac{1}{4}$	31	35	4 $\frac{1}{4}$	4 $\frac{1}{4}$	26	31	3 $\frac{3}{4}$	3 $\frac{3}{4}$
2000	36	40	4 $\frac{1}{2}$	4 $\frac{1}{2}$	29	33	4	4	25	29	3 $\frac{1}{4}$	3 $\frac{1}{4}$
1750	33	38	4	4	27	31	3 $\frac{1}{2}$	3 $\frac{1}{2}$	24	27	3 $\frac{1}{4}$	3
1500	31	35	3 $\frac{1}{2}$	3 $\frac{1}{2}$	25	29	3	3	22	25	3 $\frac{1}{4}$	2 $\frac{1}{2}$
1250	28	32	3	3	23	27	2 $\frac{3}{4}$	2 $\frac{1}{2}$	20	23	3 $\frac{1}{4}$	2 $\frac{1}{2}$
1000	25	29	2 $\frac{1}{2}$	2 $\frac{1}{2}$	20	24	3	2 $\frac{1}{4}$	19	21	3 $\frac{1}{4}$	2 $\frac{1}{2}$
750	22	25	2 $\frac{1}{4}$	1 $\frac{3}{4}$	19	21	2 $\frac{3}{4}$	2 $\frac{1}{4}$	19	21	2 $\frac{3}{4}$	2 $\frac{1}{4}$
500	19	21	2 $\frac{1}{4}$	1 $\frac{3}{4}$	19	21	2 $\frac{1}{4}$	1 $\frac{3}{4}$	19	21	2 $\frac{1}{4}$	1 $\frac{1}{2}$
375	19	21	2	1 $\frac{1}{2}$	19	21	2	1 $\frac{1}{4}$	19	21	2	1
<b>W14x398</b>												
3510	49	52	7	7	39	43	6 $\frac{1}{4}$	6 $\frac{1}{4}$	33	38	6	6
3500	49	52	7	7	39	43	6 $\frac{1}{4}$	6 $\frac{1}{4}$	34	37	6	6
3250	47	50	6 $\frac{3}{4}$	6 $\frac{3}{4}$	38	41	6	6	33	36	5 $\frac{1}{2}$	5 $\frac{1}{2}$
3000	45	48	6 $\frac{1}{4}$	6 $\frac{1}{4}$	36	40	5 $\frac{1}{2}$	5 $\frac{1}{2}$	31	35	5	5
2750	43	46	6	6	35	38	5 $\frac{1}{4}$	5 $\frac{1}{4}$	30	33	4 $\frac{3}{4}$	4 $\frac{3}{4}$
2500	41	44	5 $\frac{1}{2}$	5 $\frac{1}{2}$	33	37	4 $\frac{3}{4}$	4 $\frac{3}{4}$	28	32	4 $\frac{1}{4}$	4 $\frac{1}{4}$
2250	39	42	5 $\frac{1}{4}$	5 $\frac{1}{4}$	31	35	4 $\frac{1}{2}$	4 $\frac{1}{2}$	27	30	4	4
2000	36	40	4 $\frac{1}{2}$	4 $\frac{1}{2}$	29	33	4	4	25	29	3 $\frac{1}{4}$	3 $\frac{1}{4}$
1750	34	37	4 $\frac{1}{4}$	4 $\frac{1}{4}$	27	31	3 $\frac{1}{2}$	3 $\frac{1}{2}$	24	27	3 $\frac{1}{4}$	3
1500	31	35	3 $\frac{1}{2}$	3 $\frac{1}{2}$	25	29	3	3	22	25	3 $\frac{1}{4}$	2 $\frac{1}{2}$
1250	28	32	3	3	23	27	2 $\frac{3}{4}$	2 $\frac{1}{2}$	20	23	3 $\frac{1}{4}$	2 $\frac{1}{2}$
1000	25	29	2 $\frac{1}{2}$	2 $\frac{1}{2}$	20	24	3	2 $\frac{1}{4}$	19	21	3 $\frac{1}{4}$	2 $\frac{1}{2}$
750	22	25	2 $\frac{1}{4}$	1 $\frac{3}{4}$	19	21	2 $\frac{3}{4}$	2	19	20	2 $\frac{3}{4}$	2 $\frac{1}{4}$
