

# Tables for Equal Single Angles in Compression

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The design of single angles in compression is a time consuming, iterative procedure. A computer program was developed to perform these time consuming calculations and generate tables for grades 36 ksi and 50 ksi equal leg angles. The program uses the recently published allowable stresses given in Reference 1.

The tables are generated using the following criteria:

1. The angle is pinned at the support points. ( $K = 1.0$ )
2. The common loading case where the axial load is applied on one side by a gusset plate. (See Fig. 1.)
3. No axial load is given when  $L/r$  exceeds 200.

The following example will illustrate the procedure used by the program:

Given:

Determine the maximum axial load that can be applied as shown in Fig. 1 for an L4×4×¼ grade 36 ksi with an unbraced length of 5 ft 0 in.

Angle Properties:

- $A = 1.94 \text{ in.}^2$
- $I_x = 3.04 \text{ in.}^4$
- $Y = 1.09 \text{ in.}$
- $r_z = .795 \text{ in.}$
- $J = .0438 \text{ in.}^4$
- $r_o = 2.23 \text{ in.}$
- $H = .627$
- $F_y = 36 \text{ ksi}$
- $E = 29,000 \text{ ksi}$
- $G = 11,200 \text{ ksi}$
- $t_g = \frac{3}{8} \text{ in.}$

Solution:

Determine  $Q$ .

$$\frac{b}{t} = \frac{4}{\frac{1}{4}} = 16 \quad \frac{76}{\sqrt{F_y}} = \frac{76}{\sqrt{36}} = 12.7 \quad \frac{155}{\sqrt{F_y}} = \frac{155}{\sqrt{36}} = 25.8$$

since  $12.7 < 16 < 25.8$ , use  $Q = 1.340 - .00447 \left(\frac{b}{t}\right) \sqrt{F_y}$

$$Q = 1.340 - .00447(16)\sqrt{36} = .911$$

Determine angle properties with respect to the W and Z axes.

$$I_z = Ar_z^2 = 1.94(.795)^2 = 1.23 \text{ in.}^4$$

$$I_w = I_x + I_y - I_z = 2(3.04) - 1.23 = 4.85 \text{ in.}^4$$

$$r_w = \sqrt{\frac{I_w}{A}} = \sqrt{\frac{4.85}{1.94}} = 1.58 \text{ in.}$$

$$E_w = \frac{.7071}{2} (L_g + t_g) = \frac{.7071}{2} (4 + .375) = 1.55 \text{ in.}$$