500	19	21	2 $\frac{1}{4}$	1 $\frac{3}{4}$	19	20	2 $\frac{1}{4}$	1 $\frac{3}{4}$	19	20	2 $\frac{1}{4}$	1 $\frac{1}{2}$
375	19	20	2	1 $\frac{1}{2}$	19	20	2	1 $\frac{1}{4}$	19	20	2	1
<b>W14x370</b>												
3270	47	50	6 $\frac{3}{4}$	6 $\frac{3}{4}$	38	41	6	6	33	36	5 $\frac{1}{2}$	5 $\frac{1}{2}$
3250	47	50	6 $\frac{3}{4}$	6 $\frac{3}{4}$	38	41	6	6	33	36	5 $\frac{1}{2}$	5 $\frac{1}{2}$
3000	45	48	6 $\frac{1}{2}$	6 $\frac{1}{2}$	36	40	5 $\frac{3}{4}$	5 $\frac{3}{4}$	31	35	5	5
2750	43	46	6	6	35	38	5 $\frac{1}{4}$	5 $\frac{1}{4}$	30	33	4 $\frac{3}{4}$	4 $\frac{3}{4}$
2500	41	44	5 $\frac{1}{2}$	5 $\frac{1}{2}$	34	36	5	5	28	32	4 $\frac{1}{4}$	4 $\frac{1}{4}$
2250	39	42	5 $\frac{1}{4}$	5 $\frac{1}{4}$	31	35	4 $\frac{1}{2}$	4 $\frac{1}{2}$	27	30	4	4
2000	36	40	4 $\frac{9}{4}$	4 $\frac{9}{4}$	29	33	4	4	25	29	3 $\frac{1}{2}$	3 $\frac{1}{2}$
1750	34	37	4 $\frac{1}{4}$	4 $\frac{1}{4}$	27	31	3 $\frac{1}{2}$	3 $\frac{1}{2}$	24	27	3 $\frac{1}{4}$	3
1500	31	35	3 $\frac{3}{4}$	3 $\frac{3}{4}$	25	29	3	3	22	25	3 $\frac{1}{4}$	2 $\frac{1}{2}$

Note: Shaded values indicate that Ninth Edition design differs from Eighth Edition.

Column Base Plate Design Table (cont.)										$f_c' = 4.0 \text{ ksi}$				
For plates thicker than 8 in., $F_y$ of 32 ksi is used										Plate $F_y = 36 \text{ ksi}$				
Column Load (kips)	Bearing Area Factor (Allowable Bearing Stress)													
	1.0 ( $F_p = 1400 \text{ psi}$ )				1.5 ( $F_p = 2100 \text{ psi}$ )				2.0 ( $F_p = 2800 \text{ psi}$ )					
	B, in.	N, in.	$t_8$ , in.	$t_9$ , in.	B, in.	N, in.	$t_8$ , in.	$t_9$ , in.	B, in.	N, in.	$t_8$ , in.	$t_9$ , in.		
1250	28	32	3	3	23	26	3	2½	20	23	3¼	2½		
1000	25	29	2½	2½	20	24	3	2¼	18	21	3¼	2½		
750	22	25	2¼	1¾	18	21	2¾	2¼	18	20	3	2¼		
500	18	21	2¼	1¾	18	20	2½	1¾	18	20	2½	1½		
375	18	20	2	1½	18	20	2	1¼	18	20	2	1		
W14x342														
3030	46	48	6½	6½	37	40	5¾	5¾	31	35	5¼	5¼		
3000	45	48	6½	6½	36	40	5¾	5¾	31	35	5¼	5¼		
2750	43	46	6	6	35	38	5½	5½	30	33	4¾	4¾		
2500	41	44	5½	5½	34	36	5	5	28	32	4½	4½		
2250	39	42	5¼	5¼	31	35	4½	4½	27	30	4	4		
2000	36	40	4¾	4¾	29	33	4	4	25	29	3½	3½		
1750	34	37	4¼	4¼	27	31	3½	3½	24	27	3¼	3		
1500	31	35	3¾	3¾	25	29	3	3	22	25	3¼	2½		
1250	28	32	3¼	3¼	23	26	3	2½	20	23	3¼	2½		
1000	25	29	2½	2½	20	24	3	2¼	18	21	3¼	2½		
750	22	25	2¼	1¾	18	21	2¾	2	18	20	3	2¼		
500	18	21	2¼	1¾	18	20	2½	1¾	18	20	2½	1½		
375	18	20	2	1½	18	20	2	1¼	18	20	2	1		
W14x311														
2742	43	46	6	6	35	38	5½	5½	30	33	4¾	4¾		
2500	41	44	5½	5½	34	36	5¼	5¼	28	32	4½	4½		
2250	39	42	5¼	5¼	32	34	4¾	4¾	27	30	4	4		
2000	37	39	4¾	4¾	29	33	4½	4½	26	28	3¾	3¾		
1750	34	37	4¼	4¼	27	31	3¾	3¾	24	27	3¼	3¼		
1500	32	34	3¾	3¾	26	28	3¼	3¼	22	25	3¼	2½		
1250	28	32	3¼	3¼	23	26	3	2½	20	23	3¼	2½		
1000	26	28	2¾	2¾	20	24	3	2¼	18	21	3¼	2½		
750	22	25	2¼	2	18	21	2¾	2	18	19	3	2¼		
500	18	21	2¼	1¾	18	19	2½	1¾	18	19	2½	1½		
375	18	19	2¼	1½	18	19	2¼	1¼	18	19	2¼	1¼		
W14x283														
2499	41	44	5¾	5¾	34	36	5¼	5¼	29	31	4½	4½		
2250	39	42	5¼	5¼	32	34	4¾	4¾	27	30	4	4		
2000	37	39	4¾	4¾	30	32	4½	4½	26	28	3¾	3¾		
1750	34	37	4¼	4¼	28	30	3¾	3¾	24	27	3¼	3¼		
1500	32	34	3¾	3¾	26	28	3¼	3¼	22	25	3¼	2¾		
1250	29	31	3¼	3¼	23	26	3	2½	20	23	3¼	2½		
1000	26	28	2¾	2¾	21	23	3	2	18	20	3¼	2½		
750	22	25	2¼	2	18	20	3	2	18	19	3	2¼		
500	18	20	2½	1¾	18	19	2½	1¾	18	19	2½	1½		
375	18	19	2¼	1½	18	19	2¼	1¼	18	19	2¼	1¼		
250	18	19	1¾	1	18	19	1¾	1	18	19	1¾	1		
W14x257														
2268	39	42	5¼	5¼	32	34	4¾	4¾	27	30	4½	4½		
2250	40	41	5½	5½	32	34	4¾	4¾	27	30	4½	4½		
2000	37	39	4¾	4¾	30	32	4½	4½	26	28	3¾	3¾		
1750	34	37	4¼	4¼	28	30	3¾	3¾	25	26	3½	3½		
1500	32	34	4	4	26	28	3¼	3¼	22	25	3¼	2¾		
1250	29	31	3¼	3¼	23	26	3	2¾	20	23	3¼	2½		
1000	26	28	2¾	2¾	21	23	3	2	18	20	3¼	2½		
750	22	25	2¼	2	18	20	3	2	18	18	3	2¼		

Note: Shaded values indicate that Ninth Edition design differs from Eighth Edition.

Column Base Plate Design Table (cont.)											$f'_c = 4.0 \text{ ksi}$	
For plates thicker than 8 in., $F_y$ of 32 ksi is used											Plate $F_y = 36 \text{ ksi}$	
Column Load (kips)	Bearing Area Factor (Allowable Bearing Stress)											
	1.0 ( $F_p = 1400 \text{ psi}$ )				1.5 ( $F_p = 2100 \text{ psi}$ )				2.0 ( $F_p = 2800 \text{ psi}$ )			
	$B$ , in.	$N$ , in.	$t_B$ , in.	$t_g$ , in.	$B$ , in.	$N$ , in.	$t_B$ , in.	$t_g$ , in.	$B$ , in.	$N$ , in.	$t_B$ , in.	$t_g$ , in.