$$E_z = y\sqrt{2} - \frac{.7071}{2} (L_g - t_g)$$

$$= 1.09\sqrt{2} - \frac{.7071}{2} (4 - .375) = .260 \text{ in.}$$

$$C_w = .7071(L_g) = .7071(4) = 2.83 \text{ in.}$$

$$C_z = y\sqrt{2} = 1.09\sqrt{2} = 1.54 \text{ in.}$$

$$S_w = \frac{I_w}{C_w} = \frac{4.85}{2.83} = 1.71 \text{ in.}^3$$

$$S_z = \frac{I_z}{C_z} = \frac{1.23}{1.54} = .799 \text{ in.}^3$$

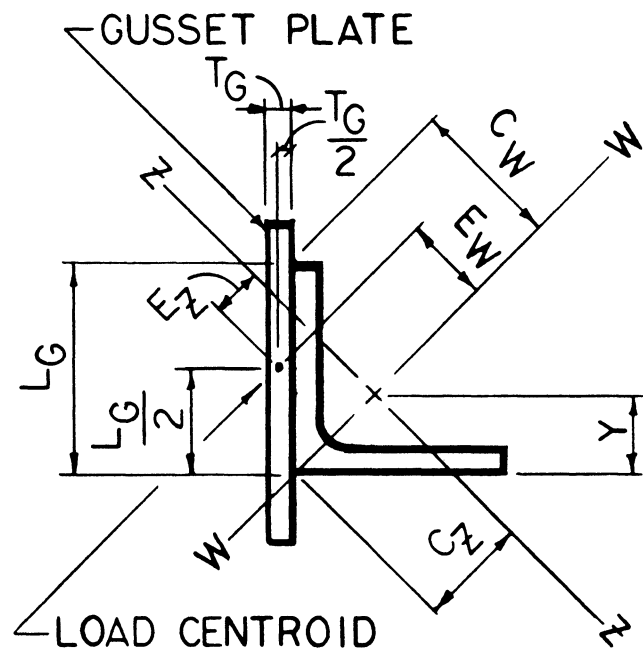


Fig. 1. Angle plan view.

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Determine the Equivalent  $L/r$  for flexural-torsional buckling.

$$F_{ej} = \frac{GJ}{Ar_o^2} = \frac{11,200(.0438)}{1.94(2.23)^2} = 50.8 \text{ ksi}$$

$$F_{ew} = \frac{\pi^2 E}{\left(\frac{L}{r_w}\right)^2} = \frac{\pi^2(29,000)}{\left(\frac{5(12)}{1.58}\right)^2} = 198.5 \text{ ksi}$$

$$F_e = \frac{F_{ew} + F_{ej}}{2H} \left(1 - \sqrt{1 - \frac{4(F_{ew})(F_{ej})H}{(F_{ew} + F_{ej})^2}}\right)$$

$$F_e = \frac{198.5 + 50.8}{2(.627)} \left(1 - \sqrt{1 - \frac{4(198.5)(50.8)(.627)}{(198.5 + 50.8)^2}}\right) = 45.7 \text{ ksi}$$

$$\left(\frac{L}{r}\right)_{equiv} = \pi \sqrt{\frac{E}{F_e}} = \pi \sqrt{\frac{29,000}{45.7}} = 79.1$$

$$\frac{L}{r_z} = \frac{5(12)}{.795} = 75.5$$

since  $79.1 > 75.5$ , flexural-torsional buckling controls.

Determine  $F_a$ .

$$C'_c = \sqrt{\frac{2\pi^2 E}{QF_y}} = \sqrt{\frac{2\pi^2(29,000)}{.911(36)}} = 132.1$$

$$\frac{L/r}{C'_c} = \frac{79.1}{132.1} = .60 \text{ using Ref. 1 Table 3 } C_a = .440$$

$$F_a = C_a QF_y = .440(.911)36 = 14.4 \text{ ksi}$$

Determine  $F_{bw}$ .

$$F_{ob} = \frac{28,250}{\frac{L}{t}} = \frac{28,250}{\frac{5(12)}{.25}} = 117.7 \text{ ksi}$$

since  $117.7 \text{ ksi} > 36 \text{ ksi}$ , use  $F_{bw} = (0.95 - .50\sqrt{\frac{F_y}{F_{ob}}})F_y \leq .66 F_y$

$$F_{bw} = (0.95 - .50\sqrt{\frac{36}{117.7}})36 = 24.2 \text{ ksi}$$

$$.66(36) = 23.8 \text{ ksi}$$

Check  $b/t$  provisions.

since  $b/t > \frac{76}{\sqrt{F_y}}$ , use  $F_{bw} = .60QF_y$

$$F_{bw} = .60(.911)36 = 19.7 \text{ ksi} \leftarrow \text{governs}$$

Determine  $F_{bz}$ .

since  $b/t > \frac{76}{\sqrt{F_y}}$  use  $F_{bz} = .60QF_y = 19.7 \text{ ksi}$

Solve for the maximum allowable axial load using:

$$\frac{P}{AF_a} + \frac{PE_w}{\left(1 - \frac{P}{AF'_{ew}}\right)S_w F_{bw}} + \frac{PE_z}{\left(1 - \frac{P}{AF'_{ez}}\right)S_z F_{bz}} \leq 1.0$$