500	18	20	2½	1¼	18	18	2½	1¼	18	18	2½	1½
375	18	18	2¼	1½	18	18	2¼	1½	18	18	2¼	1¼
250	18	18	1¾	1¼	18	18	1¾	1	18	18	1¾	1
<b>W14x233</b>												
2055	37	40	5	5	30	33	4½	4½	27	28	4	4
2000	37	39	5	5	30	32	4¼	4¼	26	28	3¾	3¾
1750	34	37	4½	4½	28	30	3¾	3¾	25	26	3½	3½
1500	32	34	4	4	26	28	3¼	3¼	23	24	3¼	3
1250	29	31	3¼	3¼	23	26	3	2¾	21	22	3¼	2½
1000	26	28	2¾	2¾	21	23	3	2	18	20	3¼	2¼
750	23	24	2¼	2	18	20	3	2	18	18	3	2¼
500	18	20	2½	1¾	18	18	2½	1¾	18	18	2½	1½
375	18	18	2¼	1½	18	18	2¼	1½	18	18	2¼	1¼
250	18	18	1¾	1¼	18	18	1¾	1	18	18	1¾	1
<b>W14x211</b>												
1860	35	38	4¾	4¾	29	31	4	4	25	27	3½	3½
1750	34	37	4½	4½	28	30	3¾	3¾	25	26	3½	3½
1500	32	34	4	4	26	28	3¼	3¼	23	24	3¼	3
1250	29	31	3¼	3¼	23	26	3	2¾	21	22	3¼	2½
1000	26	28	2¾	2¾	21	23	3	2¼	18	20	3¼	2¼
750	23	24	2¼	2¼	18	20	3	2	18	18	3	2
500	18	20	2½	1¾	18	18	2½	1¾	18	18	2½	1½
375	18	18	2¼	1½	18	18	2¼	1½	18	18	2¼	1¼
250	18	18	1¾	1¼	18	18	1¾	1	18	18	1¾	1
200	18	18	1¾	1	18	18	1¾	1	18	18	1¾	1
<b>W14x193</b>												
1704	34	36	4¼	4¼	28	30	3¾	3¾	24	26	3¼	3¼
1500	32	34	4	4	26	28	3¼	3¼	23	24	3¼	3
1250	29	31	3¼	3¼	24	25	3	3	21	22	3¼	2½
1000	26	28	2¾	2¾	21	23	3	2¼	18	20	3¼	2¼
750	23	24	2¼	2¼	18	20	3	2	18	17	3¼	2¼
500	18	20	2½	1¾	18	17	2½	1¾	18	17	2½	1¾
375	18	17	2¼	1½	18	17	2¼	1½	18	17	2¼	1¼
250	18	17	1¾	1¼	18	17	1¾	1	18	17	1¾	1
200	18	17	1¾	1	18	17	1¾	1	18	17	1¾	1
<b>W14x176</b>												
1554	33	34	4¼	4¼	27	28	3½	3½	23	25	3¼	3
1500	32	34	4	4	26	28	3¼	3¼	23	24	3¼	3
1250	29	31	3½	3½	24	25	3	3	21	22	3¼	2½
1000	26	28	2¾	2¾	21	23	3	2¼	18	20	3¼	2¼
750	23	24	2¼	2¼	18	20	3	2	18	17	3¼	2¼
500	18	20	2½	1¾	18	17	2½	1¾	18	17	2½	1¾
375	18	17	2¼	1½	18	17	2¼	1½	18	17	2¼	1¼
250	18	17	1¾	1¼	18	17	1¾	1	18	17	1¾	1
200	18	17	1¾	1	18	17	1¾	1	18	17	1¾	1

Note: Shaded values indicate that Ninth Edition design differs from Eighth Edition.

Column Base Plate Design Table (cont.)											$f_c' = 4.0 \text{ ksi}$	
For plates thicker than 8 in., $F_y$ of 32 ksi is used											Plate $F_y = 36 \text{ ksi}$	
Column Load (kips)	Bearing Area Factor (Allowable Bearing Stress)											
	1.0 ( $F_p = 1400 \text{ psi}$ )				1.5 ( $F_p = 2100 \text{ psi}$ )				2.0 ( $F_p = 2800 \text{ psi}$ )			
	$B$ , in.	$N$ , in.	$t_8$ , in.	$t_9$ , in.	$B$ , in.	$N$ , in.	$t_8$ , in.	$t_9$ , in.	$B$ , in.	$N$ , in.	$t_8$ , in.	$t_9$ , in.
<b>W14x159</b>												
1401	31	33	3 $\frac{3}{4}$	3 $\frac{3}{4}$	25	27	3 $\frac{1}{4}$	3 $\frac{1}{4}$	22	23	3 $\frac{1}{4}$	2 $\frac{3}{4}$
1250	29	31	3 $\frac{1}{2}$	3 $\frac{1}{2}$	24	25	3	3	21	22	3 $\frac{1}{4}$	2 $\frac{1}{2}$
1000	26	28	2 $\frac{3}{4}$	2 $\frac{3}{4}$	21	23	3	2 $\frac{1}{4}$	18	20	3 $\frac{1}{4}$	2 $\frac{1}{4}$
750	23	24	2 $\frac{1}{4}$	2 $\frac{1}{4}$	18	20	3	2	18	17	3 $\frac{1}{4}$	2
500	18	20	2 $\frac{1}{2}$	1 $\frac{1}{2}$	18	17	2 $\frac{1}{2}$	1 $\frac{3}{4}$	18	17	2 $\frac{1}{2}$	1 $\frac{3}{4}$
375	18	17	2 $\frac{1}{4}$	1 $\frac{1}{2}$	18	17	2 $\frac{1}{4}$	1 $\frac{1}{2}$	18	17	2 $\frac{1}{4}$	1 $\frac{1}{4}$
250	18	17	1 $\frac{3}{4}$	1 $\frac{1}{4}$	18	17	1 $\frac{3}{4}$	1	18	17	1 $\frac{3}{4}$	1
200	18	17	1 $\frac{3}{4}$	1	18	17	1 $\frac{3}{4}$	1	18	17	1 $\frac{3}{4}$	1
150	18	17	1 $\frac{1}{2}$	1	18	17	1 $\frac{1}{2}$	1	18	17	1 $\frac{1}{2}$	1
<b>W14x145</b>												
1281	30	31	3 $\frac{1}{2}$	3 $\frac{1}{2}$	24	26	3	3	21	22	3 $\frac{1}{4}$	2 $\frac{1}{2}$
1250	29	31	3 $\frac{1}{2}$	3 $\frac{1}{2}$	24	25	3	3	21	22	3 $\frac{1}{4}$	2 $\frac{1}{2}$
1000	26	28	2 $\frac{3}{4}$	2 $\frac{3}{4}$	21	23	3	2 $\frac{1}{4}$	18	20	3 $\frac{1}{4}$	2 $\frac{1}{4}$
750	23	24	2 $\frac{1}{4}$	2 $\frac{1}{4}$	18	20	3	2	17	17	3 $\frac{1}{4}$	2 $\frac{1}{4}$
500	18	20	2 $\frac{1}{2}$	1 $\frac{1}{2}$	17	17	2 $\frac{3}{4}$	1 $\frac{3}{4}$	17	17	2 $\frac{3}{4}$	1 $\frac{3}{4}$
375	17	17	2 $\frac{1}{4}$	1 $\frac{1}{2}$	17	17	2 $\frac{1}{4}$	1 $\frac{1}{2}$	17	17	2 $\frac{1}{4}$	1 $\frac{1}{4}$
250	17	17	2	1 $\frac{1}{4}$	17	17	2	1	17	17	2	1
200	17	17	1 $\frac{3}{4}$	1	17	17	1 $\frac{3}{4}$	1	17	17	1 $\frac{3}{4}$	1
150	17	17	1 $\frac{1}{2}$	1	17	17	1 $\frac{1}{2}$	1	17	17	1 $\frac{1}{2}$	1
<b>W14x132</b>												
1164	28	30	3 $\frac{1}{4}$	3 $\frac{1}{4}$	23	25	2 $\frac{3}{4}$	2 $\frac{3}{4}$	20	21	3 $\frac{1}{4}$	2 $\frac{1}{2}$
1000	26	28	3	3	21	23	2 $\frac{3}{4}$	2 $\frac{1}{4}$	18	20	3 $\frac{1}{4}$	2 $\frac{1}{4}$
750	23	24	2 $\frac{1}{4}$	2 $\frac{1}{4}$	18	20	2 $\frac{3}{4}$	2	17	17	3 $\frac{1}{4}$	2
500	18	20	2 $\frac{1}{4}$	1 $\frac{1}{2}$	17	17	2 $\frac{1}{2}$	1 $\frac{3}{4}$	17	17	2 $\frac{1}{2}$	1 $\frac{3}{4}$
375	17	17	2 $\frac{1}{4}$	1 $\frac{1}{2}$	17	17	2 $\frac{1}{4}$	1 $\frac{1}{2}$	17	17	2 $\frac{1}{4}$	1 $\frac{1}{4}$
250	17	17	1 $\frac{3}{4}$	1 $\frac{1}{4}$	17	17	1 $\frac{3}{4}$	1	17	17	1 $\frac{3}{4}$	1