$F'_{ew} = 103.4 \text{ ksi}$   $F'_{ez} = 26.2 \text{ ksi}$  using Ref. 1 Table 8

$$\frac{P}{1.94(14.4)} + \frac{P(1.55)}{\left(1 - \frac{P}{1.94(103.4)}\right)1.71(19.7)} + \frac{P(.260)}{\left(1 - \frac{P}{1.94(26.2)}\right).799(19.7)} \leq 1.0$$

$P = 9.6 \text{ kips}$

## REFERENCES

1. American Institute of Steel Construction, *Manual of Steel Construction*, 9th ed., (Chicago: AISC, 1989).

Allowable Axial Load in Kips														
L8.0x8.0														
KL (ft)	Grade 36.0 ksi							Grade 50.0 ksi						
	1 1/8	1	7/8	3/4	5/8	9/16	1/2	1 1/8	1	7/8	3/4	5/8	9/16	1/2
1	99.9	92.0	83.7	73.8	59.2	51.7	43.9	137.7	126.6	114.8	94.7	75.8	65.3	54.4
2	99.6	91.8	83.4	73.6	59.0	51.6	43.8	137.3	126.1	114.4	94.4	75.6	65.2	54.3
3	99.2	91.3	83.1	73.2	58.9	51.4	43.6	136.4	125.3	113.7	93.8	75.2	64.9	54.1
4	98.5	90.7	82.6	72.8	58.5	51.2	43.5	135.0	124.2	112.7	93.2	74.6	64.5	53.8
5	97.3	89.9	81.9	72.3	58.1	50.9	43.2	132.9	122.7	111.5	92.2	74.0	63.9	53.4
6	95.4	88.3	81.1	71.6	57.6	50.4	42.8	129.5	119.8	109.8	91.0	73.2	63.3	52.9
7	93.4	86.4	79.2	70.7	57.0	49.9	42.5	125.6	116.2	106.6	89.6	72.1	62.5	52.3
8	91.0	84.3	77.3	69.0	56.2	49.4	42.1	121.4	112.2	102.9	86.8	71.0	61.6	51.6
9	88.5	81.9	75.1	67.1	55.2	48.7	41.6	116.7	108.0	99.1	83.6	69.2	60.5	50.9
10	85.8	79.3	72.8	65.0	53.6	47.7	41.0	111.8	103.3	94.8	80.3	66.5	59.0	50.0
11	82.9	76.6	70.3	62.8	51.8	46.3	40.2	106.6	98.4	90.2	76.5	63.7	56.6	48.8
12	79.8	73.7	67.6	60.5	49.9	44.7	38.9	101.0	93.1	85.4	72.7	60.7	54.1	46.8
13	76.6	70.7	64.9	58.0	48.0	43.0	37.5	95.0	87.6	80.3	68.5	57.4	51.4	44.5
14	73.2	67.6	62.0	55.4	45.9	41.2	36.1	88.6	81.6	74.8	64.0	54.0	48.5	42.3
15	69.6	64.2	58.8	52.7	43.6	39.3	34.5	82.4	75.8	69.1	59.4	50.3	45.3	39.7
16	65.7	60.6	55.6	49.7	41.3	37.3	32.9	76.6	70.4	63.9	55.3	46.7	42.2	37.2
17	61.8	56.9	52.2	46.6	38.9	35.2	31.1	71.4	65.3	59.2	51.5	43.6	39.4	34.6
18	58.1	53.5	48.9	43.5	36.4	33.1	29.3	66.5	60.7	55.0	47.9	40.5	36.8	32.4
19	54.6	50.2	46.0	40.7	34.2	31.1	27.5	62.0	56.5	51.2	44.6	37.7	34.2	30.3
20	51.5	47.2	43.1	38.1	32.2	29.2	25.9	57.9	52.7	47.8	41.5	35.2	31.9	28.2
21	48.5	44.5	40.5	35.8	30.2	27.5	24.5	54.2	49.3	44.6	38.8	32.8	29.8	26.4
22	45.8	42.0	38.1	33.7	28.4	25.8	23.0	50.8	46.2	41.8	36.3	30.7	27.9	24.7
23	43.2	39.5	35.8	31.6	26.7	24.3	21.6	47.6	43.3	39.1	34.0	28.8	26.1	23.1
24	40.8	37.3	33.8	29.9	25.2	22.9	20.3	44.7	40.7	36.8	32.0	27.1	24.5	21.7
25	38.6	35.3	31.9	28.2	23.7	21.6	19.2	42.1	38.4	34.6	30.1	25.4	23.0	20.3
26	36.6	33.3	30.1	26.6	22.4	20.4	18.1	39.8	36.1	32.6	28.3	23.9	21.7	19.1