200	17	17	1 $\frac{3}{4}$	1	17	17	1 $\frac{3}{4}$	1	17	17	1 $\frac{3}{4}$	1
150	17	17	1 $\frac{1}{2}$	1	17	17	1 $\frac{1}{2}$	1	17	17	1 $\frac{1}{2}$	1
125	17	17	1 $\frac{1}{4}$	1	17	17	1 $\frac{1}{4}$	1	17	17	1 $\frac{1}{4}$	1
<b>W14x120</b>												
1059	27	29	3	3	22	23	2 $\frac{3}{4}$	2 $\frac{1}{2}$	19	20	3 $\frac{1}{4}$	2 $\frac{1}{4}$
1000	26	28	3	3	21	23	2 $\frac{3}{4}$	2 $\frac{1}{4}$	18	20	3 $\frac{1}{4}$	2 $\frac{1}{4}$
750	23	24	2 $\frac{1}{4}$	2 $\frac{1}{4}$	18	20	2 $\frac{3}{4}$	2	17	17	3 $\frac{1}{4}$	2
500	18	20	2 $\frac{1}{4}$	1 $\frac{1}{2}$	17	16	2 $\frac{3}{4}$	1 $\frac{3}{4}$	17	16	2 $\frac{3}{4}$	1 $\frac{3}{4}$
375	17	17	2 $\frac{1}{4}$	1 $\frac{1}{2}$	17	16	2 $\frac{1}{4}$	1 $\frac{1}{2}$	17	16	2 $\frac{1}{4}$	1 $\frac{1}{4}$
250	17	16	2	1 $\frac{1}{4}$	17	16	2	1	17	16	2	1
200	17	16	1 $\frac{3}{4}$	1	17	16	1 $\frac{3}{4}$	1	17	16	1 $\frac{3}{4}$	1
150	17	16	1 $\frac{1}{2}$	1	17	16	1 $\frac{1}{2}$	1	17	16	1 $\frac{1}{2}$	1
125	17	16	1 $\frac{1}{2}$	1	17	16	1 $\frac{1}{2}$	1	17	16	1 $\frac{1}{2}$	1
<b>W14x109</b>												
960	26	27	3	3	21	22	2 $\frac{3}{4}$	2 $\frac{1}{4}$	18	20	3 $\frac{1}{4}$	2
750	23	24	2 $\frac{1}{4}$	2 $\frac{1}{4}$	18	20	2 $\frac{3}{4}$	1 $\frac{3}{4}$	17	17	3 $\frac{1}{4}$	2
500	18	20	2 $\frac{1}{4}$	1 $\frac{1}{2}$	17	16	2 $\frac{3}{4}$	1 $\frac{3}{4}$	17	16	2 $\frac{3}{4}$	1 $\frac{3}{4}$
375	17	17	2 $\frac{1}{4}$	1 $\frac{1}{2}$	17	16	2 $\frac{1}{4}$	1 $\frac{1}{2}$	17	16	2 $\frac{1}{4}$	1 $\frac{1}{4}$
250	17	16	2	1 $\frac{1}{4}$	17	16	2	1	17	16	2	1
200	17	16	1 $\frac{3}{4}$	1	17	16	1 $\frac{3}{4}$	1	17	16	1 $\frac{3}{4}$	1
150	17	16	1 $\frac{1}{2}$	1	17	16	1 $\frac{1}{2}$	1	17	16	1 $\frac{1}{2}$	1
125	17	16	1 $\frac{1}{2}$	1	17	16	1 $\frac{1}{2}$	1	17	16	1 $\frac{1}{2}$	1
100	17	16	1 $\frac{1}{4}$	1	17	16	1 $\frac{1}{4}$	1	17	16	1 $\frac{1}{4}$	1

Note: Shaded values indicate that Ninth Edition design differs from Eighth Edition.

Column Base Plate Design Table (cont.)											$f'_c = 4.0 \text{ ksi}$	
For plates thicker than 8 in., $F_y$ of 32 ksi is used											Plate $F_y = 36 \text{ ksi}$	
Column Load (kips)	Bearing Area Factor (Allowable Bearing Stress)											
	1.0 ( $F_p = 1400 \text{ psi}$ )				1.5 ( $F_p = 2100 \text{ psi}$ )				2.0 ( $F_p = 2800 \text{ psi}$ )			
	B, in.	N, in.	$t_8$ , in.	$t_9$ , in.	B, in.	N, in.	$t_8$ , in.	$t_9$ , in.	B, in.	N, in.	$t_8$ , in.	$t_9$ , in.
<b>W14x99</b>												
873	24	26	2½	2½	20	21	2¾	2¼	17	19	3¼	2
750	23	24	2¼	2¼	18	20	2¾	1¾	17	17	3¼	2
500	18	20	2¼	1½	17	16	2¾	1¾	17	16	2¾	1¾
375	17	17	2¼	1½	17	16	2¼	1½	17	16	2¼	1¼
250	17	16	2	1¼	17	16	2	1	17	16	2	1
200	17	16	1¾	1	17	16	1¾	1	17	16	1¾	1
150	17	16	1½	1	17	16	1½	1	17	16	1½	1
125	17	16	1½	1	17	16	1½	1	17	16	1½	1
100	17	16	1¼	1	17	16	1¼	1	17	16	1¼	1
<b>W14x90</b>												
795	23	25	2½	2½	19	20	2¾	2	17	18	3¼	2
750	23	24	2¼	2¼	18	20	2¾	1¾	17	17	3¼	2
500	18	20	2¼	1½	17	16	2¾	1¾	17	16	2¾	1¾
375	17	17	2¼	1½	17	16	2¼	1½	17	16	2¼	1¼
250	17	16	2	1¼	17	16	2	1	17	16	2	1
200	17	16	1¾	1	17	16	1¾	1	17	16	1¾	1
150	17	16	1½	1	17	16	1½	1	17	16	1½	1
125	17	16	1½	1	17	16	1½	1	17	16	1½	1
100	17	16	1¼	1	17	16	1¼	1	17	16	1¼	1
<b>W14x82</b>												
723	20	26	2½	2½	16	22	2¼	2¼	14	19	2½	1¾
500	17	22	1¾	1¾	14	18	2¼	1½	12	16	2½	1¾
375	15	19	1¾	1½	12	16	2¼	1½	12	16	2¼	1½
250	12	16	1¾	1¼	12	16	1¾	1¼	12	16	1¾	1
200	12	16	1¾	1¼	12	16	1¾	1	12	16	1¾	1
150	12	16	1½	1	12	16	1½	1	12	16	1½	1
125	12	16	1¼	1	12	16	1¼	1	12	16	1¼	1
100	12	16	1¼	1	12	16	1¼	1	12	16	1¼	1
75	12	16	1	1	12	16	1	1	12	16	1	1
<b>W14x74</b>												
654	20	24	2½	2½	15	21	2¼	2	13	18	2½	1¾
500	17	22	1¾	1¾	14	18	2¼	1½	12	16	2½	1¾
375	15	19	1¾	1½	12	16	2¼	1½	12	16	2¼	1½
250	12	16	1¾	1¼	12	16	1¾	1¼	12	16	1¾	1
200	12	16	1¾	1¼	12	16	1¾	1	12	16	1¾	1
150	12	16	1½	1	12	16	1½	1	12	16	1½	1
125	12	16	1¼	1	12	16	1¼	1	12	16	1¼	1
100	12	16	1¼	1	12	16	1¼	1	12	16	1¼	1
75	12	16	1	1	12	16	1	1	12	16	1	1
<b>W14x68</b>												
600	18	24	2¼	2¼	15	20	2¼	1¾	12	18	2½	1¾
500	17	22	1¾	1¾	14	18	2¼	1½	12	16	2½	1¾
375	15	19	1¾	1½	12	16	2¼	1½	12	16	2¼	1½
250	12	16	1¾	1¼	12	16	1¾	1¼	12	16	1¾	1
200	12	16	1¾	1¼	12	16	1¾	1	12	16	1¾	1
150	12	16	1½	1	12	16	1½	1	12	16	1½	1
125	12	16	1¼	1	12	16	1¼	1	12	16	1¼	1
100	12	16	1¼	1	12	16	1¼	1	12	16	1¼	1
75	12	16	1	1	12	16	1	1	12	16	1	1

Note: Shaded values indicate that Ninth Edition design differs from Eighth Edition.