L6.0x6.0																		
KL (ft)	Grade 36.0 ksi									Grade 50.0 ksi								
	1	7/8	3/4	5/8	9/16	1/2	7/16	3/8	5/16	1	7/8	3/4	5/8	9/16	1/2	7/16	3/8	5/16
1	61.3	56.2	50.5	44.4	40.6	34.7	29.9	24.2	18.2	84.7	77.5	69.5	57.0	52.1	45.5	37.9	30.0	21.8
2	61.0	55.9	50.3	44.1	40.5	34.5	29.8	24.1	18.2	84.1	77.0	69.0	56.6	51.8	45.2	37.8	29.9	21.7
3	60.3	55.5	49.9	43.7	40.1	34.3	29.6	24.0	18.1	82.9	76.0	68.2	56.1	51.3	44.8	37.5	29.7	21.6
4	59.0	54.3	49.2	43.3	39.7	33.9	29.3	23.7	17.9	80.5	74.0	67.0	55.2	50.5	44.2	37.0	29.3	21.4
5	57.5	52.9	47.8	42.5	39.1	33.4	29.0	23.5	17.8	77.6	71.4	64.6	54.0	49.6	43.5	36.5	28.9	21.1
6	55.7	51.2	46.3	41.1	38.0	32.8	28.5	23.2	17.6	74.3	68.4	61.7	51.6	47.8	42.4	35.8	28.4	20.9
7	53.6	49.3	44.6	39.6	36.6	31.7	27.9	22.8	17.3	70.6	64.9	58.6	49.1	45.4	40.4	34.8	27.9	20.5
8	51.4	47.2	42.6	37.9	35.0	30.3	26.8	22.3	17.1	66.6	61.1	55.1	46.4	42.8	38.1	33.0	27.2	20.2
9	49.1	45.0	40.6	36.1	33.2	29.0	25.6	21.4	16.7	62.2	57.0	51.4	43.4	39.9	35.7	31.1	25.7	19.7
10	46.4	42.6	38.4	34.1	31.4	27.4	24.3	20.4	16.2	57.4	52.5	47.3	40.0	36.9	33.1	28.9	24.2	18.9
11	43.6	40.0	36.0	32.0	29.4	25.7	22.9	19.2	15.5	52.3	47.8	42.9	36.4	33.5	30.2	26.6	22.4	17.8
12	40.7	37.2	33.4	29.7	27.4	23.9	21.4	18.1	14.6	47.7	43.4	38.9	33.1	30.5	27.4	24.2	20.5	16.5
13	37.5	34.3	30.7	27.3	25.1	22.0	19.7	16.8	13.7	43.5	39.6	35.2	30.1	27.7	24.9	22.1	18.7	15.2
14	34.7	31.7	28.3	25.1	22.9	20.3	18.1	15.4	12.7	39.8	36.2	32.0	27.5	25.2	22.7	20.1	17.1	13.9
15	32.1	29.2	26.1	23.0	21.0	18.7	16.7	14.3	11.8	36.5	33.0	29.2	25.1	22.9	20.6	18.3	15.6	12.9
16	29.7	27.1	24.1	21.2	19.3	17.2	15.4	13.2	10.9	33.6	30.3	26.7	23.0	20.9	18.8	16.7	14.2	11.7
17	27.6	25.0	22.4	19.5	17.8	15.9	14.2	12.1	10.2	30.8	27.8	24.6	21.1	19.2	17.3	15.3	13.0	10.7
18	25.7	23.3	20.7	18.0	16.4	14.7	13.1	11.2	9.4	28.5	25.6	22.6	19.4	17.6	15.9	14.0	12.0	9.9
19	23.9	21.7	19.2	16.8	15.3	13.6	12.2	10.4	8.7	26.3	23.7	20.9	18.0	16.3	14.6	13.0	11.0	9.1
20									8.0									8.4

L5.0x5.0														
KL (ft)	Grade 36.0 ksi							Grade 50.0 ksi						
	7/8	3/4	5/8	1/2	7/16	3/8	5/16	7/8	3/4	5/8	1/2	7/16	3/8	5/16
1	42.8	39.1	34.6	29.5	24.6	21.0	16.4	59.2	54.0	47.6	37.8	32.9	26.9	20.5
2	42.5	38.8	34.4	29.2	24.4	21.0	16.4	58.5	53.5	47.1	37.5	32.6	26.7	20.3
3	41.6	38.2	33.9	28.9	24.2	20.7	16.3	56.9	52.3	46.4	36.9	32.1	26.3	20.1
4	40.3	37.1	33.0	28.4	23.7	20.4	16.0	54.6	50.2	44.6	36.1	31.4	25.9	19.8
5	38.8	35.6	31.7	27.4	23.2	20.1	15.8	51.9	47.7	42.3	34.4	30.4	25.3	19.4
6	37.2	34.1	30.3	26.1	22.2	19.4	15.4	48.9	44.7	39.8	32.4	28.7	24.2	18.9
7	35.3	32.4	28.8	24.8	21.1	18.5	14.9	45.4	41.6	36.9	30.1	26.7	22.6	18.1
8	33.2	30.4	27.0	23.2	19.8	17.4	14.2	41.6	38.0	33.6	27.5	24.5	20.8	16.8
9	31.0	28.3	25.0	21.6	18.4	16.2	13.3	37.4	34.1	30.1	24.7	22.0	19.0	15.5
10	28.6	26.0	23.0	19.7	17.0	14.9	12.3	33.5	30.4	26.8	22.1	19.6	17.0	13.9
11	26.0	23.6	20.8	17.9	15.4	13.6	11.2	30.1	27.3	23.8	19.7	17.6	15.2	12.5
12	23.6	21.5	18.9	16.0	14.0	12.3	10.2	27.1	24.5	21.3	17.6	15.6	13.6	11.2
13	21.6	19.6	17.2	14.5	12.6	11.2	9.3	24.5	22.1	19.1	15.8	14.0	12.2	10.1
14	19.8	17.8	15.6	13.2	11.6	10.1	8.5	22.2	19.9	17.2	14.2	12.6	11.0	9.1
15	18.2	16.3	14.3	12.0	10.6	9.1	7.7	20.2	18.0	15.7	12.9	11.4	9.8	8.2
16	16.7	15.0	13.1	11.0	9.7	8.4	7.0	18.4	16.5	14.3	11.7	10.4	9.0	7.4