Column Base Plate Design Table (cont.)											$f_c' = 4.0 \text{ ksi}$	
For plates thicker than 8 in., $F_y$ of 32 ksi is used											Plate $F_y = 36 \text{ ksi}$	
Column Load (kips)	Bearing Area Factor (Allowable Bearing Stress)											
	1.0 ( $F_p = 1400 \text{ psi}$ )				1.5 ( $F_p = 2100 \text{ psi}$ )				2.0 ( $F_p = 2800 \text{ psi}$ )			
	$B$ , in.	$N$ , in.	$t_8$ , in.	$t_9$ , in.	$B$ , in.	$N$ , in.	$t_8$ , in.	$t_9$ , in.	$B$ , in.	$N$ , in.	$t_8$ , in.	$t_9$ , in.
<b>W14x61</b>												
537	18	22	2	2	14	19	2½	1½	12	17	2½	1¾
500	17	22	1¾	1¾	14	18	2¼	1½	12	16	2½	1¾
375	15	19	1¾	1½	12	16	2¼	1½	12	16	2¼	1½
250	12	16	1¾	1¼	12	16	1¾	1¼	12	16	1¾	1
200	12	16	1¾	1¼	12	16	1¾	1	12	16	1¾	1
150	12	16	1½	1	12	16	1½	1	12	16	1½	1
125	12	16	1¼	1	12	16	1¼	1	12	16	1¼	1
100	12	16	1¼	1	12	16	1¼	1	12	16	1¼	1
75	12	16	1	1	12	16	1	1	12	16	1	1
<b>W14x53</b>												
468	16	22	2	2	12	19	2	1½	10	17	2¼	1½
375	14	20	1½	1½	11	17	1¾	1¼	10	16	2	1½
250	11	17	1½	1¼	10	16	1¾	1¼	10	16	1¾	1
200	10	16	1½	1	10	16	1½	1	10	16	1½	1
150	10	16	1¼	1	10	16	1¼	1	10	16	1¼	1
125	10	16	1¼	1	10	16	1¼	1	10	16	1¼	1
100	10	16	1	1	10	16	1	1	10	16	1	1
75	10	16	1	1	10	16	1	1	10	16	1	1
<b>W14x48</b>												
423	15	21	1¾	1¾	12	18	1¾	1½	10	16	2	1½
375	14	20	1½	1½	11	17	1¾	1¼	10	16	2	1½
250	11	17	1½	1¼	10	16	1¾	1¼	10	16	1¾	1
200	10	16	1½	1	10	16	1½	1	10	16	1½	1
150	10	16	1¼	1	10	16	1¼	1	10	16	1¼	1
125	10	16	1¼	1	10	16	1¼	1	10	16	1¼	1
100	10	16	1	1	10	16	1	1	10	16	1	1
75	10	16	1	1	10	16	1	1	10	16	1	1
<b>W14x43</b>												
378	14	20	1½	1½	11	17	1¾	1¼	10	16	2	1½
375	14	20	1½	1½	11	17	1¾	1¼	10	16	2	1½
250	11	17	1½	1¼	10	16	1¾	1¼	10	16	1¾	1
200	10	16	1½	1	10	16	1½	1	10	16	1½	1
150	10	16	1¼	1	10	16	1¼	1	10	16	1¼	1
125	10	16	1¼	1	10	16	1¼	1	10	16	1¼	1
100	10	16	1	1	10	16	1	1	10	16	1	1
75	10	16	1	1	10	16	1	1	10	16	1	1
<b>W14x38</b>												
336	12	20	1½	1½	10	17	1½	1¼	9	16	1¾	1¼
250	10	18	1¼	1	9	16	1½	1¼	9	16	1½	1
200	9	17	1¼	1	9	16	1¼	1	9	16	1¼	1
150	9	16	1¼	1	9	16	1¼	1	9	16	1¼	1
125	9	16	1	1	9	16	1	1	9	16	1	1
100	9	16	1	1	9	16	1	1	9	16	1	1
75	9	16	1	1	9	16	1	1	9	16	1	1
<b>W14x34</b>												
300	12	19	1½	1½	9	17	1½	1¼	9	16	1¾	1¼
250	10	18	1¼	1	9	16	1½	1¼	9	16	1½	1
200	9	17	1¼	1	9	16	1¼	1	9	16	1¼	1
150	9	16	1¼	1	9	16	1¼	1	9	16	1¼	1
125	9	16	1	1	9	16	1	1	9	16	1	1
100	9	16	1	1	9	16	1	1	9	16	1	1

Note: Shaded values indicate that Ninth Edition design differs from Eighth Edition.