**Allowable Axial Load in Kips (cont.)**

<b>L4.0x4.0</b>														
<b>KL (ft)</b>	<b>Grade 36.0 ksi</b>							<b>Grade 50.0 ksi</b>						
	$\frac{3}{4}$	$\frac{5}{8}$	$\frac{1}{2}$	$\frac{7}{16}$	$\frac{3}{8}$	$\frac{5}{16}$	$\frac{1}{4}$	$\frac{3}{4}$	$\frac{5}{8}$	$\frac{1}{2}$	$\frac{7}{16}$	$\frac{3}{8}$	$\frac{5}{16}$	$\frac{1}{4}$
1	27.7	24.9	21.6	19.5	17.2	13.7	10.3	38.4	34.4	29.7	26.9	22.1	17.6	12.8
2	27.3	24.5	21.4	19.3	17.1	13.6	10.2	37.6	33.8	29.3	26.4	21.8	17.4	12.7
3	26.5	23.8	20.8	18.9	16.7	13.4	10.1	36.0	32.2	28.3	25.8	21.3	17.0	12.5
4	25.3	22.7	19.9	18.1	16.2	13.0	9.9	33.8	30.4	26.5	24.1	20.3	16.5	12.2
5	23.9	21.4	18.7	17.1	15.2	12.4	9.6	31.3	28.1	24.5	22.3	18.8	15.5	11.8
6	22.4	20.0	17.5	15.9	14.2	11.6	9.1	28.5	25.4	22.2	20.2	17.1	14.1	11.0
7	20.7	18.4	16.1	14.6	13.0	10.6	8.5	25.2	22.5	19.5	17.7	15.1	12.6	10.0
8	18.7	16.7	14.4	13.2	11.7	9.7	7.7	22.1	19.6	16.9	15.2	13.1	11.0	8.8
9	16.6	14.8	12.8	11.6	10.3	8.6	7.0	19.3	17.1	14.6	13.2	11.4	9.6	7.7
10	14.9	13.2	11.3	10.2	9.0	7.6	6.2	17.0	15.0	12.7	11.4	9.9	8.4	6.7
11	13.4	11.8	10.1	9.1	8.0	6.7	5.4	15.1	13.2	11.2	10.1	8.7	7.3	5.9
12	12.0	10.5	9.0	8.1	7.1	6.0	4.9	13.5	11.7	9.9	8.9	7.6	6.5	5.2
13			8.1	7.2	6.3	5.4	4.3			8.8	7.9	6.8	5.7	4.6

<b>L3.5x3.5</b>											
<b>KL (ft)</b>	<b>Grade 36.0 ksi</b>					<b>Grade 50.0 ksi</b>					
	$\frac{1}{2}$	$\frac{7}{16}$	$\frac{3}{8}$	$\frac{5}{16}$	$\frac{1}{4}$	$\frac{1}{2}$	$\frac{7}{16}$	$\frac{3}{8}$	$\frac{5}{16}$	$\frac{1}{4}$	
1	17.7	16.1	14.5	11.7	9.3	24.3	22.1	18.6	15.7	11.7	
2	17.4	15.8	14.3	11.5	9.1	23.8	21.7	18.3	15.5	11.6	
3	16.7	15.2	13.8	11.2	8.9	22.5	20.6	17.5	15.0	11.3	
4	15.7	14.3	13.0	10.6	8.7	20.7	18.9	16.2	14.0	10.9	
5	14.6	13.3	12.1	9.9	8.1	18.7	17.0	14.6	12.6	9.9	
6	13.3	12.1	11.0	9.1	7.4	16.3	14.9	12.8	11.1	8.8	
7	11.9	10.8	9.8	8.1	6.7	14.0	12.6	10.9	9.4	7.6	
8	10.4	9.4	8.5	7.1	5.9	12.0	10.7	9.4	8.1	6.6	
9	9.0	8.3	7.4	6.2	5.1	10.2	9.3	8.1	6.9	5.5	
10	8.0	7.2	6.4	5.5	4.5	8.9	7.9	7.0	6.0	4.9	
11	7.1	6.3	5.6	4.7	3.9	7.8	6.9	6.0	5.2	4.2	

<b>L3.0x3.0</b>												
<b>KL (ft)</b>	<b>Grade 36.0 ksi</b>						<b>Grade 50.0 ksi</b>					
	$\frac{1}{2}$	$\frac{7}{16}$	$\frac{3}{8}$	$\frac{5}{16}$	$\frac{1}{4}$	$\frac{3}{16}$	$\frac{1}{2}$	$\frac{7}{16}$	$\frac{3}{8}$	$\frac{5}{16}$	$\frac{1}{4}$	$\frac{3}{16}$
1	14.0	12.8	11.6	10.1	7.9	5.5	19.2	17.7	15.9	13.0	10.3	6.9
2	13.5	12.4	11.3	9.9	7.7	5.4	18.5	17.0	15.4	12.6	10.1	6.8
3	12.8	11.8	10.7	9.4	7.5	5.3	17.2	15.7	14.3	11.9	9.6	6.5
4	11.8	10.9	9.9	8.7	7.0	5.1	15.4	14.2	12.8	10.6	8.8	6.2
5	10.8	9.9	8.9	7.8	6.3	4.7	13.3	12.2	11.1	9.2	7.6	5.5
6	9.5	8.6	7.8	6.9	5.5	4.1	11.2	10.2	9.2	7.7	6.3	4.7
7	8.1	7.4	6.7	5.9	4.7	3.6	9.4	8.6	7.6	6.5	5.3	4.0
8	7.0	6.4	5.7	4.9	4.0	3.1	8.0	7.2	6.4	5.4	4.4	3.3
9	6.0	5.5	4.9	4.2	3.5	2.6	6.8	6.1	5.4	4.6	3.8	2.8

<b>L2.5x2.5</b>										
<b>KL (ft)</b>	<b>Grade 36.0 ksi</b>					<b>Grade 50.0 ksi</b>				
	$\frac{1}{2}$	$\frac{3}{8}$	$\frac{5}{16}$	$\frac{1}{4}$	$\frac{3}{16}$	$\frac{1}{2}$	$\frac{3}{8}$	$\frac{5}{16}$	$\frac{1}{4}$	$\frac{3}{16}$
1	10.4	8.8	7.7	6.5	4.7	14.3	12.1	10.6	8.4	6.0
2	9.8	8.4	7.4	6.3	4.6	13.4	11.4	10.1	8.0	5.8
3	9.1	7.8	6.8	5.9	4.4	12.1	10.2	9.1	7.2	5.4
4	8.3	6.9	6.1	5.2	3.9	10.5	8.7	7.7	6.2	4.7
5	7.2	6.0	5.3	4.5	3.4	8.5	7.0	6.2	5.0	3.9
6	6.0	5.0	4.3	3.7	2.8	7.0	5.8	4.9	4.1	3.1
7	5.0	4.1	3.6	3.1	2.3	5.7	4.6	4.0	3.4	2.5
8	4.3	3.5	3.1	2.6	2.0	4.8	3.9	3.3	2.7	2.1

<b>L2.0x2.0</b>										
<b>KL (ft)</b>	<b>Grade 36.0 ksi</b>					<b>Grade 50.0 ksi</b>				
	$\frac{3}{8}$	$\frac{5}{16}$	$\frac{1}{4}$	$\frac{3}{16}$	$\frac{1}{8}$	$\frac{3}{8}$	$\frac{5}{16}$	$\frac{1}{4}$	$\frac{3}{16}$	$\frac{1}{8}$
1	6.0	5.4	4.7	3.7	2.2	8.3	7.5	6.5	4.8	2.8
2	5.6	5.1	4.4	3.5	2.2	7.6	6.8	5.9	4.5	2.7
3	5.0	4.5	3.9	3.1	2.0	6.4	5.7	5.0	3.8	2.4
4	4.3	3.8	3.2	2.6	1.7	5.1	4.5	3.8	3.0	2.0
5	3.4	3.0	2.6	2.1	1.4	3.9	3.5	3.0	2.3	1.5
6	2.8	2.5	2.1	1.7	1.1	3.1	2.7	2.3	1.8	1.2